| From: | Tremblay, Jean-Daniel |
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| To: | Simard, Gilles |
| Subject: | LCP Basis of Estimate |
| Date: | Monday, October 15, 2012 10:40:00 AM |
| Attachments: | 505573-0000-33RA-I-0001.pdf <br> image001.ipq <br> image002.ipg |
|  | image003.ipg |

Bonjour Gilles,

Tel que discuté, ci-joint la version du 15 décembre 2011 du BOE que j'avais préparé.

Bonne lecture et à bientôt.

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SNC-Lavalin Inc.
Lower Churchill Project Office, 350 Torbay Road
St. John's | Newfoundland and Labrador | Canada | A1A 4E1


[^0]
## Lower Churchill Project <br> DG3 Capital Cost Estimate BASIS OF ESTIMATE

SLI Document No. 505573-0000-33RA-I-001
Nalcor Reference No. LCP-SN-CD-0000-EP-ES-0002-01
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## 1 VOLUME I - CAPITAL COST BASIS OF ESTIMATE - GENERAL CONSIDERATIONS

### 1.1 PROJECT DESCRIPTION

The Churchill River is located in Labrador in the Province of Newfoundland and Labrador, Canada. The existing 5,428 megawatt (MW) Churchill Falls Generating Station, which began producing power in 1971, harnesses about 65 per cent of the potential generating capacity of the river. The remaining 35 percent is planned to be developed via two sites on the lower Churchill River, known as the Lower Churchill Project (LCP).

### 1.1.1 Description of the LCP

The LCP consists of two undeveloped hydroelectric sites and associated transmission systems: Gull Island Hydroelectric Development, located 225 kilometres downstream from the existing Churchill Falls Generating Station; and Muskrat Falls Hydroelectric Development, located 60 kilometres downstream from the proposed Gull Island Hydroelectric Development.

The Gull Island Hydroelectric Development will consist of a generating station with a capacity of 2,250 MW, while the Muskrat Falls Hydroelectric Development will consist of a generating station of 824 MW capacity and associated transmission systems.

### 1.1.2 LCP Phase 1

Phase 1 of the Lower Churchill Project comprises the Muskrat Falls Hydroelectric Plant and associated transmission lines and DC specialties. It is comprised of three discrete physical Components, as follows:

- Component 1: Muskrat Falls Hydroelectric Development
- Component 3: High voltage direct current transmission system specialties
- Component 4: High voltage overhead transmission lines (ac and dc) including:

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Sub-component 4A: HVdc overhead transmission lines Muskrat Falls to Soldiers Pond

Sub-component 4B: HVac overhead transmission lines Muskrat Falls to Churchill Falls

### 1.1.2.1 Component 1 - Muskrat Falls Hydroelectric Development

The Muskrat Falls Hydroelectric Development will include the following subcomponents which are broken down under the five principal areas of the development.

## Infrastructure

a) 22 km of access roads, including upgrading and new construction, and temporary bridges;
b) A 1,500 person accommodations complex (for the construction period); and

## Dams and Spillway

a) A north RCC overflow dam;
b) A south RCC dam;
c) River diversion during construction via the spillway;
d) Gated spillway.

## Reservoir

a) Reservoir preparation and reservoir clearing;
b) Replacement fish and of terrestrial habitat;
c) North spur stabilization.

## Intake / Powerhouse / Turbine Generator

A close coupled intake and powerhouse, including:
4 intakes with gates and trash racks;

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4 turbine/generator units at approximately 206 MW each with associated ancillary electrical/mechanical and protection/control equipment;

5 power transformers (includes 1 spare), located on the draft tube deck of the powerhouse;

2 overhead cranes.

A more detailed Project description of Component 1 is included in document 505573-3000-4000-0001.

### 1.1.2.2 Component 3 - High Voltage Direct Current Transmission System Specialties

Component 3 consists of the HVdc converter station systems associated with the high voltage direct current (HVdc) transmission system. The Component 3 HVdc facilities will comprise the following:

AC switchyard at Muskrat Falls;
Churchill Falls switchyard extension.

Muskrat Falls HVdc converter station:
HVdc bipolar converter station;
345 kV ac, converted to $\pm 320 \mathrm{kV}$ dc;
Pole capacity of 450 MW ; and
Shoreline pond electrode located on the Labrador side of the Strait of Belle Isle.

The shoreline pond electrode will be connected to the converter station at Muskrat Falls with dual overhead conductors supported on a wood pole line. The wood pole line and conductors will form part of Component 4.
a) Soldiers Pond HVdc converter station:

HVdc bipolar converter station;

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230 kV ac, converted from $\pm 320 \mathrm{kV}$ dc;
Pole capacity of 450 MW ; and
Shoreline pond electrode located on the east shore of Conception Bay.
The shoreline pond electrode will be connected to the converter station at Soldiers Pond with dual overhead conductors supported on a wood pole line. The wood pole line and conductors will form part of Component 4.

HVdc Transition Compounds for the Strait of Belle Isle submarine cable terminations:
One transition compound for each side of the Strait of Belle Isle submarine cable crossing,
Associated switch works to manage the junction of multiple submarine cables and the overhead transmission line.
Telecoms.
For the purposes of the EPCM Contract, the scope of work does not include any infrastructure or services associated with the actual crossing of the Strait of Belle Isle.

### 1.1.2.3 Component 4 - High Voltage Overhead Transmission Lines

The high voltage overhead transmission lines required for Phase 1 comprise high voltage alternating current ( HVac ) lines, high voltage direct current ( HVdc ) lines, and electrode lines described as follows:

Sub-Component 4A: HVdc Overhead Transmission Lines Muskrat Falls to Soldiers Pond

Overhead Transmission Line:
Transmission line from Muskrat Falls converter station to Soldiers Pond converter station (near St. John's, NL):
$900 \mathrm{MW}, \pm 320 \mathrm{kV}$ dc, bipole line, single conductor per pole;
Galvanized lattice steel guyed suspension and rigid angle towers;
1100 km long.

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Connections to HVdc transmission system specialties installations, as described in Component 3 herein, will be required.

Electrode Lines:
Dual overhead conductors supported on a wood pole line from Muskrat Falls converter station to the shoreline pond electrode located on the Labrador side of the Strait of Belle Isle;
Dual overhead conductors supported on a wood pole line from Soldiers Pond converter station to the shoreline pond electrode located on the east shore of Conception Bay.

## Sub-Component 4B: HVac Overhead Transmission Lines Muskrat Falls to Churchill Falls

## Churchill Falls

Transmission lines from Muskrat Falls to Churchill Falls:
$2-345 \mathrm{kV}$ ac, 3 phase lines, double bundle conductor;
Single circuit galvanized lattice steel guyed suspension and rigid angle towers; 265 km long.

### 1.2 ABBREVIATIONS

NE-LCP - Nalcor Energy - Lower Churchill Project
SLI - SNC Lavalin Inc.
SOBI - Strait of Belle Isle
CCE - DG3 Capital Cost Estimate
ES - Estimating Software (HCSS Heavy Bid estimating software)
BOQ - Bill of Quantities
MTO - Material Take Off

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RCC - Roller Compacted Concrete
HADD - Harmful Alteration Disruption or Destruction (of fish habitat)
HVac - High Voltage Alternating Current
HVdc - High Voltage Direct Current
EIA - Environmental Impact Assessment
MF - Muskrat Falls
CF - Churchill Falls
SP - Soldier's Pond
GI - Gull Island
ROW - Right Of Way
PMPC - Project Management / Project Controls
DWSM - Dual Window Single Mode

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### 1.3 ESTIMATING TEAM STRUCTURE AND MEMBERS



### 1.4 TYPE OF ESTIMATE

The DG3 Capital Cost Estimate (CCE) is a Class III AACE 17R-97 estimate. The CCE describes the complete project and installations to be built and provides sufficient scope definition for Management / Board approval, financing, budgeting and control. All costs are expressed in Canadian Q4 of 2011.

Estimate accuracy is suitable for external financing (i.e. bankable document).

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### 1.5 SCOPE OF ESTIMATE

The CCE builds on the estimating work completed since late 2007 for the Project, and reflects the latest project configuration as defined in the latest Basis of engineering document. The CCE was prepared to confirm the business case in order to proceed to Project Sanction.

The CCE was compiled using the latest engineering definition and layout, materials and labour pricing the cost estimate was a bottom up estimate using the four (4) estimate elements:

1. Project Definition / Scope: location, plant definition, major equipment, design constraints, materials, and quantities
2. Construction Methodology: build sequence, construction equipment, labour demands, trade mix, in-directs, support facilities, seasonality
3. Price: labour rates, equipment rates, commodity rates, material costs, and contracting and procurement strategy.
4. Performance: labour productivity, mobilization, seasonality impacts, and project management resources.

The following estimating activities were performed by the estimating team and were integrated into the Estimating Software (ES) (HCSS's Heavy Bid software version 2010.3):

- Assemble the project MTO's from engineering;
- Perform bottom up estimate on a first principle basis (quantities, crews, production rates and unit costs)
- Perform reasonable evaluation based on past experience for similar projects in comparable conditions if needed;
- Perform all commercial bid evaluations on equipment and bulk materials quotes;
- Compile and use In-House pricing as necessary;

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- Prepare Basis of Estimate for estimator-specific scopes;
- Participate in estimate reviews with the engineering and project management team;
- Populate estimating forms for integration of estimates into the ES.
- Joint SLI / Nalcor estimate review meeting from November 15 to 18, 2011 from which an action items list was developed, addressed and integrated into the December 15, 2011 CCE.

The CCE quantities have been developed using the Metric System of measurement. Cable and wire have been measured in American Wire Gauge (WG).

The CCE considers all costs from Project construction initiation to commissioning, including:

- All accesses and ancillary works
- Procurement and logistics
- Camps and living accommodations for all Components
- Camps security and medical services
- Contractor Construction Management (CCM)
- On-site Temporary Construction Facilities
- Construction
- Commissioning
- EPCM Costs

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### 1.6 WORK BREAKDOWN STRUCTURE

The work breakdown structure coding system implemented for the CCE (Appendix 1) is an eight (8) digit coding system that integrates within the first four (4) digits the NALCOR physical components coding structure as provided by NALCOR (Appendix 2). The last four digits of the coding system serve to further breakdown these physical components into estimated work items comprising the actual work activities.

### 1.7 TIME PHASING METHODOLOGY

The relevant construction portions of the latest Master Project Schedule were provided to each estimator along with the other documents required for them to produce the estimate. Final time phasing was conducted and validated at estimate close-out while producing labour and cash flow curves.

### 1.8 SPECIAL PROJECT ORDER (CRAFT WAGE RATES) AND LABOUR HOURS

At date of issuance of the CCE, the Lower Churchill Project SPO had not been sanctioned and negotiations between Nalcor and Unions were pending or underway. Craft wage rates used throughout the CCE were provided by Nalcor and reflect the rates of the other unspecified SPO. The CCE labour rates are presented in Appendix 3 and include all shifts, burdens/benefits, and premiums.

For the purpose of producing labour flow curves and indicating the labour requirements over the duration of the Project, the CCE includes all labour hours required to perform the work of all Components of the Project.

- All direct labour hours based on readily available published productivity charts and/or SLI historical data.
- All base hours for electrical, mechanical, structural steel and architectural work estimates are based on USGC to which a site-specific adjustment factor was applied to the chart hours.

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- For major items for which a turn-key lump sum budget or bid price was obtained for the purpose of the estimate, an evaluation based on past experience and proxy crews was conducted to establish the total labour hours by trade required for the construction of these items.


### 1.9 EQUIPMENT RATES

Construction equipment rates taken mainly from WEB based Equipment Watch July 2011 (www.equipmentwatch.com). For specialized equipment not present in the Equipment Watch tables, rates were developed from past experience on similar project in comparable conditions. Fuel consumption per equipment included in the tables was used to determine the fuel consumption for the Project. The fuel costs reflected in these tables are the following:

- Diesel fuel cost at $\$ 1.44 / \mathrm{litre}$
- Gasoline fuel cost at $\$ 1.44 / \mathrm{litre}$

The equipment rates used in the CCE are presented in Appendix 4.

### 1.10 ASSUMPTIONS, EXCLUSIONS AND EXCEPTIONS

- General instructions were provided to estimators prior to commencement of detailed estimating work. These instructions, referred to as the Estimate Ground Rules, addressed general assumptions and base rates to be considered for estimating direct costs and construction indirect costs throughout the CCE. The Estimate Ground Rules are presented in Appendix 5.
- Room and board provided to Contractors at free issue but considered and estimated for each Component and identified as a Project Indirect Cost in the CCE.
- Labour rotation is 21 days work on site and 7 days off.

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- No environmental Assessment report was available at time of CCE issuance. Assumptions and provisions included in the CCE related to environmental impact mitigation (HADD mitigation work) items are based on past experience for similar projects
- The Goods and Services taxes are not included in the estimate.
- All equipment and bulk materials import duties are excluded.
- Brokerage/agents fees for equipment imported into Canada duty free are excluded.
- No provisions or allowances have been included in the CCE to account for the following costs as these are owned by NALCOR:
- Contingencies and risks allowances
- Escalation on labour rates and inflation
- Financing costs
- Insurance and bonding
- Land acquisitions
- Project level governmental permitting
- Owner costs


### 1.11 ALLOWANCES

The CCE includes no allowances other than those indicated in the details of the following sections of this Basis of estimate document for specific items for which they were deemed necessary to properly estimate the work item.

### 1.12 PROJECT AND CONSTRUCTION INDIRECT COSTS

Project indirect costs are incurred on a Project level to support all the construction work package activities whereas the Construction indirect costs are incurred by

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Contractors in the effort of executing their awarded construction work package. The basis for the estimation of these costs is presented below.

### 1.12.1 Project Indirect Costs

### 1.12.1.1 Main Access Road and Existing Bridges Replacement

The estimated cost of the 22 km main access road from the Trans Labrador Highway to the Muskrat Falls project site was based on the cost of other road work in Labrador factored to project cost.

The cost for the Kenamu Bridge and Paradise Bridge replacements required to increase the load capacity to 250 metric tons are based on the actual cost of the existing bridges adjusted by increases in current labour and material cost.

### 1.12.1.2 Construction Camps Construction and Operations for the Duration of the Project

Costs of site preparation of the main Camp area at Muskrat Falls include the following:

- Clearing based on a cost per hectare established on a first principal basis developed for clearing highway right of ways in Labrador and applied to the main camp area.
- Civil works and camp infrastructure construction based on similar work being done in Labrador by SLI, factored to project cost.
- A provision for the procurement, installation and operation of a 150 people starter-camp to lodge first workers and staff on site. The definite scope of this work item still needs to be clarified and agreed by Nalcor.

Procurement cost of the 1500 people camp facilities as well as administrative and support facilities including transport to site and installation are based on parametric data as well as quotes provided by suppliers and validated by benchmarking with similar projects in comparable conditions. Firm quotes from suppliers are expected in early 2012.

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Camp operations include all necessary activities to provide suitable living and working accommodations. Basis of Camp operation costs are as follow:

- Catering costs based on past experience and Nalcor recommendations
- House keeping costs based on past experience
- Facilities maintenance and cleaning based on past experience
- Site maintenance costs based on past experience
- Garbage removal based on past experience

Cost of Transmission lines (TL) camps to be constructed along the TL ROW were estimated by factoring the main camp cost as well as by benchmarking similar project in comparable conditions on a per bed basis and adjusted to consider additional operating costs due to lower capacity and increased remoteness.

### 1.12.1.3 Air Travel and Transportation of Workforces, EPCM and Client Personnel Between Work Areas and Point of Origin

Air travel costs were estimated using a unit value per kilometre travelled provided by local airlines for commercial flights and chartered flights applied to distances between five points of origins and the Muskrat Falls site. Over the duration of the Project, an estimated total of 138000 trips will be made to the Muskrat Falls site, on 21-7 rotations for craft personnel or 11-3 rotations for staff, from five origins in the following proportions for all Component of the Project:

- St-John's: $25 \%$
- Deer Lake: 25\%
- Moncton: 20\%
- Montreal: 15\%
- Toronto: 15\%
- Plane capacity utilization at $75 \%$

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- Chartered flights for the St-John's and Deer lake origins
- Commercial flights for Toronto, Montreal and Moncton origins
- Travel time paid to personnel includes only 8hres hire-in and 8hres termination-out for a total 16 hrs per turnaround. Assumption for the number of turnarounds is 1000 pers $\times 3$ turnarounds $=3000$.
- No travel time is paid on 21-7 rotations
- Hotel \& Meals at St-John's and Deer Lake at a cost of $150 \$$ for each rotation
- Hotel \& Meals at Toronto, Montreal and Moncton at a cost of $190 \$$ for each rotation
- Transportation expenses (Taxi, bus, etc.) between home and airport at $100 \$$ for each rotation


### 1.12.1.4 Health and Medical Services

The CCE includes Construction health and medical services for both the Muskrat Falls facilities as well as services to be provided along the TL ROW.

Quantification of the required provision of medical services is based on the assumption that the services include the following:

Component 1:

- a well equipped $24 / 7$ medical facility at the Muskrat Falls construction camp site to cover the camp's medical requirements as well as a portion of the requirement for the reservoir clearing.
- Medical transport vehicles adequate to transport patients to the Happy Valley Goose Bay hospital
- For remainder of reservoir clearing operation, Emergency Medical Technician (EMT) equipped with Mobile Treatment Centers (MTC) which can double as Medical transport vehicles

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Component 4:

- EMTs and MTCs in each of the satellite camps
- Provision


## Component 3:

- Medical services provided by either Component 1 or Component 4 services in the Labrador portion of the Project and in remote area in Long Range Mountains in Newfoundland
- Medical services will be provided by existing medical facilities in Newfoundland where work areas are relatively close by.

Scope of medical services requirement was developed while preparing the Medical services contract document to be issued for bids in late 2011 and integrate coordinated needs of Components 1, 3 and 4. Cost of medical services was estimated based on estimator experience and input from specialized vendors and service providers.

The CCE also includes the cost for helicopter medical evacuations (medevacs) based on the following assumptions:

- Over the course of the entire project, there will be 1 medevac made per week (both non-work related medical emergencies and work related injuries and illnesses) for a total of 50 medevacs per year for 5 years, resulting in a total of 250 medevacs for the project.
- Each medevac flight will have an average duration of 3 hours
- Average cost for flight hour is $\$ 2,200.00$


### 1.12.1.5 Mandatory Pre-Access Drug and Alcohol Testing

All personnel working on any phase of the project outside the project office in St. John's will be required to undergo a Drug and Alcohol Screening Test and have a

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Medical Examination completed prior to being dispatched to site. The estimate included in the CCE is based on the current market value of those services and the projected number of personnel anticipated to work on the Project and comprises the following assumptions and rates:

- Cost of Drug and Alcohol Screen using current Urine or Mouth Swab techniques will be $\$ 250.00$ per test
- Pre access Medical Examination will be $\$ 250.00$ per test

It is projected that a total of 12,000 personnel (SNC-Lavalin, Nalcor and Contractor personnel) will be engaged over the life of the project. This number also takes into consideration those personnel who will be away from the project for a period of 3 months or more and will require to be retested.

### 1.12.1.6 Safety and Security Services and Equipment

The CCE includes estimates based on estimator experience and supplier input for the following:

- On site security service including security personnel, vehicles and equipment
- Rescue boat including 1 boat trailer and rescue equipment
- Safety signage on Sites and on access road to Main site
- Security access swipe cards for access to Main site and accommodation complex
- Personal Protection Equipment for EPCM personnel


### 1.12.2 Construction Indirect Costs

Construction indirect costs included in the CCE are based on typical costs, based on past experience, incurred by Contractors required for executing their awarded construction work packages such as:

- Contractor mobilization and demobilization costs

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- Rental, installation and operation of temporary construction site offices and facilities
- Contract administration and management personnel
- Site supervision, health and safety, survey and Contractor quality assurance personnel over viewing work performed by own foremen and direct workforce
- Utility supply such as air, water, electricity, etc.
- Job office expenses
- Administration fees to cover contractor home office expenses, overhead and profits were included to the estimated items as follow:
- A $10 \%$ of direct costs allowance was added to all electrical, mechanical, powerhouse superstructure and architecture as well as substations electrical and civil works
- A $15 \%$ of direct costs allowance was added to the powerhouse concrete works
- No allowance was included in the mass excavation, dams and cofferdams estimate as direct and indirect values are at cost.
- All other estimates developed using market pricing or budget quotes are deemed to be inclusive of profit and administration at a reasonable rate.
- Pickups, site communication, heavy equipment repair and maintenance shops and ownership insurance.


### 1.13 <br> EPCM COSTS

Engineering, Procurement and Construction Management (EPCM) costs were developed using a bottom-up approach for each Component of the Project as well as general items which are not Component specific. The EPCM costs are presented in

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the estimate as a one line item and estimate details and backup are submitted as a separate document.

### 1.13.1 Engineering of Components 1, 3 and 4

The engineering of all Project Components was sufficiently developed to allow for the production of Bill of Quantities (BOQ) sufficiently detailed to allow for bottom up estimation for most.

### 1.14 OWNER COSTS

Owner costs are not included in the scope of the CCE basis of estimate (BOE) document. These costs include:

- All contingencies
- Project risks and exposure
- Land acquisition costs
- Project level permitting costs
- Escalation of labour rates through the duration of the Project
- Inflation in the cost of commodities, materials, and equipment rates
- Financing costs
- All-risk Project insurance
- Costs related to Owner personnel and equipment

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## 2 VOLUME II - COMPONENT 1 DIRECT COSTS DETAILED BASIS OF ESTIMATE

### 2.1 INTRODUCTION

As described in Volume I, the Project's Component I includes the facilities, installations and equipments relative to infrastructure and main camp accommodations, the reservoir work, the dams and spillway and the powerhouse intake and turbine generators.

The following sections describe the basic assumptions considered as well as the means and methods utilized to develop the relevant cost estimates included in the CCE.

### 2.2 BASIS OF ESTIMATE - DIRECT COSTS

### 2.2.1 Reservoir Clearing

### 2.2.1.1 Scope

- The reservoir will be cleared using the "partial clearing criteria" as defined by Nalcor in their "Design Philosophy for LCP - Reservoir Preparation Plan"
- $40 \%$ of the area is located on the North Bank and $60 \%$ on the South bank
- the clearing method will be by a mechanical harvesting operation
- total area to be cleared, including reservoir, road rights-of-way and storage yards, is approximately 2200 ha, total merchantable wood is approximately $448,000 \mathrm{~m} 3$ which will be trucked out of the reservoir and piled at storage yards
- total road construction will be approx. 152 km . and 99 streams will be crossed

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### 2.2.1.2 Construction Methodology \& Timeline Factors

- Mechanical harvesting of merchantable \& non-merchantable wood with fellerbunchers and skidded to roadside
- Process merchantable wood at roadside to remove limbs and tops
- Merchantable wood will be trucked to storage yards and piled
- When possible deadfalls will be skidded to roadside as non-merchantable wood
- Non-merchantable wood, including deadfalls, and slash from processing merchantable wood will be mulched at roadside and the mulched fibre will be left
- Any areas of deadfalls not skidded and areas of shrubs (alder and willow) will be mulched wherever they occur within the ice and stickup zones and the mulched fibre will be left
- Clearing of the North Bank is scheduled to start in mid 2012 and will be finished at the end of 2014
- Clearing of the South Bank is scheduled to start towards the end of 2012 and will finish in early 2016
- People employed by the clearing contractor must be very skilled - from operators and mechanics to foremen and supervisors


### 2.2.1.3 Price Factors

- Labour and equipment rates as per general CCE rates as stated in Volume I
- Materials costs were obtained from suppliers of the various products used for the estimate and were FOB Goose Bay (as examples: bridges, culverts, material to construct bridge abutments, etc.)
- Certain items were estimated from past experience and bench-marking with industry contacts

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### 2.2.1.4 Performance Factors

- Assumed labour productivity at $70 \%$ based on rotation times of 21 days work/7days home and evaluated by using industry standard productivity tables.
- Equipment productivity factored to account for operating in sandy soils which offer poor traction and for skidding full-tree uphill to honour Nalcor's requirement that, where possible, roads be constructed $2 m$ below full supply level of 39 masl
- 42 - 43 weeks/year considered as the time frames for clearing operations. Note: there may be times during winter months that operations will be curtailed because of extreme snow depths and the weeks/year will be less than considered average


### 2.2.2 Mass Excavation

### 2.2.2.1 Scope

Bills of quantities (BOQ) were issued by engineering and a check BOQ was developed by estimators. Reconciled Engineering and Estimator BOQs revealed no significant differences in quantities. CCE Mass excavation major Quantities are as follow:

- Overburden material at the Powerhouse site: 455000 m 3
- Overburden material at the North Spur site: 600000 m 3
- Rock excavation : total volume 2092000 m 3
- Powerhouse : 1590000 (including rock plugs)
- Spillway : 250 000m3
- North Spur : 100 000m3
- $4,0 \mathrm{~m}$ long Rock bolt quantity : 882 units

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Rock bolts were quantified by engineering on the basis of available geotechnical information suggesting that the rock is of "excellent" quality (1 bore hole on North side) to "very good" quality (1 bore hole on South side) and based on rock bolt quantities for similar projects in James Baie with similar rock conditions.

For a Project this size, the number of boreholes (2) is clearly insufficient to properly assess the quality of the rock. An investigation campaign will be required when Project goes forward. There is a provision in the estimate to account for the risk related to the uncertainty of the rock characterization and the possibility that poor undetected geotechnical conditions arise during construction.

- Wire mesh area and pins : 50000 m 2
- Costs were included to account for average 500 mm thick concrete mud slabs where the Powerhouse and Spillway are to be concreted.


### 2.2.2.2 Construction Methodology \& Timeline Factors

- General assumption is that rock quality is not a concern and Project is standard rock excavation project.
- All excavation activities estimated on a six days per week basis to allow for a buffer for bad weather conditions. A total duration of 200 workdays (end of July 2012 to mid-April 2013) is considered in the estimate for the mass excavation of the powerhouse and spillway
- Rock excavation to start when overburden excavation has exposed sufficient areas to allow drill and blast operations to start.
- Excavation crew :
- Cat 992K loader
- 5 Cat 775F off-road dump truck
- Cat D8 at dump site

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- No provision is included for the cost of spare stand-by equipment on site but usually there should be 1 spare equipment for every five.


### 2.2.2.3 Price Factors

- Labour rates considered for this portion of the estimate is as provided by Nalcor.
- Equipment rates are a mix of Equipment watch rates with some specialized equipment having been adjusted to reflect actual rates of similar projects with comparable site conditions.


### 2.2.2.4 Performance Factors

- Haul and dump distance of $2,5 \mathrm{~km}$ from site to stockpile
- Production drilling at $20 \mathrm{~m} / \mathrm{hr}$ per drill using ROC D7 drills
- Large diameter line drilling performed with three drills at a rate of $15 \mathrm{~m} / \mathrm{hr}$ (re: action itemS1-6).
- Rock excavation drilled and blasted on two work shifts on multiple faces at a daily average of 10000 m 3 (or $5000 \mathrm{~m} 3 /$ shift) to meet the duration in schedule.
- Load and haul production estimated at $250 \mathrm{~m} 3 / \mathrm{hr}$ per crew and 2 crews are considered.
- Overburden mass excavation production rate $=150 \mathrm{~m} 3 / \mathrm{h}$
- Rock excavation - dry conditions production rate $=250 \mathrm{~m} 3 / \mathrm{h}$
- Drilling are estimated at a rate $=54 \mathrm{~m} / \mathrm{h}$
- Dynamite operations are estimated at a rate $=250 \mathrm{~kg} / \mathrm{h}$
- Excavated roc will be dump and stock piled at the north shore quarry.

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### 2.2.3 Fill structures

### 2.2.3.1 Scope factors

The scope of work considered in the CCE was developed by the engineering group who provided bill of quantities to estimators. Quantities were validated by estimators through an independent take-off exercise which revealed minimal differences. The quantities provided by the engineering group were used to develop the fill structures estimate and are as follow:

## Powerhouse Downstream Cofferdam

- Compacted Till-Zone 1: $12900 \mathrm{~m}^{3}$
- Compacted Granular - Zone 2C : $3700 \mathrm{~m}^{3}$
- Compacted Rockfill - Zone 3C : $12400 \mathrm{~m}^{3}$
- Riprap (produced by others) 4 Class 1:1200 m ${ }^{3}$


## Spillway Upstream Cofferdam

- Compacted Till - Zone $1: 8000 \mathrm{~m}^{3}$
- Compacted Granular - Zone 2C : $5500 \mathrm{~m}^{3}$
- Compacted Rockfill - Zone 3C : $43000 \mathrm{~m}^{3}$
- Riprap (produced by others) 4 Class $1: 3000 \mathrm{~m}^{3}$


## Spillway Downstream Cofferdam

- Compacted Till - Zone 1:5700 $\mathrm{m}^{3}$
- Compacted Granular - Zone 2C : $4500 \mathrm{~m}^{3}$
- Compacted Rockfill - Zone 3C : $33660 \mathrm{~m}^{3}$
- Riprap (produced by others) 4 Class $1: 2400 \mathrm{~m}^{3}$


## North Downstream Cofferdam

- Compacted Till - Zone 1:5466 m

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- Compacted Granular - Zone 2C : $2489 \mathrm{~m}^{3}$
- Compacted Rockfill - Zone 3C : 2352 m $^{3}$


## North Dam Upstream Rockfill Cofferdam

- Dumped Rockfill 0-900mm : $220000 \mathrm{~m}^{3}$
- Boulders $1000-1200 \mathrm{~mm}: 20000 \mathrm{~m}^{3}$
- Boulders 1200-1500: $25000 \mathrm{~m}^{3}$
- Dumped Granular or Crushed Rock max 300mm Zone 2E : $26000 \mathrm{~m}^{3}$
- Compacted Till-Zone 1: $19000 \mathrm{~m}^{3}$
- Compacted Granular - Zone 2C : $14000 \mathrm{~m}^{3}$
- Compacted Rockfill - Zone 3C ( $0-450 \mathrm{~mm}$ ) : $35000 \mathrm{~m}^{\mathbf{3}}$
- Compacted Rockfill - Zone 3D (0-900mm) : $38000 \mathrm{~m}^{3}$
- Riprap (produced by others) 4 Class $1: 3200 \mathrm{~m}^{3}$
- Dumped Rockfill (access road) 0-900mm : $75000 \mathrm{~m}^{3}$
- Dumped Till : $159000 \mathrm{~m}^{3}$


## South Rockfill Dam

- Compacted Till - Zone 1: $22118 \mathrm{~m}^{3}$
- Compacted Filter - Zone 2: $15373 \mathrm{~m}^{3}$
- Compacted Rockfill - Zone 3, 3B and $4: 77000 \mathrm{~m}^{3}$


### 2.2.3.2 Construction Methodology and Timeline Factors

- It is assumed that the main access road from the Trans-Labrador will be available for mobilization and commencement of the work in early summer 2012, that the contractor's pad will be ready, that the soil will be dry (overburden), that the borrow pits are suitable for the production of material.

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- The work will be done on a 6 days/week, $10 \mathrm{~h} / \mathrm{shift}, 2$ shifts/day schedule.

The heavy equipment considered to develop the fill structures estimate are as follow:
Compacted Till zones heavy equipment:

- CAT 325B Backhoe
- CAT D8N Dozer
- CAT 345B Backhoe
- CAT D5 Dozer
- Vibratory compactor CAT 563
- 13-10 wheels dump truck


## Compacted Granular zones heavy equipment:

- CAT 966F
- CAT D5G Dozer
- Vibratory Compactor CAT 563
- 6-10 wheels truck

Compacted rockfill zones heavy equipment

- CAT 992K
- CAT 365B Backhoe
- CAT D8N Dozer
- 4 CAT 775F Dump Truck
- CAT 325B Backhoe

Riprap zones heavy equipment:

- CAT 365B Backhoe
- 2 CAT 775F Dump Truck

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## Dumped Rockfill zones heavy equipment:

- CAT 992 K
- CAT 365B Backhoe
- 2 CAT D8N Dozer
- 4 CAT 775F Dump Truck
- CAT 325B Backhoe


## Boulders zones heavy equipment:

- CAT 992K
- 3 CAT 365B Backhoe
- CAT D8N Dozer
- 4 CAT 775F Dump truck


### 2.2.3.3 Price Factors

- Labour rates considered for this portion of the estimate is as provided by Nalcor.
- Equipment rates are a mix of Equipment watch rates with some specialized equipment having been adjusted to reflect actual rates of similar projects with comparable site conditions.


### 2.2.3.4 Performance Factors

- Load, haul and placing compacted till production rate $=170 \mathrm{~m}^{3} / \mathrm{h}$
- Load, haul and placing compacted granular production rate $=170 \mathrm{~m}^{3} / \mathrm{h}$
- Load, haul and placing compacted rockfill production rate $=250 \mathrm{~m}^{3} / \mathrm{h}$
- Load, haul and placing riprap production rate $=125 \mathrm{~m}^{3} / \mathrm{h}$
- Load, haul and placing dumped rockfill production rate $=250 \mathrm{~m}^{3} / \mathrm{h}$
- Load, haul and placing boulders production rate $=200 \mathrm{~m}^{3} / \mathrm{h}$

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- Load, haul and placing dumped granular production rate $=170 \mathrm{~m}^{3} / \mathrm{h}$


### 2.2.4 North Spur stabilization work

### 2.2.4.1 Scope Factors

The scope of work considered in the CCE was developed by the engineering group who provided bill of quantities to estimators. Quantities were validated by estimators through an independent take-off exercise which revealed minimal differences. The quantities provided by the engineering group were used to develop the North Spur Stabilization estimate and are as follow:

- Overburden Excavation: 368242 m ${ }^{3}$
- Overburden Excavation (2F Material): 228638 m $^{3}$
- Till Blanket - Zone 1 North Shore deposit : $171094 \mathrm{~m}^{3}$
- Granular Material - Zone 2A: $123462 \mathrm{~m}^{3}$
- Granular Material - Zone 2C: $63513 \mathrm{~m}^{3}$
- Compacted Granular material - Zone 2F: 228638 m $^{3}$
- Dumped Rockfill - Zone 3: $71410 \mathrm{~m}^{3}$
- Compacted Rockfill - Zone 3A: 14222 m
- Compacted Rockfill - Zone 3A South Shore excavation: 14222 m³
- Compacted Rockfill - Zone 3B: 57450 m $^{3}$
- Compacted Rockfill - Zone 3B South Shore excavation: $57450 \mathrm{~m}^{3}$
- Compacted Rockfill - Zone 3C: $58115 \mathrm{~m}^{3}$
- Compacted Rockfill - Zone 3C South Shore excavation: 116231 m ${ }^{3}$
- .Riprap - Zone 4 - North Shore quarry: $\mathbf{2 2} \mathbf{2 0 0}$ m $^{3}$
- Zone 5 Material crushed stone max 31.5 mm (permanent road): $8000 \mathrm{~m}^{3}$

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- Compacted Rockfill - Zone 3C South Shore excavation (permanent road): $16000 \mathrm{~m}^{3}$
- Geotextile: $20000 \mathrm{~m}^{2}$
- Geomembrane: $60000 \mathrm{~m}^{2}$
- Slurry Cut-Off wall: $41150 \mathrm{~m}^{2}$


### 2.2.4.2 Construction Methodology and Timeline Factors

Work on cofferdam to be performed before the 2014 flood. Borrowed rock will come from the south once the cofferdam is completed. Work schedule: 6 days/week, 10 h/shift, 2 shifts/day.

### 2.2.4.3 Price Factors

- Labor rates considered for this portion of the estimate are as provided by Nalcor.
- Equipment rates Equipment rates are a mix of Equipment watch rates with some specialized equipment having been adjusted to reflect actual rates of similar projects with comparable site conditions.


### 2.2.4.4 Performance Factors

- Overburden excavation estimated production rate: $100 \mathrm{~m}^{3} / \mathrm{h}$
- Placing compacted materials estimated production rate: $100 \mathrm{~m}^{3} / \mathrm{h}$
- Placing dumped Rockfill materials estimated production rate: $150 \mathrm{~m}^{3} / \mathrm{h}$
- Geotextile and geomembrane installation rate: $250 \mathrm{~m}^{2} / \mathrm{h}$


### 2.2.5 Roller Compacted Structures

### 2.2.5.1 Scope

The scope of work considered in the CCE was developed by the engineering group who provided bill of quantities to estimators. Quantities were validated by estimators through an independent take-off exercise which revealed minimal differences. The

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quantities provided by the engineering group were used to develop the RCC structures estimate and are as follow:

## North Dam

- RCC volume: $188750 \mathrm{~m}^{3}$
- Total formwork area: 25000 m 2


## Riverside Cofferdam

- RCC volume: $37000 \mathrm{~m}^{3}$
- Total formwork area: 6600 m 2


### 2.2.5.2 Construction Methodology and Timeline Factors

- RCC lift height $=300 \mathrm{~mm} / \mathrm{lift}$
- RCC will be pour by conveyor

Main assumptions are that green cuts will be made when needed by the RCC crew during formwork preparation for the next lift but will be kept to a minimum by the use of a low high paste low water demand ( $60 \%$ fly ash/40\% cement) mix allowing for better maneuverability and a 16 to 20 hour setting time.

- Formwork will be fabricated on site by the formwork crew in sufficient quantities to allow continuous operations by jumping lower form panels.
- All formwork activities estimated on a 6 days/week, $10 \mathrm{~h} /$ day basis.
- RCC activities estimated on a 7days/week, 20h/day basis.
- Foundations ready in 2014, RCC placement will begin in spring 2015


## Formwork crews:

- 1 Foreman

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- 3 Carpenters
- 3 Laborers
- 1 Welder
- RCC crew:
- 3 Heavy equipment operators
- 1 Backhoe operator
- 1 Dozer operator
- 6 Concrete laborers
- 1 Foreman
- 1 Concrete conveyor operator
- 10 Highway truck operator


## RCC heavy equipment:

- CAT 315 DL Backhoe
- CAT D5 Dozer
- CAT D4 Dozer
- CAT 950 H
- Vibratory compactor CAT cs 533E
- Boom truck with boom conveyor 100'
- 10-10 wheels dump truck
- 2 - twin shaft paddle batch mixer


## North Dam

- Total duration of 90 workdays (3,5 months).
- A total of 60 upstream formwork panels will be needed.

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- Upstream formwork panels will be used up to 8 times.
- A total of 155 downstream formwork panels will be needed.
- A total of 108 RCC lifts of 300 mm high will be made.


## Riverside Cofferdam

- Total duration of 52 workdays ( 2 months).
- A total of 54 formwork panels will be needed.
- Formwork panels will be used up to 7 times.
- A total of 56 RCC lifts of 300 mm high will be made.


## Price Factors

- Labor rates considered for this portion of the estimate is as provided by Nalcor.
- Equipment rates are a mix of Equipment watch rates with some specialized equipment having been adjusted to reflect actual rates of similar projects with comparable site conditions.


### 2.2.5.3 Performances Factors

- Formwork fabrication rate $=4 \mathrm{~m} 2 / \mathrm{h}$
- Formwork installation rate $=6.30 \mathrm{~m} 2 / \mathrm{h}$
- RCC average production/hauling/placing $=148 \mathrm{m3} / \mathrm{h}$
- 2.5 km from concrete batch plant to RCC dam/cofferdam.


### 2.2.6 Structural Concrete Structures

Direct costs were determined by a "bottom-up" contractor-style estimate, starting with detailed quantity takeoffs for each structural concrete element. Takeoff quantities were reconciled with BOQ values prior to the Nov 15-18 estimate review meeting later adjusted according to agreed action items identified during review meeting. Crews and productions were assigned to each element of work, and resource

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requirements (e.g. form fabrication quantities) were also determined for each element of work. Crane layouts were sketched to determine required capacities and number of cranes.

Construction indirect costs related to the subject work scope are included in the estimate. Those costs were estimated up to a "Structure Level", so no "Project Level" (e.g. camp, turnaround, right of way, higher level management) costs are included. In other words, the construction indirect costs included are sufficient to directly plan and supervise the work in the field only, including contractor's quality control personnel, construction engineering, and surveying. The Construction indirect costs were estimated in four groups so as to be able to rationally distribute them to determine total costs for the main components of work estimated: Spillway; Intake; Powerhouse; and Transition Structures.

Construction Materials were estimated based on cost experience and research, unit rates were established for all construction materials required. In general, all construction material rates were determined by side estimate and input to the estimate by m, m2, or m3 as appropriate. Labour related small tools, supplies, and safety equipment were input by the man-hour (\$4.00) in the Construction indirect costs.

## Included Items:

Supervision - Construction supervision and vehicles; quality control and assurance personnel; surveying; construction engineering. Established indirect wage rates are weighted to account for rotation of personnel.

Temporary Buildings - Office facilities; craft tool rooms/dry shacks; warehouses/shops; stair towers; winter protection enclosures (for Intakes and Powerhouse only). Scaffolding and walkways are included in the direct costs in the various formwork and falsework fabrication items.

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Utilities - Power and water hook-ups; water pumping and transportation; sanitary facilities; phone and internet expenses (for site offices and indirect personnel only).

Support Equipment - Crew pickups/flatbeds; hydraulic cranes; boom trucks; labour related small tools, supplies, and safety equipment ( $\$ 4.00$ for every man-hour, including indirect man-hours).

Administration and Profit - 15\% contractor mark-up on all costs, including indirect costs. No other adders for bond, liability insurances, home office overhead, etc. are included.

## Excluded Items:

Labour Related - No turnaround or rotation transportation (airfare) costs are included in the structural cost estimate as these costs are captured as a Project Indirect Cost detailed in Volume I. No costs for employee training, safety indoctrinations, drug testing, bonuses, or other compensation outside the agreed wage rates are included as these are addressed in the Project Indirect costs. No costs for camp (room and board) or other site services (other than construction office maintenance) are included.

Equipment, Construction Materials, Permanent Materials Related - No exclusions other than it was assumed access roads, equipment pads, yard areas, dewatering, snow removal, signs, barricades, etc. would be provided elsewhere in the estimate. No costs are included for any of these items, other than the costs included in the Construction indirect costs for surface water and snow control inside the structure footprints (only).

Contractor Overheads - Other than the $15 \%$ contractor mark-up on all costs (included in the Construction indirect costs), there are no other overhead or profit allowances. Separate allowances for items such as Bond, General Liability Insurance, Builders Risk Insurance, Home Office Overhead, etc. are not included.

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Subcontractor Mark-ups - The assumption is that all the work is to be selfperformed; hence any additional mark-ups due to subcontracted work are not included. If, for example, the contractor elects to subcontract the furnishing and placement of reinforcing steel on the project, a substantial mark-up would be required by the subcontractor (on approximately $\$ 100 \mathrm{M}$ worth of work).

### 2.2.6.1 Scope

Structural concrete estimate includes the direct and indirect costs for the following structural concrete elements of the project:

- Powerhouse Concrete Cofferdam
- Spillway Concrete Structure
- Spillway Centre Pier for temporary construction bridge
- Intake Concrete Structure
- Powerhouse Substructure
- North Transition Structure
- Centre Transition Structure
- South Transition Structure (estimated as part of the Powerhouse)

Structural concrete estimate includes costs for furnishing, forming, placing, finishing, and curing the structural concrete for the above listed elements. It includes installation of all scaffolding and shoring for concrete as well as furnishing and installing reinforcing steel and waterstops for those elements. It also includes installation only of primary anchors only for gate, stoplog, and trashrack assemblies as well as supply and install of miscellaneous embedded metals.

The structural concrete estimate does not include any other structural concrete elements (e.g. RCC dam facing, temporary structures other than the Spillway Centre

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Pier), structural steel, or grouting. It does not include embedded guides for gate, stoplog, and trashrack assemblies.

The quantities considered were provided to estimating by engineering and are derived from the CATIA model developed for the Project. An independent take-off by estimating revealed no significant differences with quantities provided by engineering.

The major quantities for the concrete estimate are presented in table below:

### 2.2.6.2 Construction Methodology \& Timeline Factors

General considerations and recommendations pertaining to the Schedule:
In the CCE, the basic assumption is that the Intake-Powerhouse-Draft tube structures are to be constructed concurrently along with the Spillway and transition structures all in accordance to the master Project schedule provided to the estimating team. In effect, the sequencing of the work and the volumes of the components to be poured dictate the required monthly production rates.

However, following the above mentioned assumption, the monthly placement volumes obtained using the resulting production rates are quite high. In effect, 16 months are required to pour 284000 m 3 which represent two thirds of the structural concrete for all the structures resulting in an average of 17775 m 3 per month or roughly 585m3 per day every day. Furthermore, in order to achieve this production, it is estimated that the necessary work schedule involves working 2 shifts, 7 days a week. In these conditions there is no float or margin to account for any unexpected events.

Sustaining such a high level of production for such an extended period of time will be quite challenging if not overly optimistic. As the critical path of the Project is generally through the centerline of the turbine/generator units, SLI's recommendation to alleviate the scheduling pressure on the structural concrete operations would be to remove from the critical path a portion of the concrete to be poured. This could be achieved by adding a construction joint upstream and

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downstream of the center portion of the Powerhouse, where the units are housed and pouring the Intake and Draft tube later.

Another way to reduce the required monthly pouring rate would be to extend the schedule to better spread over time the required volumes of concrete to be poured.

In any case, SLI has been instructed by Nalcor, in a meeting held on Friday November 18, 2011 to maintain as they are the current assumptions carried in the CCE.

Cold Weather Concreting - costs are included for heating concrete during winter months (generally $1 / 2$ of each year) as well as a provision for a temporary building enclosure for the Intakes and Powerhouse only at a cost of $\$ 1320 / \mathrm{m}$ 2 (plus heating and lighting costs) for a "substantial" building that would be insulated and structurally capable of supporting gantry cranes for work inside.

Remote Site -long truck hauls were considered necessary for mob/demob as well as the furnishing of all permanent and temporary materials and supplies.

Labour - Labour crafts were assigned by type of work as follow:

- Carpenters for formwork
- Labourers for concrete placing
- Operators for equipment
- Teamsters for trucking
- Cement masons for concrete finishing.

Crew sizes and makeups were established based on the elements of work.

Equipment - Equipment is included in each crew. Cranes, forklifts, generators, compressors, welding machines, concrete pumps, manlifts, etc. are all included in the direct cost of each element of the work. Only pickups and limited support

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equipment such as hydraulic cranes and boom trucks are included in the construction indirect costs.

Concrete Placing - The cost of the work was estimated under the assumption that all concrete would be pumped, and the average pump boom size would be 52 m . There is a good chance that a contractor would place at least some of the concrete by other means, but an overall unit placing cost derived from pumping all concrete with a 52 m pump adequately meets the required precision of this estimate.

Mob \& Demob - Included in the estimate is the employee travel time (not including bus and driver costs) to/from site one-way from camp ( $1 / 2$ hour on top of each 10 hour shift); equipment transportation and setup/down; site facilities setup/down.

### 2.2.6.3 Price Factors

All direct costs, including labour, equipment, construction materials, and permanent materials are included. All work was assumed to be self-performed; no subcontractor costs are included (with the exception of provisions for mob/demob trucking). The potential (likely) added project cost due to mark-ups on subcontracted work could be significant but is not included in the structural concrete estimate.

- Labour rates are agreed "all-in" rates for each craft based on 10 hours a day 7 days a week.
- Equipment rates are agreed "all-in" rates for each equipment resource as stated in Volume I.

Permanent Materials - Unit rates considered are as follows:

- Supply only of Concrete (all) $\$ 235 / \mathrm{m} 3$
- Waterstop (all) $\$ 15 / \mathrm{m}$
- Liquid Expansion Joint Filler $\$ 11 / \mathrm{m} 2$
- Rebar (all, black) $\$ 2.00 / \mathrm{kg}$

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- Concrete material unit cost does not include transportation costs from the batch plant, which was estimated separately and included in the various items of work at a rate of 8 m 3 per hour per truck and driver.


### 2.2.6.4 Performance Factors

Labour Productivity was factored to take into account remoteness, climate, pace of work, large crew sizes, multiple shifts, and long work weeks resulting in labour not being as productive as it could be otherwise. Quantifying reduced productivity is subjective, but $60 \%$ to $80 \%$ of what could be expected under more favourable conditions is a reasonable estimate of what was assumed for hourly labour productivity. More favourable conditions would be: closer to metropolitan area; not as adverse climate conditions; 40 hours per week; single shift; smaller crew size; slower build-up to maximum crew size.

However, prior to CCE close-out, SLI has conducted a further review of the structural concrete component of the Project with respect to, amongst others, the aggressiveness of the concreting schedule, as described in the Construction Methodology \& Timeline Factors section above. As a result of this review and not withstanding Nalcor's directive to maintain unchanged the initial estimate assumptions, SLI has elected to carry in the CCE and additional 200000 labour hours to cover for the inherent loss of labour productivity that will result from the congestion of the concreting work areas and the strain on the supply chain of materials to the worksite..

### 2.2.7 Powerhouse and Spillway Heavy mechanical systems

### 2.2.7.1 Scope factors

The Powerhouse Heavy Mechanical and the Spillway Heavy Mechanical systems have been divided into two packages due to schedule requirements and the need for the spillway to be operational for river diversion two years before the powerhouse is complete.

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The scope of work for the Powerhouse Heavy Mechanical includes the following:

- Twelve intake vertical emergency closure head gates, including embedded guides and wire rope hoists, for reach water passage;
- One set of five bulkhead gate s section for one water passage, including twelve sets of embedded guides, for each water passage, and one lifting beam designed to install and remove the bulkhead gates with a mobile crane;
- Twelve sets of trashracks, including embedded guides, for each water passage;
- Four sets of draft tube stoplogs, two sets per unit, with eight sets of embedded guides, for each water passage;
- One draft tube stoplog handling overhead crane.

The scope of work for the Spillway Heavy Mechanical includes the following:

- five spillway vertical gates, including three vertical surface gates, and two low level outlet gates;
- two set of temporary upstream stoplogs needed for construction which will be modified to one set of permanent upstream stoplogs;
- two sets of temporary downstream stoplogs needed for construction;
- three hoist houses with two wire rope hoists, steel towers and two stairs for the vertical surface gates;
- two hoist houses with two wire rope hoists for the low level outlet gates;
- one monorail hoist for handling the permanent stoplogs;
- eighteen set of vertical embedded guides for the gates and stoplogs.


### 2.2.7.2 Construction methodology and timeline factors

The installation crew for the Powerhouse Heavy Mechanical is estimated at 10 total staff working 13 hour days on a $20 / 8$ rotation for 36 months. The installation crew for

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the Spillway Mechanical is estimated at 10 total staff working 10 hour days on a $20 / 8$ rotation for 28 months.

The Schedule was discussed with the two fabricators who supplied budget prices, and both agreed lead times were acceptable for fabrication and installation

### 2.2.7.3 Price Factors

Direct costs include the design, supply, transportation, installation and commissioning of the above listed packages.

For the direct cost estimate, preliminary design was completed to determine weights of all components, and the costs were estimated from other comparable hydroelectric projects on a cost per kilogram basis. The estimate weights of all mechanical components for the Powerhouse Heavy Mechanical equipment is 7,726 tonnes, and for the Spillway Mechanical equipment is 2,843 tonnes.

Preliminary drawing and a summary specification were produced, and these were provided to three fabricators who were chosen as they had in house design capabilities and these companies were considered experienced in gate design and fabrication, and have participated in similar installations in remote sites similar to Labrador.

Budget prices were received from two of the three fabricators, and these prices were considered as acceptable as they were within $12 \%$ on the total price, so the higher of the two prices were used in the Gate 3 Estimate. On a price per kilogram basis, the budget prices were considered reasonable.

Indirect costs were not included in the estimate, but one fabricator provided a manhour estimate for the installation from which the SLI estimators produced indirect costs for these two packages.

The project should realize a saving if both of these packages are awarded to one contractor, but these two packages cannot be awarded simultaneously as the start times for each project are offset by six to nine months depending on how the packages are finally assembled. The start times will be finalized if the Draft Tube

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Stoplogs and embedded steel is included in the Powerhouse Heavy Mechanical or the Spillway Mechanical packages, and will depend on the final construction sequence for the powerhouse civil contract.

### 2.2.8 Powerhouse Intake Trash Cleaning System

### 2.2.8.1 Scope factors

The Powerhouse Intake Trash Cleaning System was provided in the Gate 3 Estimate, but the requirement for this system is not yet finalized.

The scope of work for the Powerhouse Intake Trash Cleaning System includes the one purpose built trash cleaning system:

- capable of cleaning floating debris in front of the intake;
- capable of cleaning the trashracks; and capable of cleaning debris from the rock; and
- capable of cleaning sediment trap in from of the intake trashracks.

The only system available that has the above three capabilities is a purpose built trash cleaner built in Germany by Muhr and distributed in North America by Lakeside Industries. Construction methodology and timeline factors

### 2.2.8.2 Construction methodology and timeline factors

Installation of this contract would take about six weeks for 8 workers working 10 hour days on a 20/8 rotation, and indirect costs such as accommodation and site transport were included in the direct costs.

### 2.2.8.3 Price Factors

Prices from Muhr were provided for design, fabrication, transportation, installation, and commissioning of the Trash Cleaning System.

Costs for the supply and installation of the rails on the intake deck were included in the Powerhouse General Civil Contract.

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### 2.2.9 Powerhouse Bridge Cranes

### 2.2.9.1 Scope factors

The Powerhouse bridge cranes are required for installation and maintenance of the generating units. The arrangement used is two bridge cranes rated at 380 tonnes with two trolleys on each rated at 190 tonnes. Each of the cranes will be supplied with a lift beam to lift 360 tonnes; and another lift beam to connect both cranes to lift 680 tonnes which is estimated to be the largest single piece for assembly of the generating units.

Cranes weights received from one of the three suppliers was estimated at 212 tonnes each, or 472 tonnes for both cranes with lifting beams.

### 2.2.9.2 Construction methodology and timeline factors

Installation of this contract would take about three weeks with 10 workers working 10 hour days on a $20 / 8$ rotation, and indirect costs such as accommodation and site transport were included in the direct costs.

### 2.2.9.3 Price factors

Prices were received from three crane suppliers for supply, transport, and installation of the cranes including start up, commissioning and load testing. Prices received are within $15 \%$ and considered consistent with industry prices for this equipment.

Costs for the supply and installation of the rails on the powerhouse superstructure steel were included in the Powerhouse General Civil Contract.

### 2.2.10 Powerhouse Elevator

### 2.2.10.1 Scope factors

The powerhouse elevator is a passenger/freight elevator designed for access at seven landings from the drainage sump at EL. 20.2 m up to the Intake deck at El. 45.5 m .

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### 2.2.10.2 Construction methodology and timeline factors

Installation of this contract would take about 20 weeks with two workers working 10 hour days on a $20 / 8$ rotation, and indirect costs such as accommodation and site transport were included in the direct costs.

### 2.2.10.3 Price factors

Budget prices were received from two suppliers, but only one elevator system complied with the specified requirements for the size of the cab and doorway. although higher priced it was carried in the CCE.

Costs for the concrete structure were included in the Powerhouse General Civil Contract.

### 2.2.11 Steel Superstructure and Architecture

### 2.2.11.1 Scope

The scope includes Construction of Steel Structure for Powerhouse Superstructure, 46.965 m width, 198.840 m length and 27.80 m height (from +15.50 m to +43.30 $\mathrm{m})$. It also includes construction of two mezzanine floors at +25.00 and +34.47 m level, made of concrete floor over metal decking. Structural Steel for roof over mezzanine floors and catwalk access is also included as well as the steel columns and beams required to carry the loads of the two heavy overhead cranes in the Powerhouse. The scope also includes Metal access Doors, Ladders, Handrails, Guard Rails, Removable Handrails and Crane rails at Intake Deck.

Extension of the powerhouse structure by 2 bays for construction purpose is considered as an optional item (Option 1) and estimated separately as standalone case.

Use the 2 units of steel superstructure as winter protection shelter is considered as an optional item (Option 2) and estimated separately as standalone case.

In-House pricing was used to estimate the majority of Architectural items and benchmarked with other projects using similar architectural systems as well as

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specialized supplier input. For very few of these items, information from Richardson Cost Data was used. Wherever no information was available, a lump sum provisional amount was provided. The final architectural cost included in the CCE was adjusted to reflect architectural costs encountered in similar projects in comparable conditions.

- Quantities are based on $40 \%$ engineering progress, as of 24 November, 2011. Any changes resulting from development thereafter are excluded.
- Bill of quantities were issued by engineering on a basis of heavy, medium and light profiles for an approximate total of 3200 tonnes.
- Quantities include connection allowance of $10 \%$ and quantity growth allowance of $10 \%$.
- All structural steel is generally painted, except specified otherwise.
- Concrete for mezzanine floor is included in concrete works for powerhouse.
- All miscellaneous embedded steel is included in concrete works for powerhouse.
- No additional allowance needs to be added.
- Any changes resulting from development thereafter like addition of roofs over mezzanine floors are excluded.
- Costs and labour productivity included in the CCE have also been benchmarked with similar projects in comparable conditions.

Miscellaneous exterior steel guardrails (WBS30002100)
The scope includes guardrails along the south RCC dams, the intake, the center dam, the permanent access road and the tailrace deck.

- Foundation of the Guardrails is included in Civil / Concrete works of Powerhouse and is assumed to consist only of drilled holes for expansion anchors.

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- Quantities are neat and do not include any kind of allowance what so ever.


### 2.2.11.2 Construction Methodology \& Timeline Factors

Construction will be carried out by multiple sub-contractors to the prime EPCM which will be chosen to perform the work under a competitive bidding process.

Sub-contractor will be given responsibility for the supply, construct, manage, perform and deliver the following on site construction activities in general:

- Craft Labour, Discipline foremen and for all construction / installation activities;
- Construction Equipment for all construction / installation activities;
- Permanent materials and associated bulks;
- Small tools, consumables and supplies;
- Scaffolding;
- Construction supervision and management;
- Temporary facilities \& offices and expenses;
- Personnel transportation;
- Mob / Demob of Personnel, Equipment and all facilities
- Construction Equipment requirements have been identified on an as needed basis for individual crews;
- An average of $\$ 8.00$ per Direct Labour Hour has been considered. On average the following breakdown applies;
- Small Tools 4-5 \% of DFL Cost.
- Consumables 3-4 \% of DFL Cost.
- PPE 2-3 \% of DFL Cost.

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Any kind of pre-assembly / dry assembly at site is not envisaged. All structural steel components are stick built for erection purpose. Roof truss is assembled at shop and delivered in two parts.

Duration based on schedule PCS - Oct 6.pdf supplied by the Project Controls group.

### 2.2.11.3 Price Factors

Budgetary Offers from fabricators were invited for supply, fabricate (including shop drawing), paint and delivery at site of structural steel components. Offers were received from OCEAN STEEL of New Brunswick, SUPER METAL of Quebec and DAERONG of South Korea. Detailed bid evaluation was not carried out and it is assumed the bids are within the acceptable limits of exclusions. An average price of all three bids is considered for present estimation.

- All direct labour hours for Civil / Concrete / Steel are based on readily available USGC (United States Gulf Coast) charts and/or SLI historical data.
- Construction Equipment rates are based on blue book hourly rates provided with the Estimate Ground Rules- September 12th 2011; and is inclusive of Fuel, Lubricants and Periodic routine maintenance but excludes operating personnel.


### 2.2.11.4 Performance Factors

- All direct labour hours based on readily available published charts and/or SLI historical data.
- All base hours based on USGC.
- A site-specific adjustment factor 1.25 for Structural Steel by prime account was applied to the chart hours.
- Factors that were considered for site conditioning include; Work week, Project Size, Plant Type, Work Space per Man, \& Climate.
- Factors not considered for site conditioning include; Craft Availability, Craft Skill, Quality of Craft Supervision, \& Union Influence.

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### 2.2.12 Power Generation

A complete bid package has been issued to Alstom, Andritz and Voith on October 14, 2011 with expected return date of quotation of January 27, 2012. The scope of the work includes the supply, installation testing and commissioning of four (4) 206 MW Kaplan units including the following for each unit:

- Turbine
- 229 MVA Generator
- Governor
- Static excitation system

As the actual quoted cost was not available at the time of the CCE, a provision based on similar projects in comparable conditions was included. In order to meet Project schedule, it is most critical that the Power Generation Contract be awarded in early spring of 2012

### 2.2.13 Auxiliary Mechanical Works

### 2.2.13.1 Scope

The Mechanical Equipment Bill of Quantities received from project engineering is the basis for the scope of the Mechanical Equipment estimate and cover the following Powerhouse systems:

- Raw and cooling water system
- Fire protection system
- Service water system
- Shaft seal water system
- Dewatering system
- Drainage system

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- Oily water drainage system
- Domestic water and Wastewater systems exclusive of appliances carried in architecture estimate
- High and low pressure compressed air systems
- Lubricating and hydraulic oil handling system
- Piezometer and water level system
- Powerhouse HVAC as well air fans in inspection gallery of main RCC dam
- Instrumentation and related piping systems
- Miscellaneous small hoist and handling systems
- Machine shop equipment

Mechanical Engineering Group also added a number of control panels required into $B O Q$ to facilitate the electrical needs for the mechanical equipment material and labour cost calculation.

- Individual datasheets with applicable Codes and NALCOR standards to solicit the Vendor Bids for individual equipment were not received.
- Portable pumps assumed to be un-crated and stored in warehouse. No additional hours for permanent installation.
- Pre-commissioning spares have not been considered.
- Cost of Vendor Representatives has been excluded.
- No Material Take off Allowance was added.
- No Design Development Allowance was added.


## HVAC:

HVAC BOQ received from project engineering department is the basis of mechanical HVAC account. Mechanical Engineering Group also added number

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of control panels required into BOQ to facilitate the electrical needs for the mechanical equipment material and labour cost calculation.

- Individual datasheets with applicable Codes and NALCOR standards to solicit the Vendor Bids for individual equipment were not received.
- Take off is measured through fittings.
- HVAC duct estimated by hrs per lb. Assumed fitting mix is $20-30 \%$ of weight.
- $20 \%$ waste included in weight.
- Pre-commissioning: spares have not been considered.
- Cost of Vendor Representatives has been excluded.
- No Material Take off Allowance was added.
- No Design Development Allowance was added.


## Piping:

- The BOQ has been verified by engineering against the P\&ID's.
- BOQ includes all large bore, small bore piping and valves.
- Assumed local fabrication of piping spools.
- Pipe Insulation requirements were indicated on the insulation specifications.
- Pipe Paint requirements were indicated on the painting specifications.
- The piping layout is based on the 3D model.
- High point vents and low point drains captured on BOQ were developed by estimating, one vent or drain for every 150 LM of large bore piping.
- Assumed 5-10\% of welds require NDE testing.
- Assumed $30 \%$ of welds on site and $70 \%$ shop welds where shop rates were estimated through contacting east coast suppliers

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- Additional man-hours included for hydro testing and air blowing.
- Additional hours for material handling (prorated on LM of pipe).
- No Material Take Off allowance was added.
- No Design Development allowance was added.
- An allowance for Standard Pipe supports has been included. This includes man-hours as well as material cost.
- All BOQ quantities are "neat"
- No allowances were considered by engineering.


## Instrumentation:

Instrumentation cable \& bulks for the Auxiliary Mechanical Package were defined by estimation. An allowance including man-hours and material cost has been included in the estimate.

- Instrumentation items for the Auxiliary Mechanical Package have been defined by SNC engineering. No additional instrumentation items have been added by estimating.


## Insulation:

- Piping systems requiring insulation have been identified in the project Insulation specifications.
- Insulation quantities have been calculated based on pipe and fitting length using the Denis formula.


## Electrical:

- Electrical bulks for the Auxiliary Mechanical Package were defined by estimation.

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- Electrical control panels for the Auxiliary Mechanical Package have been defined by SNC engineering. Control Panel assumed to have 50 LM Control Cable, 50 LM Power Cable, 25 LM Conduit \& 12.5 LM of Tray.
- An allowance for cable, conduit, \& tray for the Auxiliary Mechanical Package has been included. This includes man-hours as well as material cost.


## Paint:

- Piping systems requiring painting have been identified in the project paint specifications provided by engineering.
- An allowance for paint material and labour has been included based upon system requirements as well as field touch-ups after welding

Also, the Mechanical Equipment Bill of Quantities received from project engineering is the basis for the scope of the Mechanical Equipment estimate and cover the following North Spur systems:

- Refurbish existing pump wells including pump removal, inspection, cleaning and reconnection.


### 2.2.13.2 Construction Methodology \& Timeline Factors

As a result of mechanical construction sequence prior and after installation of Power generation units, the estimate considers a 6 month period where little or no mechanical work is performed which extends the duration for which the temporary contractor installations would be required. For the calculation of the construction indirect costs it was assumed that two packages would be included in one contract.

Mechanical work was assumed to be performed using shared supervision of multiple crews as well as shared service and access equipment.

Scaffolding was estimated by applying an allowance of $17 \%$ of direct labour costs and 2500 of labour hours

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### 2.2.13.3 Price Factors

Detailed Technical bid evaluation (TBE) was not carried out for budget quotes; it is assumed the bids were within the acceptable limits of exclusions.

- All Items were sent for budget pricing through the SNC Procurement group.
- Mechanical and Piping packages were sent to multiple Vendors. When vendor response was limited In house pricing was used to estimate the remaining items.
- Those items that did not receive a budget quote were priced in house using data from similar major projects from the last eighteen months.
- Supply of piping and fittings, valves, accessories have been quoted by vendor or in house priced
- Shop Fabrication of spools pricing is based on multiple offers from East Coast Fabricators.
- HVAC equipment has been quoted by vendor or in house.
- Major Equipment has been quoted by vendor or in house.
- Electrical equipment for power and control of Aux Mechanical package was priced in house.
- Instrument cable for Aux Mechanical package was priced in house.
- Instrument hardware for Aux Mechanical package was vendor quoted.
- Insulation material has been quoted in house.
- An allowance for Standard Pipe supports has been included. This includes man-hours as well as material cost.

Budget quotes were obtained from suppliers for (or part of) the following systems:

- Mechanical system and equipment
- Piping bulks.

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- Fire protection items.
- Sand filter.
- Mobile oil purifying unit.
- Oil storage tank
- Oil Water Separator
- Fans, diffusers, coils
- Shop Fabrication

Freight
In-house prices were carried for:

- Construction materials, mechanical equipment, electrical equipment and instruments not mentioned above and for which, generally, an $8 \%$ allowance was carried for freight.


### 2.2.13.4 Performance Factors

Labour productivity assumptions are as follow:

- All direct labour hours are based on readily available USGC (United States Gulf Coast) charts and/or SLI historical data.
- The following productivity factors were added to the chart to account for the location of the Project:
- 1.13 for Mechanical and HVAC systems man hours.
- $\mathbf{1 . 5 5}$ for Piping / Insulation systems man hours.
- A 6\% allowance was added to direct labour costs to account for congestion of the worksite

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### 2.2.14 Auxiliary Electrical Works

### 2.2.14.1 Scope

The Auxiliary Electrical work estimate includes the direct and construction indirect costs for the following elements of the project:

- Spillway Electrical Works
- North Spur pumping system upgrade Electrical Works
- RCC inspection gallery Electrical Works
- Building Electrical Services
- Electrical Ancillary / Auxiliary Systems
- Powerhouse Grounding Works
- Protection, Control and Monitoring
- Generator Transformers (4 working and 1 standby)
- Emergency Diesel generator
- Spare Parts and Special Tools
- Operations Telecommunication System - Muskrat Fall

All material take-off quantities were developed based on the single-line-diagram and drawings prepared by engineering. Cable lengths were estimated by evaluating horizontal and vertical runs throughout the Powerhouse along with the cable tray layout drawings.

Quantities are neat from engineering and no quantity allowance is considered at this stage of estimate.

This applies to the following WBS BOQ's:

- Powerhouse Station AC/DC Electrical Auxiliaries
- Generator Step-up (GSU) Transformers

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- Generator Circuit Breakers
- Station Auxiliary Service Transformers
- Isolated Phase Bus
- MF Power Station BOQ Telecom, CCTV, PA, SACS, TELEPHONY
- MF Spillway BOQ Telecom, CCTV, PA, SACS, TELEPHONY

For the HV Power Transformers elements of the Electrical Works, an estimate validation check for Labour hours was performed using the Aspen Capital Cost Estimator estimating software.

### 2.2.14.2 Construction Methodology \& Timeline Factors

No heavy lifting equipment has been considered as it is assumed all heavy permanent equipment such as the generator transformers are directly off loaded onto foundation by others.

As the duration of the Electrical Works for the Powerhouse and area considered in the CCE extends from mid 2014 to 2016, the construction indirect costs are calculated accordingly. The contracting packaging strategy to be developed with respect to Electrical Works could alleviate these costs be optimizing and possibly decreasing the overall duration of the electrical contractors need to be on site.

## Scaffolding and accesses

- A provision of $5 \%$ of total direct Labour hours for Scaffolding labour and $3 \%$ of total direct Labour cost for scaffolding materials cost are included in the estimate.

Construction equipment

- Diesel Generators are used to provide requisite electrical supply to construction works

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- Lifting and carrying equipment like forklifts, small cranes, pickup trucks, welding machines, etc are estimated to be mobilized for the construction duration as required

Congestion of work site

- A small percentage of $4-5 \%$ idle time is assumed to account for site congestion
- Its assumed the work front from other disciplines will be available as per schedule


### 2.2.14.3 Price Factors

- Majority of Items were sent for budget pricing through the project Procurement group.
- For some of the high value items average costs of two higher quotes are considered.
- Those items that did not receive a budget quote were priced in house using data from similar major projects from the last eighteen months.
- DC portion of cost will be provided by engineering discipline as a Sub Contract all inclusive cost.
- Telecommunication portion of cost will be provided by engineering discipline as a Sub Contract all inclusive cost.
- For the accessories which were not quantified by engineering an allowance was used.


## Freight

In-house prices were carried for:

- Construction materials.
- Mechanical equipment, electrical equipment and instruments.

Generally an $8 \%$ allowance was carried for freight.

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### 2.2.14.4 Performance Factors

Labour productivity assumptions are as follow:

- All direct labour hours are based on readily available USGC (United States Gulf Coast) charts and/or SLI historical data.
- A productivity factor of 1.44 over Richardson was added to the chart to account for the location of the Project
- A 6\% allowance was added to direct labour costs to account for congestion of the worksite

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## 3

## 3.1

## INTRODUCTION

As described in Volume I, the Project's Component 3 includes the facilities, installations and equipments relative to the Churchill Falls, Muskrat Falls and Soldier's Pond Switchyards, the Muskrat Falls Tap, the Muskrat Falls and Soldier's Pond AC/DC Converters, the SOBI Transition Compounds and Pond Electrodes, the Soldier's Pond Synchronous Condenser and the Telecommunication System.

The following sections describe the basic assumptions considered as well as the means and methods utilized to develop the relevant cost estimates included in the CCE.

### 3.2 BASIS OF ESTIMATE - DIRECT COSTS

The following general assumptions were considered for estimating the above mentioned work items of Component 3.

For each of the sites, engineering was developed to provide sufficiently detail material take off quantities for the CCE. Approximately 130 drawings were issued including site layouts and line diagrams.

Approximately 25 short-term specifications were issued by Engineering and provided to Procurement for the costing of the major equipments.

### 3.2.1 Scope Factors

The scope of work includes, for each of the sites, all clearing and grubbing, cut \& fill for site grading, fencing, slope protection, access roads, cable trenches and duct banks, concrete foundations, galvanized steel gantries and supports, pre engineered buildings, Supply and Installation of all electrical equipment, auxiliary building mechanical works as well as mechanical handling equipment and operation and maintenance shops where required.

- Quantities are based on $40 \%$ engineering progress, as of 5 December, 2011.

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- Quantities are neat and do not include any kind of allowance what so ever.
- The preliminary civil/structural design is based on the National Building Code of Canada.
- In the absence of geotechnical information, shallow footing with allowable soil bearing capacity of 150 kPa and a frost depth of 2.40 meters is considered for all the foundations.
- Site grading design is based on balanced cut and fill with site specific assumptions for overburden / rock ratios
- Piling for foundations not envisaged.
- Civil works related to Cathodic Protection are excluded.
- Requirement of fire protection of the power transformers at the Churchill Falls and Muskrat Falls Tap have been excluded following consultation with Nalcor.
- For miscellaneous works where quantities were not available estimating has assumed a quantity


### 3.2.1.1 Civil Works

All the site locations are considered as green field locations and any kind of demolitions are not envisaged with the exception of the existing Churchill Falls 230/138 kV switchyard and the existing 138/25kV Construction Power installations at Muskrat Falls 315/138 kV switchyard. All civil works are considered to be performed during summer and no provision has been added for winter works.

- Access roads / approach roads are included.
- Ditches/Swales along periphery of the plot are considered as un-lined ditches and are part of site grading activities. No additional quantities are considered.
- Buried Cable Trenches are not envisaged. Precast Polymer Concrete cable trenches are considered.

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- Excavation in rock is considered at some of the location as per information available at this point in time and agreed assumptions as to the presence of rock are carried in the CCE.


### 3.2.1.2 Concrete

- Manholes / Cable Pull Pits are not envisaged at this time. If required to be placed outside the control buildings and between cable run, shall be included at a later date.
- Transformer blast/fire wall is considered in the BOQ.


### 3.2.1.3 Steel

- All Steel structures like Gantries and Support steel are considered as galvanized, unless specified otherwise.


### 3.2.1.4 Buildings

- All buildings are considered as Pre-Engineered Buildings.
- Civil / Concrete works up to grade are part of Civil/Concrete BOQ.
- Building wall acting as Firewall, if required is under concrete BOQ.
- Building includes electromechanical works like HVAC, Plumbing, and Lighting etc.
- Over Head Cranes, Handling equipment, Shop equipments etc are quantified and included in estimate.
- Building Includes Furniture, Furnishings and Kitchen / Washroom fittings / appliances.
- Tie in points for Potable Water, Sanitary Drainage, Lighting are considered available near building.


### 3.2.1.5 Electrical Works

- All required supply and installation of electrical equipment including:

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- Circuit breakers
- Disconnect switches
- Capacitor voltage transformers
- Current transformers
- Surge arresters
- Power transformers
- Batteries and chargers
- Busbars and overheard connections
- Grounding
- Control system (panels)
- Lighting and building electrical services
- Operations Telecommunication System - Island Link
- Tie in for Small Power for Lighting etc are considered available near building.
- Cathodic Protection works are not included.


### 3.2.2 Construction Methodology \& Timeline Factor

Standard construction methods have been considered for of each of the facilities and installations of Component 3. Productivity factors by discipline have been applied as indicated in the Performance factors section below.

Where the remoteness of the site requires the provision of a camp to lodge workers and staff during construction, an estimate has been included in the CCE. The sites where such camps are required are indicated in the site-specific considerations below.

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### 3.2.3 Price factors

- Following the issuance of a short-term specification, two turn-key budget quotes were received for the Synchronous Condenser from the following suppliers:
- Alstom for a 3 unit +150/-100 MVAr
- Toshiba for a 2 unit $\mathbf{+ 3 0 0} /-200$ MVAr

For the purpose of the CCE, the Alstom budget quote was considered.

- Following the issuance of a short-term specification, three turn-key budget quotes were received for the Muskrat Falls and Soldiers Pond Converter stations from the following suppliers:
- ABB
- Siemens
- Alstom

For the purpose of the CCE, the ABB budget quote was considered.

- Following the issuance of a short-term specification, three (3) turn-key budget quotes were received for the Shoal Cove and Forteau Point Transition Compounds from the following suppliers:
- ABB
- Siemens
- Alstom

For the purpose of the CCE, the ABB budget quote was considered.

- Pre-engineered building were estimated on a unit cost per area basis in using the following assumptions:
- 1 level standards height: $\quad 1,800 \$ / \mathrm{m}^{2}$

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- 1 level "tall" building :
- 2 levels standard building:
- Foundation works for all buildings
$2,000 \$ / \mathrm{m}^{2}$
$2,700 \$ / \mathrm{m}^{2}$
$600 \$ / \mathrm{m}^{2}$
- All other standards electrical equipment were priced through issuance of short-form technical specifications for the purpose of obtaining budget prices from suppliers. Generally, and where applicable, the average of two highest submitted prices were considered. Where not applicable an estimator judgement call was applied based on past experience.
- For site Testing, Commissioning and Training work of substation electrical equipment approximately $12 \%$ of total material costs is assumed.


### 3.2.4 Performance Factors

Labour productivity assumptions are as follow:

- All direct labour hours are based on readily available USGC (United States Gulf Coast) charts and/or SLI historical data.
- For civil works, productivity factor of 1.31 over Richardson was added to the chart to account for the location of the Project
- For electrical works, productivity factor of 1.44 over Richardson was added to the chart to account for the location of the Project
- For mechanical Works, productivity factors over Richardson were added to the chart to account for the location of the Project:
- 1.13 for Mechanical and HVAC systems man hours.
- $\mathbf{1 . 5 5}$ for Piping / Insulation systems man hours.
- A 6\% allowance was added to direct labour costs to account for congestion of the worksite

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### 3.3 SITE-SPECIFIC CONSIDERATIONS

For each of the Component 3 facilities and installations, some site-specific assumptions were made to adequately capture costs that relate to conditions that apply to these sites only. These site-specific considerations are indicated in the following sections.

### 3.3.1 New Churchill Falls Switchyard 735/315Kv

The remoteness of this site will require the construction of a 150 person camp for the 46 months duration of this portion of the Project. Two (2) new 735 kV interconnections lines will need to be built from the existing CFLCO switchyard to feed the new Churchill Falls switchyard. Some work will need to be performed within the existing CFLCO switchyard and it is assumed that all required permits and authorizations will have been secured by Nalcor at commencement of the Works.

### 3.3.1.1 Site Preparation and Access

Minimal access roads are required for this site as it next to the existing Trans Labrador Highway. Clearing and soil stripping works are included in the CCE.

### 3.3.1.2 Civil Works

As no geotechnical information was available for this site an agreed assumption of balanced cut and fill mass excavation work, comprising 50\% overburden and 50\% rock was considered in the CCE.

The switchyard area of the 735 kV portion of the switchyard is $300 \mathrm{~m} \times 246 \mathrm{~m}$. The area of the 315 kV portion of the switchyard is $192 \mathrm{~m} \times 175 \mathrm{~m}$. In order to reduce the earthworks it is considered in the CCE that the 735 kV portion of the switchyard will be at a level 3 m higher than the 315 kV portion.

All earthworks including final grade using crushed stone as well as fencing around the full extents of the switchyard are included in the CCE including the oil containment and fire wall structure around the power transformers.

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All concrete foundations work for circuit breakers, disconnect switches, capacitor voltage transformers, current transformers, surge arresters, power transformer, gantries, etc. are included in the CCE.

### 3.3.1.3 Electrical Equipment

No backup 735/230kV transformer is included in the estimate as this option was not retained.

### 3.3.1.4 Other Works

An 11m x 30m meter pre-engineered type maintenance and operations building complete with a 5 tonnes overhead crane and all tools and equipment are included in the CCE. There are no provisions for cabinets, tool chests or heavy shelving.

A control building housing 44 control panels, batteries, chargers is also included.

### 3.3.2 Construction Power

The supply of Construction Power to the Project will be provided by a new 138/25kV terminal station at Muskrat Falls with a tap to the existing 138kV transmission line between Churchill Falls-Happy Valley substations. This tap station will be located on the North side of the Churchill River with access from Trans Labrador highway. The construction power will be extended to the construction site and camp site through a 25 kV transmission line approximately 17 km long crossing the Churchill River to the south side.

The new tap substation at Muskrat Falls and an extension by third transformer at Churchill Falls substation is required as supporting infrastructure for the construction of the Muskrat Falls power generation and the camp facilities.

### 3.3.2.1 Site Preparation and Access

Minimal access roads are required at this site as it is next to an existing road

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### 3.3.2.2 Civil Works

The area of the Muskrat Falls construction power substation is $100 \mathrm{~m} \times 100 \mathrm{~m}$. All earthworks including final grade using crushed stone as well as fencing around the full extents of the substation are included in the CCE.

All concrete foundations work for circuit breakers, disconnect switches, capacitor voltage transformers, current transformers, surge arresters, power transformer, gantry, etc. are included in the CCE.

A provision for the demolition of the temporary Muskrat Falls Construction Power substation following completion of the works is included in the CCE.

### 3.3.2.3 Electrical Equipment

Supply and Installation of all electrical equipment required for Construction Power have been estimated using budget quotes provided by suppliers and in-house estimating.

### 3.3.2.4 Other Works

A 17 km wood pole 25 kV transmission line will connect the new tap substation to the Muskrat Falls powerhouse construction site and the camp site. A provision of 100 $000 \$$ per km was made for the construction of the power line

### 3.3.3 Muskrat Falls TAP 315/138kV

This substation will be fed by two new 315 kV lines from Churchill Falls and will supply Happy Valley at 138 kV .

### 3.3.3.1 Site Preparation and Access

Minimal access roads are required at this site as it is next to an existing road

### 3.3.3.2 Civil Works

The area of the Muskrat Falls TAP $315 / 138 \mathrm{kV}$ is $175 \mathrm{~m} \times 275 \mathrm{~m}$. As no geotechnical information was available for this site an agreed assumption of balanced cut and fill mass excavation work, comprising 100\% overburden was considered in the CCE.

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All earthworks including final grade using crushed stone as well as fencing around the full extents of the switchyard are included in the CCE including the oil containment and fire wall structure around the power transformers.

All concrete foundations work for circuit breakers, disconnect switches, capacitor voltage transformers, current transformers, surge arresters, power transformer, gantry, etc. are included in the CCE.

### 3.3.3.3 Other Works

A control building housing 42 control panels, a telecommunications room, batteries, and chargers is also included in the CCE.

### 3.3.4 Muskrat Falls Switchyard 315kV and Converter Station 350kV DC

As this site is located next to the Muskrat Falls Main Camp facilities, it is assumed in the CCE that all workers and staff for this portion of the Project will be lodged at this Camp. For the 34 months duration of the construction work at this site it is expected that accommodations for a peak of 276 workers will be required.

### 3.3.4.1 Site Preparation and Access

Minimal access roads are required at this site as it is next to an existing road

### 3.3.4.2 Civil Works

The extents of the Muskrat Switchyard area are $187 \mathrm{~m} \times 252 \mathrm{~m}$. No rock excavation is anticipated at this site as the area will consist mainly of fill laid down in 2013 during the Powerhouse mass excavation activities and used as a lay down area until the substation work begins.

All earthworks including final grade using crushed stone as well as fencing around the full extents of the switchyard are included in the CCE including the oil containment and fire wall structure around the power transformers.

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## 315kV Switchyard

All concrete foundations work for circuit breakers, disconnect switches, capacitor voltage transformers, current transformers, surge arresters, gantries, etc. are included in the CCE.

A control building housing 60 control panels, batteries, chargers is also included.

## Converter 350 Kv DC

All concrete foundations work for circuit breakers, disconnect switches, capacitor voltage transformers, current transformers, power transformers, surge arresters, filters, gantries, etc. are included in the CCE.

For the valves control building, typical engineering referenced with similar projects was performed. A provision of $2,700 \$+600 \$ / \mathrm{m} 2$ was considered in the CCE.

### 3.3.4.3 Electrical Equipment

## Switchyard

All standard electrical equipment was priced through issuance of short-form technical specifications for the purpose of obtaining budget prices from suppliers. Generally, and where applicable, the average of two highest submitted prices were considered. Where not applicable an estimator judgement call was applied based on past experience.

## Converter 350 Kv DC

For the converter's specialized electrical equipment a short-form technical specifications was issued for the purpose of obtaining budget prices from suppliers. This specification stated that Supply of equipment needed to include the design, manufacturing, quality control, transportation to site, storage and documentation. The supply is to include all equipment and materiel, required to provide a complete and operational converter station. The main equipments included in the Converters station are as follow:

- Thyristor valves and valve cooling system

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- Converter transformer
- Smoothing reactors
- Surge arresters
- AC filters
- DC filters
- Measuring devices
- Control and protection system
- DC switching Device
- AC breakers and switching devices
- Busworks and insulators
- AC/DC station auxiliary power supply
- Smoke detectors in valve hall
- CCTV (camera system)
- Steel structures


### 3.3.4.4 Other Works

An $20 \mathrm{~m} \times 50 \mathrm{~m}$ meter pre-engineered type maintenance and operations building complete with a 5 tonnes overhead crane and all tools and equipment are included in the CCE. There are no provisions for cabinets, tool chests or heavy shelving.

### 3.3.5 Forteau Point and Shoal Cove Transition Compounds

The remoteness of these sites will require the construction of 80 person camps at each location for the 28 months duration of these portions of the Project, the cost of these camps are included in the CCE. However, as these facilities are located in the Transmission Line ROW, there could be an opportunity to save the mobilization and demobilization costs of the Transition Compound camp facilities, mainly the Forteau camp, if the personnel required for this work

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could be lodged at the camp required for the construction of the Transmission lines. The CCE currently carries distinct camp facilities.

The transition compounds are required to interface the submarine/land cable terminated at both transitions compounds through air-bushing cable sealing ends and the DC transmission lines. However, the CCE includes no provision whatsoever for any interface with the SOBI Directional Drilling Contractor at these locations.

### 3.3.5.1 Site Preparation and Access

Access roads to both these sites are included in the CCE.

### 3.3.5.2 Civil Works

The extents of the Transition compounds area are $100 \mathrm{~m} \times 100 \mathrm{~m}$. As no geotechnical information was available for this site an agreed assumption of balanced cut and fill mass excavation work, comprising $100 \%$ overburden was considered in the CCE.

All earthworks including final grade using crushed stone as well as fencing around the full extents of the switchyard are included in the CCE including the oil containment and fire wall structure around the power transformers.

All concrete foundations work for circuit breakers, disconnect switches, capacitor voltage transformers, current transformers, surge arresters, transformer, gantries, etc. are included in the CCE.

A $14 \mathrm{~m} \times 24 \mathrm{~m}$ control building is also included in the CCE housing the control equipment provided by the Turnkey contractor.

### 3.3.5.3 Electrical Equipment

The transition compounds will be provided with all required switching equipment, including:

- 350 KV dc switchyard including all necessary disconnecting and ground switches, surge arresters, post isolator, bushings, voltages dividers, DC current transducers and busworks
- Gantries and steel structures for supporting the equipment on its foundations

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- Auxiliary power supply: one 14.4 Kv transformer and one 150 KW diesel generator
- LV and telecommunication
- Control and protection equipment
- Electrode line monitoring equipment


### 3.3.5.4 Other Works

In order to protect the Transition Compounds' electrical equipment from the salt spray inherent to their location near the SOBI, a $28 \mathrm{~m} \times 43,2 \mathrm{~m} \times 13,5 \mathrm{~m}$ high preengineered building is included in the CCE for each site. These building will consist mainly in a steel shell to house the cable sealing end, circuit breakers, surge arresters, current transformers, disconnect switches, etc. Main access doors will enable service vehicles to access the building and proceed to any assembly or maintenance work from within the building.

### 3.3.6 Soldier Pond Converter Station 350kV, Switchyard 230kV and DC Synchronous Condensers

### 3.3.6.1 Site Preparation and Access

An access road connecting the site to the Trans-Canada Highway is included in the CCE.

### 3.3.6.2 Civil Works

The extents of the Soldier Pond Switchyard area are $314 \mathrm{~m} \times 500 \mathrm{~m}$. For the synchronous condenser, the yard area is $150 \mathrm{~m} \times 300 \mathrm{~m}$.

Following review of a 2008 report relative to a geotechnical study conducted at this site, an agreed assumption of balanced cut and fill mass excavation work, comprising $85 \%$ overburden and $15 \%$ rock was considered in the CCE excluding the synchronous condenser portion of the site.

In order to avoid disrupting an existing small pond near the Soldier Pond Project site, the Synchronous Condenser was detached from the main facilities and located

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approximately 140 meters to the (South-East). The assumption considered for the synchronous condenser site excavation work is $100 \%$ rock.

## 315kV Switchyard

All concrete foundations work for circuit breakers, disconnect switches, capacitor voltage transformers, current transformers, surge arresters, gantries, etc. are included in the CCE.

A control building housing 72 control panels, batteries, chargers is also included.

## Converter 350 Kv DC

All concrete foundations work for circuit breakers, disconnect switches, capacitor voltage transformers, current transformers, power transformers, surge arresters, filters, gantries, etc. are included in the CCE.

For the valves control building, typical engineering referenced with similar projects was performed. A provision of $2,700 \$+600 \$ / \mathrm{m} 2$ was considered in the CCE.

### 3.3.6.3 Electrical Equipment

## Switchyard

All standard electrical equipment was priced through issuance of short-form technical specifications for the purpose of obtaining budget prices from suppliers. Generally, and where applicable, the average of two highest submitted prices were considered. Where not applicable an estimator judgement call was applied based on past experience.

## Converter 350 Kv DC

For the converter's specialized electrical equipment a short-form technical specifications was issued for the purpose of obtaining budget prices from suppliers. This specification stated that Supply of equipment needed to include the design, manufacturing, quality control, transportation to site, storage and documentation. The supply is to include all equipment and materiel, required to provide a complete and

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operational converter station. The main equipments included in the Converters station are as follow:

- Thyristor valves and valve cooling system
- Converter transformer
- Smoothing reactors
- Surge arresters
- $A C$ filters
- DC filters
- Measuring devices
- Control and protection system
- DC switching Device
- AC breakers and switching devices
- Busworks and insulators
- AC/DC station auxiliary power supply
- Smoke detectors in valve hall
- CCTV (camera system)
- Steel structures

In order to perform the work related to the AC/DC Switchyard and Converter stations, the displacement and diversion of the LT-218 Hollyrood existing line is required prior to commencement of the Work in 2013. These costs are included in the Component 4 - Transmission Lines portion of the CCE.

Furthermore, if, following detailed engineering studies, the location of the facilities was to change from what is currently assumed in the CCE, it could be required to relocate the TL-242 Hollyrood line as well.

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### 3.3.6.4 Other Works

An $20 \mathrm{~m} \times 50 \mathrm{~m}$ meter pre-engineered type maintenance and operations building complete with a 5 tonnes overhead crane and all tools and equipment are included in the CCE. There are no provisions for cabinets, tool chests or heavy shelving.

For integration into existing Power Grid modifications and upgrades to protection systems will be required at in the following Substations:

- Holyrood
- Wester Avalon
- Oxen Pond
- Hardwood


### 3.3.7 L'anse-au-Diable and Dowden's Point Shoreline Pond Electrodes

Estimate is a unit Rate Based estimate based on scope, design and bulk quantities developed from the concept designs as detailed in the Shoreline Pond Electrodes Design Brief SLI doc no. 505573-480B-47EM-0004 (the Design Brief)

All construction work, with the exception of the Dowden's Point dredging activities can be performed from shore.

L'anse-au-Diable Pond electrode
This proposed site at L'Anse-au-Diable is in a south facing cove with somewhat rectangular dimensions of 130 m to 150 m wide and length of approximately 150 m . It is assumed that no excavation will be needed at this site as it is exposed rock.

The construction of this facility will occur over a 6 to 8 month period. The facility is close to existing access roads and will use standard civil equipment for construction. It is not anticipated that the contractor would need to mobilize any marine based equipment.

Approximately 400 m of access road will be required to access the site; there will be a small lay down construction area constructed at the approach for the new

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breakwater. All material will be end dumped into the ocean and shaped with a long reach backhoe. Armour stone will be dumped on the slope and repositions with a crane or long reach backhoe.

- Rates are based on non union sites. (Marine Contractors are generally nonunion
- No dredging is anticipated at L'Anse-au-Diable
- Sheet pile cut-off wall work has been included to avoid silting of the permeable material during breakwater construction
- There is no allowance for winter construction.
- Armour stone in the sizes required is readily available within a 10 km radius.
- Service Building is prefabricated off site.


## Dowden's Point Pond electrode

At the Dowden's Point Shoreline Pond Electrode, the crest of the breakwater aligns with the top of the existing bank and the sea side toe line coincides with the existing low tide shoreline. The depth of the soil above the bedrock at Dowden's Point is anticipated to be approximately 30 m , which would permit excavation without the need to blast bed rock.

The construction of this facility will occur over a 6 to 8 month period. The facility is close to existing access roads and will use standard civil equipment for construction. The current concept required that the contractor will mobilize marine based equipment for a dredging operation. Dredging costs are based on ocean dumping Approximately 400 m of access road will be required to access the site; there will be a small lay down construction area constructed at the approach for the new breakwater. All material will be end dumped into the ocean and shaped with a long

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reach backhoe. Armour stone will be dumped on the slope and repositions with a crane or long reach backhoe

- Unit Rates are based on historical data for Marine Construction in Atlantic Canada and Newfoundland.
- Dredging rates for Dowdens Point location assumed dredged spoils from dredging operations use disposal at sea.
- Rates assume availability of Marine contractors and competitive bidding.
- Rates are based on non union sites. (Marine Contractors are generally nonunion)
- Disposal of mass excavation from Dowdens Point assumes a haul distance of 2 km.
- There is no allowance for winter construction.
- Service Building is prefabricated off site.
- Provisions have been included in the CCE for the relocation of the east coast trail at the Dowden's Point location.


### 3.3.7.1 Site Preparation and Access

Access roads
For both sites, access roads to the site will be constructed to link with existing local roads (approximately 400 m ). From the entrance to the site, the road will extend along the inside of the breakwater to provide access for maintenance of the shoreline pond electrodes. The width of the access road is assumed to be 6.0 m

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### 3.3.7.2 Civil Works

## Marine Structures (Breakwater)

The breakwater is designed to withstand the expected worst case site conditions, including wave action, tidal effects, pack ice and freezing inside the shoreline pond. Wave height is assumed to be 6.0 m and this is the basis for sizing and pricing the armour stone. Armour stone has a maximum size of 10 tonnes that will need to placed on the ocean side at a shallower slope than the natural angle of repose of the material which implies increased construction cost that has been considered in the CCE. The core material is a uniformly sized material to allow maximum water permeability through the breakwater berm. This material will need to be selected and treated to meet these requirements and has been estimated accordingly.

Only preliminary topographical and bathymetric mapping of the site area was available at time of the CCE.

## Electrode Supports and Protection

The structural supports and protection for electrode and cables are designed utilizing concrete to withstand the expected worst case site conditions, including freezing spray, tidal effects, and freezing inside the shoreline pond. Fibre reinforced plastic (FRP) reinforcements will be used to eliminate corrosion problems due to currents.

The CCE caries minimal cast in place concrete as most of the concrete elements will be prefabricated

Relatively small quantities of cast in place concrete will be required to encase electrical ducts element at both Pond electrode locations. These quantities are assumed to be mixed and placed using portable mixers using hand fed bagged concrete

### 3.3.7.3 Electrical Equipment

The electrical work for the pond electrodes includes the following:

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- The threading of the electrodes from the surface through a 300 mm protective concrete pipe reaching $1,5 \mathrm{~m}$ below the low water level and depositing the electrode in a submerged PVC saddle supported on concrete blocks with the help of divers.
- Anotec electrodes type 4884 H priced through budget quotes from specialized suppliers, Anotec
- Electrode main feeder cable, of $750 \mathrm{~mm}^{2}$, Single core XLPE electrical cable at each location, estimated using load current bearing capacity and layout drawings
- 1 set of Telecommunication Service Panel and Optical Distribution Panel
- 1 set each of Service panel, Protection and Monitoring panel, 48 VDC battery chargers, 48 VDC battery bank, 120-240 V AC distribution panel, DC distribution panel, lighting control panel.
- The Electrode main feeder cable shall be laid in cable trench
- A small control building for which a provision has been included in the CCE


### 3.3.7.4 Other Works

Fencing
The site will be fenced on all sides by chain link fencing to prevent public access to the pond. The fencing in contact with the berm needs to be a special isolated fence comprised of timber posts with isolators between each panel of chain link fence

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## 4 VOLUME IV - COMPONENT 4 DETAILED ESTIMATE ASSUMPTIONS

### 4.1 INTRODUCTION

The Component 4 estimate assumptions were developed by the SLI transmission lines Group and are included in document 505573-4600-33RA-0002 entitled GATE 3 ESTIMATE ASSUMPTIONS Component 4 - Transmission Lines. This document is presented herein as an integral part of the CCE.
4.2 DOCUMENT 505573-4600-33RA-0002-GATE 3 ESTIMATE ASSUMPTIONS COMPONENT 4 - TRANSMISSION LINES

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## GATE 3 ESTIMATE ASSUMPTIONS

## Component 4 - Transmission Lines



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## 1 ABBREVIATIONS

NE-LCP - Nalcor Energy - Lower Churchill Project

SLI - SNC Lavalin Inc.

EPCM - Engineering Procurement and Construction Management

HVac - High Voltage Alternating Current
HVdc - High Voltage Direct Current

EIA - Environmental Impact Assessment

MF - Muskrat Falls

CF - Churchill Falls

SP - Soldier's Pond

GI - Gull Island

ROW - Right Of Way

PMPC - Project Management / Project Controls

DWSM - Dual Window Single Mode

## 2 REFERENCES

This document is based on:

- LCP-PT-ED-0000-EN-PH-0021-01 - "Design Philosophy for HVac Transmission Lines".
- LCP-PT-ED-0000-EN-PH-0022-01 - "Design Philosophy for HVdc Transmission Lines".
- MFA-PT-ED-6200-TL-DC-0001-01 - "Meteorological Loading 315 kV Transmission Lines Muskrat Falls to Churchill Falls".

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- MFA-PT-ED-6200-TL-DC-0002-01 - "Overhead Transmission Meteorological Loading for the Labrador - Island Transmission Link".
- LCP-PT-ED-0000-EN-RP-0001-O1 - "Basis of Design".
- File No. TF1116574 - " 315 kV HVac Transmission Line Foundations, Muskrat Falls to Churchill Falls: Geotechnical Design Parameters"
- 505573-361A-4ZEC-0001 - "315 kV HVac Route Selection Criteria"
- 505573-361B-44ER-0001 - "315 kV HVac Geotechnical Baseline"
- 505573-361B-43EC-0001 - "315 kV HVac Tower Design Criteria"
- 505573-361B-42EC-0001 - "315 kV HVac Foundation Design Criteria"
- 505573-462B-43ER-0001 - " 315 kV HVac and 350 kV HVdc Cascading Assumptions"
- 505573-462C-4ZEC-0008 - "350 kV HVdc Line Design Criteria"
- 505573-462B-43EC-0001 - "350 kV HVdc Tower Design Criteria"
- 505573-462B-44ER-0001 - "350 kV HVdc Geotechnical Baseline"
- 505573-462B-43ER-0002 - "Assessment of Installing the HVdc Ground Return on a Separate Wood Pole Line"
- 505573-462B-43ER-0002 - "350 kV HVdc Foundation Design Criteria"
- 505573-462A-4ZEC-0002 - "Electrode Lines - Route Selection Criteria"
- 505573-463C-4ZEC-0001 - "Electrode Lines on Wood poles - Design Criteria"
- 505573-362C-4ZEC-0001 - " 25 kV construction Power Line \& 138 kV tap Design Criteria"


## 3

MAJOR EXCLUSION PRIOR TO ENVIRONMENTAL ASSESSMENT APPROVAL
This estimate does not include the costs associated with:

- Consultation: Nalcor Energy is responsible for consultations and open houses. SNC Lavalin Inc. (SLI) will provide technical support to Nalcor.

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- Environmental: Nalcor is responsible for environmental permits. SLI will provide engineering support to Nalcor.
- Regulatory: Nalcor is responsible for all costs associated with the regulatory process. SLI will provide engineering support to Nalcor.
- Land: Nalcor is responsible for land negotiations and easement acquisitions.


## 4 TRANSMISSION LINE GENERAL SCOPE OF WORK

The LCP line project includes:

- The Engineering, Procurement, and Construction Management (EPCM) of two new 315 kV single circuit HVac transmission lines, each approximately 250 km in length. The south transmission line and the north transmission line between Muskrat Falls (MF) and Churchill Falls (CF) consider a 50 m Right of Way (ROW) each. A 50 m distance between centerlines will be used when the lines are parallel to one another. See section 4.1 of this document for the outline of engineering assumptions for the HVdc line.
- The EPCM of a new $\pm 350 \mathrm{kV}$ bi-pole HVdc transmission line, approximately 1100 km in length. The future HVdc line from MF to SP considers a 60 m ROW; see section 4.2 of this document for the outline of engineering assumptions for the HVdc line.
- The EPCM of approximately 35 km of electrode lines on wood pole structures, see section 4.3 of this document for the outline of engineering assumptions for the electrode line.
- The EPCM of approximately 17 km of 25 kV distribution lines to supply power to the accommodation complex and camp. See section 4.4 of this document for the outline of engineering assumptions for the 25 kV construction power line.
- The EPCM for the modification to six existing transmission lines to accommodate the new $\pm 350$ kV HVdc crossings. See section 4.5 of this document for the outline of engineering assumptions for the HVdc crossings.

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- The EPCM for the re-termination of four 230 kV transmission lines into the future Soldier's Pond Substation. See section 4.6 of this document for the outline of engineering assumptions for the re-termination of the 230 kV transmission lines.
- The EPCM of approximately 600 m of two new single circuit 735 kV HVac transmission lines at the Churchill Falls Substation. See section 4.7 of this document for the outline of engineering assumptions for the 735 kV HVac transmission line.
- The EPCM of approximately 500 m of four new 315 kV HVac transmission lines to interconnect the Muskrat Falls Powerhouse to the new Switchyard. See section 4.8 of this document for the outline of engineering assumptions for the 315 kV HVac interconnection.


## 5 ENGINEERING ASSUMPTIONS

### 5.1 315 KV HVac TRANSMISSION LINE

### 5.1.1 Tower Design and Testing

- The 315 kV lattice steel tower families are developed specifically for the LCP project. The tower design criteria is based on criteria document "315 kV HVac Tower Design Criteria (SLI No. 505573-361B-43EC-0001)" and " 315 kV HVac and 350 kV HVdc Cascading Assumptions (SLI No. 505573-462B-43ER-0001)".
- The two transmission lines are estimated based on the 35 mm radial ice loading zone.
- OPGW dead-ending on suspension structures is considered.
- All tower weights are estimated based on the preliminary tower designs completed by SLI.
- The design of the tower family and associated foundations are engineered by SLI. The tower detailing and the prototype testing will be by the supplier.
- Tower Types $A$ and $B$ are guyed mast structures and tower types $C, D$ and $E$ are rigid self supporting towers with four legs.
- No long-span or special crossing structures have been considered.

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- Phase transposition is assumed to take place near existing dead-end structures using additional insulators and hardware to facilitate the transposition. This estimate assumes that phase transposition will occur at three locations along each HVac line.
- Tower testing is included for the A and D type towers only. Tower types B, C and E will not be tested.


### 5.1.2 Hardware Assemblies and Testing

- The creation of 315 kV hardware assembly design requirement drawings for the tower family is included (i.e. assemblies for conductors, counterpoise, OHSW, and OPGW, etc.).
- All 315 kV assemblies will use reduced-corona hardware.
- Hardware assembly prototype testing is included, along with test witnessing by SLI.
- Third party inspection during manufacturing has been included.


### 5.1.3 Centerline / Layout

- This estimate is based on the center line and layout on the route map drawings (SLI Doc. 505573-361A-4ZDD-0022-PA).
- The centreline for the estimate has been established based on document " 315 kV HVac Route Selection Criteria (SLI Doc. 505573-361A-4ZEC-0001)".
- It is assumed that there is some flexibility to modify the centerline and Pl (Point of Inflection) location in an effort to optimize the line layout.
- The survey data used for the preliminary layout was provided by Nalcor and based on 2010 LiDAR survey and orthophotography.
- The layout was completed based on document " 315 kV HVac Line Design Criteria (SLI Doc. $505573-361 \mathrm{C}-4 Z E C-0001$ )" as well as $40 \%$ completion of detailed engineering.

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### 5.1.4 Quantities of Towers and Foundation Steel

- The quantity of towers estimated includes all basic/standard towers, body extensions, and leg/mast extensions, including nuts, bolts, plates, washers, and attachment vangs, as per the design drawings, specifications and other contract documents.
- The quantity of towers is based on preliminary ( $40 \%$ completed engineering) tower spotting using PLS-CADD.
- The material extras for spares, un-foreseen re-routes, structure additions, design changes, etc. are not included.
- Four types of foundations are considered:
- Type 1 for granular soil with a net allowable bearing capacity of $\mathbf{2 5 0} \mathbf{~ k P a}$,
- Type 2 for granular soil with a net allowable bearing capacity of 100 kPa ,
- Type 3 for rock foundations, and
- Type 4 for a deep foundation using screw piles or driven steel piles.
- Two types of materials have been defined in the " 315 kV HVac Geotechnical Baseline (SLI No. 505573-361B-44ER-0001)" as acceptable for the backfill to be installed for the steel grillage for the type 1 and type 2 foundations.
- Four types of guy wire anchors are defined:
- Soil anchors for granular soil with a net allowable bearing capacity of 250 kPa ,
- Soil anchors for granular soil with a net allowable bearing capacity of 100 kPa ,
- Rock anchors, and
- Steel pile anchors for weak soil conditions.
- The quantities of guy wire anchors are estimated based on the structure quantities from the preliminary design and layout. The guy wire length is assumed to be 40 m per guy, four guys per tower.
- The foundation types will be derived from the results of the geotechnical assessment completed by AMEC entitled " 315 kV HVac Transmission Line Foundations, Muskrat Falls to Churchill

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Falls: Geotechnical Design Parameters" and the " 315 kV HVac Geotechnical Baseline (SLI No. 505573-361B-44ER-0001)".

### 5.1.5 Quantities for Conductor, OHSW and OPGW Hardware Assemblies

- The quantity of hardware assemblies is based on total tower quantities, from the preliminary centerline and layout.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.1.6 Quantities of Insulators

- The quantities of insulators are based on the total tower quantities derived from the preliminary centerline and layout.
- Porcelain or toughened glass insulators are assumed to be acceptable in this estimate. The quantity and strength of insulators per tower is based on the document "315 kV HVac Line Design Criteria (SLI Doc. 505573-361C - 4ZEC - 0001)".
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.1.7 Quantities of Conductor and OHSW / OPGW

- Two-bundle, $795 \mathrm{kcmil}, 26 / 7$ ACSR "Drake", will be used as the phase and jumper conductor. The quantity is based on the linear line length, with an additional $4 \%$ included for sag and wastage.
- One OHSW will be installed using $1 / 2^{\prime \prime}$ grade 220 steel. The quantity is based on the linear line length, with an additional $2 \%$ included for sag and wastage.
- One OPGW will be installed using fibre type DWSM based on standard ITU-T6.654. The quantity is based on the linear line length, with an additional $5 \%$ extra included for sag, down leads, splices, and wastage.

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- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.1.8 Quantities of Conductor Accessories

- Spacer dampers are assumed to be installed every 60 m , per phase, and are assumed to be adequate for the damping requirements of the line.
- $100 \%$ of the line has been considered for compression type splices, dead-ends and jumper connectors.
- Conductor splices are assumed to be installed approximately every 3000 m .
- Each 315 kV HVac line will have approximately five structures that will require the use of counter weights ( 25 kg each), considering four weights per phase. The quantities are based on the preliminary layout.
- Rigid spacers will be used on jumper conductors, assuming 6 spacers, per phase, per jumper.
- One jumper assembly per phase, per tower type $C, D$ and $E$ is considered.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.
- Three aerial marker cones (1 white and 2 orange) will be included per crossing. They will be installed on the approprlate wire for each respective crossing. The estimate considers 35 crossings for each 315 kV HVac Line ( 20 highway crossings, 5 transmission line crossings, 10 river crossings).


### 5.1.9 Quantities of OPGW Accessories

- Two spiral vibration dampers per structure will be used on the OPGW as per the tower quantity estimation.
- OPGW splice boxes will be installed approximately every 6000 m and on the first structure outside of each substation.

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- The OPGW down lead clamps will be installed every 3 m .
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.1.10 Quantities of OHSW Accessories

- Two spiral vibration dampers per structure will be used on the OHSW as per the tower quantity estimation.
- The bonding conductor is assumed to be \#2 ACSR "Sparrow" and the length is estimated to be 1.5 m for suspension towers and 2.0 m for dead-end structures.
- Splices will be installed approximately every 3000 m on the OHSW.
- $100 \%$ of the line has been considered for compression type splices.
- Bird diverters are not required and not included in the estimate.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.1.11 Counterpoise

- The counterpoise length is estimated as the linear line length plus an additional $2 \%$ for wastage.
- A bonding conductor of 10 m , the same material as the counterpoise, is included per tower.


### 5.1.12 Quantities of Miscellaneous Hardware and Material

- The hardware required for tower grounding is included.
- Aerial structure number boards will be installed on every $10^{\text {th }}$ structure.
- One structure number tag will be installed on every structure.
- Two danger signs will be installed on every structure.

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- Six aerial line number boards will be included per line, and will be installed on the first structure outside each substation.
- Phasing signs will be installed on every $10^{\text {th }}$ structure.


### 5.1.13 Geotechnical Investigations

- The document "315 kV HVac Geotechnical Baseline (SLI No. 505573-361B-44ER-0001)" includes:
- The geotechnical report based on references from past soil investigations.
- Assessment of the foundation types to be used for each of the new 315 kV HVac towers.
- The selection criteria for the design parameters of soil and rock for each of the foundation types (1, 2, 3 and 4).
- The detail of the additional geotechnical investigations necessary to confirm the selection of the foundation types, including the location, type of investigation, and the estimated cost for those additional soil tests.


### 5.1.14 Electrical Effects / Considerations

- The transmission line ROW is 50 m , which is assumed to be within the acceptable limits for:
- Edge of right of way electric / magnetic field levels,
- Edge of right of way audible noise levels, and
- Edge of right of way radio and television interference.


### 5.1.15 Distribution and Transmission Line Conflicts

- Crossing line modifications for the HVac lines are not included in this estimate.

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## $5.2 \pm 350 \mathrm{kV}$ HVdc TRANSMISSION LINE

### 5.2.1 Tower Design and Testing

- The $\pm 350 \mathrm{kV}$ lattice steel tower families are developed specifically for the LCP project. The tower design criteria is based on criteria document " 350 kV HVdc Tower Design Criteria (SLI Doc. $505573-462 \mathrm{~B}-43 \mathrm{EC}-0001$ )" and " 315 kV HVac and 350 kV HVdc Cascading Assumptions (SLI No. 505573-462B-43ER-0001)".
- These steel towers will be designed for the combination of the meteorological loading zones ( 50 mm ice, Alpine [ 135 mm rime ice] and 75 mm ice); the different pollution levels (Inland and Coastal) and with and without electrode conductors, giving a total of ten different tower families.
- OPGW dead-ending on suspension structures is considered.
- The majority of towers used in the Labrador segment will be designed and constructed to support the electrode conductors from the Muskrat Falls substation to the grounding site at L'Anse-au-Diable.
- The design of the tower family and its foundations are to be done by SLI. Tower detailing and the prototype testing are by the supplier.
- Suspension tower types A and B are guyed mast structures, dead-end tower types C, D and E are rigid self supporting four leg towers.
- Neither long-span, nor special crossing structures have been considered.
- All tower weights are estimated based on tower designs by SLI for tower types A and D of the F1, F2, F4, F6 and F7 families. These ten towers represent more than $85 \%$ of the towers for the 350 kV HVdc line.
- The geometry and weights of the remaining tower families and types were extrapolated based on the design of those ten tower types and based on the relative weights of the 315 kV HVac tower weights already defined for tower types $\mathrm{A}, \mathrm{B}, \mathrm{C}, \mathrm{D}$ and E .
- Tower testing is included for six towers (four suspension towers and two dead-end towers); detailing is considered for twenty towers.

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### 5.2.2 Hardware Assemblies and Testing

- The estimate includes the creation of the $\pm 350 \mathrm{kV}$ hardware assembly design requirement drawings for the tower family (i.e. assemblies for conductors, electrode, OPGW, etc.).
- All pole conductor assemblies will use reduced-corona hardware.
- The hardware assembly prototype testing is included, along with witness testing by SLI.
- Third party inspection during manufacturing has been included.


### 5.2.3 Centerline / Layout

- The estimate is based on the center line and layout shown on the alignment sheet drawings (SLI Doc. 505573-462A-4ZDD-0001, 0002, 0003, 0004, 0005, and 0016).
- It is assumed that there is flexibility to modify the centerline and PI location in an effort to optimize the line layout.
- The survey data used for preliminary layout was provided by Nalcor and based on 2010 LiDAR survey and orthophotography.
- The centreline for the estimate has been established based on the document " $\pm 350 \mathrm{kV}$ HVdc Muskrat Falls to Soldier's Pond Transmission Line - Route Selection Design Criteria (SLI Doc. 505573-462A-4ZEC-0001)".
- The layout was completed based on the document " 350 kV HVdc Line Design Criteria (SLI Doc. 505573-462C-4ZEC-0008)".


### 5.2.4 Quantities of Towers and Foundation Steel

- The quantity of towers estimated includes all basic / standard towers, body extensions, and leg/mast extensions, including nuts, bolts, plates, washers, and attachment vangs, as per the design drawings, specifications, and other contract documents.
- The quantities of steel towers are based on preliminary ( $40 \%$ complete engineering) tower spotting using PLS-CADD.

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- Material extras for spares, un-foreseen re-routeing requirements, structure additions, design changes, etc. are not included.
- The quantities of guy wire anchors are estimated based on the preliminary design and layout. Guy wire length is assumed to be 40 m per guy, four guys per steel tower.
- Four types of foundations are defined:
- Type 1 for granular soil with a net allowable bearing capacity of 250 kPa ,
- Type 2 for granular soil with a net allowable bearing capacity of 100 kPa ,
- Type 3 for rock foundations, and
- Type 4 for a deep foundation using screw piles or driven steel piles.
- Two types of material have been defined in the " 350 kV HVdc Geotechnical Baseline (SLI No. 505573-462B-44ER-0001)" as acceptable for the backfill to be installed for the steel grillages of type 1 and type 2 foundations.
- Four types of guy wire anchors are defined:
- Soil anchors for granular soil with a net allowable bearing capacity of 250 kPa ,
- Soil anchors for granular soil with a net allowable bearing capacity of 100 kPa ,
- Rock anchors, and
- Steel pile anchors for weak soil conditions.
- The quantity and weight of each of the foundation types are based on the relative quantities and weights of the foundation types for each tower type as defined for the HVac Lines.


### 5.2.5 Quantities for Conductor and OPGW Hardware Assemblies

- The quantities of hardware assemblies are based on the total tower structure quantities from the preliminary centerline/layout.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.

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### 5.2.6 Quantities of Insulators

- The quantities of insulators are based on total structure quantities, from the preliminary centerline/layout.
- Porcelain or toughened glass insulators are assumed to be acceptable in this estimate. The quantity and strength of insulators per structure is based on the document " 350 kV HVdc Line Design Criteria (SLI Doc.505573-462C-4ZEC-0008)".
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.2.7 Quantities of Electrode conductor

- Two types of electrode conductor are used depending on the loading zone:
- Single 1192.5 kcmil ACSR "Grackle" is considered for the 50 mm and 75 mm ice load zones, and
- Single 1510.5 kcmil ACSR "Parrot" is considered for the 135 mm ice Alpine load zone.
- The quantity is based on the linear line length, with an additional $4 \%$ included for sag and wastage.


### 5.2.8 Quantities of Conductor and OPGW

- A single $3640 \mathrm{kcmil}, 91 / 0$ Strand, Aluminum Stranded Conductor (ASC) is used as the pole and jumper conductor. The quantity is based on the linear line length, with an additional 4\% included for sag and wastage.
- Three types of OPGW cable we used depending on the loading zone:
- 14.5 mm , 24 Fibre, 140 kN UTS - for the 50 mm ice load zone,
- $15.5 \mathrm{~mm}, 24$ Fibre, 177 kN UTS - for the 75 mm ice load zone, and
- $20.6 \mathrm{~mm}, 24$ Fibre, 277 kN UTS - for the 135 mm ice Alpine load zone.

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- Each quantity is based on the linear line length, with an additional 5\% extra included for sag, down leads, splices, and wastage.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.
- There is no OHSW on the HVdc line.


### 5.2.9 Quantities of Conductor Accessorles

- The quantity of conductor accessories is based on total structure quantities from the preliminary centerline / layout.
- $100 \%$ of the line has been considered for compression type splices, dead-ends and jumper connectors.
- Splices will be installed approximately every 1200 m on conductor.
- One jumper assembly, per pole, per tower type $C, D$ and $E$ is considered.
- Preliminary layout has determined that the $\pm 350 \mathrm{kV}$ HVdc line will have approximately 20 structures that will require the use of counter weights ( 25 kg each), four weights per pole.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.
- Three aerial marker cones ( 1 white and 2 orange) will be included per crossing. They will be installed on the appropriate wire for each respective crossing. There are 71 crossings ( 20 highways, 18 transmission line crossings, 6 water crossings, and 27 distribution crossings) included.


### 5.2.10 Quantities of OPGW Accessories

- Two spiral vibration dampers, per structure, will be used on the OPGW as per the tower quantity estimation.

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- OPGW splice boxes will be installed approximately every 6000 m and on the first structure outside of each substation.
- OPGW down lead clamps have been assumed to be required every 3 m .
- Bird diverters are not required, and not included in the estimate.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.2.11 Counterpoise

- The counterpoise length is estimated as the linear line length plus an additional $2 \%$ for wastage.
- A bonding conductor of 10 m , the same material as the counterpoise, will be included per tower.


### 5.2.12 Quantities of Miscellaneous Hardware and Material

- The hardware required for tower grounding is included.
- Aerial structure number boards will be installed on every $10^{\text {th }}$ structure.
- One structure number tag will be installed on every structure.
- Two danger signs will be installed on every structure.
- Ten aerial line number boards will be included per line, and will be installed on the first structure outside each substation.


### 5.2.13 Geotechnical Investigations

- The document "350 kV HVdc Geotechnical Baseline (SLI No. 505573-462B-44ER-0001)" includes:
- The geotechnical report references from past soil investigations,
- The assessment of foundation types to be used for each of the new $\pm 350 \mathrm{kV}$ HVdc towers,

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- The selection criteria for the design parameters of soil and rock for each of the foundation types (1, 2, 3 and 4), and
- The detail of the additional geotechnical investigations necessary to confirm the selection of the foundation types, including the location, type of investigation, and estimated cost for those additional soil tests.


### 5.2.14 Electrical Effects / Considerations

- The transmission line ROW for the $\pm 350 \mathrm{kV}$ HVdc line is 60 m , which is assumed to be within the acceptable limits for:
- Edge of right of way electric / magnetic field levels,
- Edge of right of way audible noise levels, and
- Edge of right of way radio and television interference.


### 5.2.15 Distribution and Transmission Line Conflicts

- The estimate assumes that dead-end structures are required between and on either side of existing power lines when the HVdc line crosses two or more existing power lines. Based on this, six transmission line conflicts have been identified that require modifications. Details of the engineering assumptions made for the modification to these six transmission lines is in Section 4.5 of this document.


### 5.3 ELECTRODE LINES ON WOOD POLES

### 5.3.1 Electrode Line Structures

- The electrode lines will be routed to two facilities for the electrode grounding, one at L'Anse-auDiable and another at Dowden's Point.
- Tangent and angle structures will be single pole direct embedded, Class H 1 , wood poles, with a horizontal V-brace configuration.

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- Dead-end structures will be Class H 1 , guyed, two pole H -frame structures.
- H 1 wood pole sizing will range from $12.3 \mathrm{~m}(40 \mathrm{ft})$ to a maximum of $18.5 \mathrm{~m}(60 \mathrm{ft})$ in length.
- No long-span or special crossing structure is included.


### 5.3.2 Hardware Assemblies

- The Electrode line hardware assemblies used for the wood pole sections will be similar to the hardware specified in section 4.1.2 of this document.


### 5.3.3 Centerline / Layout

- The centreline for the estimate has been established based on the document "Electrode Lines Route Selection Criteria (SLI Doc. 505573-462A-4ZEC-0002)".
- The layout was completed based on the document "Electrode Lines on Wood Pole - Design Criteria (SLI Doc. 505573-463C-4ZEC-0001)".
- It is assumed that there is flexibility to modify the centerline and PI location in an effort to optimize the line layout.
- The survey data used for preliminary layout was based on available orthophotography; no LiDAR has been used for the electrode line routes.


### 5.3.4 Quantities of Poles and Foundations

- The quantity of wood poles is based on preliminary PLS-CADD spotting.
- Wood poles will be direct embedded using standard setting methods.
- The quantities of guy wire and anchors are estimated based on the preliminary design and layout. The guy wire length is assumed to be 30 m per guy, four guys per wood pole dead-end.
- Material extras for spares, un-foreseen re-routes, structure additions, design changes, etc. are not included.

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### 5.3.5 Quantities for Conductor Hardware Assemblies

- The quantity of hardware assemblies is based on total wood pole structure quantities from the preliminary centerline/layout.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.3.6 Quantities of Insulators

- The quantity of insulators is based on total structure quantities, from the preliminary centerline/layout.
- Porcelain or toughened glass insulators are assumed to be acceptable in this estimate. The quantity and strength of insulators per structure is based on the document "Electrode Lines on Wood Pole - Design Criteria (SLI Doc. No. 505573-463C-4ZEC-0001)".
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.3.7 Quantitles of Electrode conductor

- Both the Labrador and Island Electrode wood poles lines will use single 1192.5 kcmil, ACSR "Grackle", as the conductor.
- The quantity is based on the linear line length, with an additional $4 \%$ included for sag and wastage.


### 5.3.8 Quantities of Electrode Conductor Accessories

- 100\% of the electrode lines have considered compression type splices, dead-ends and jumper connectors.

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- Stockbridge dampers will be used, as per the manufacturer's recommendation, for each span along the line.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.
- There is neither OHSW nor OPGW on the electrode lines.


### 5.3.9 Quantities of Miscellaneous Hardware and Material

- Aerial structure number boards will be installed on every $25^{\text {th }}$ structure of the electrode line.
- One structure number tag will be installed on every structure.
- One danger sign will be installed on every structure.
- Aerial line number boards will be included, and will be installed on the first and last structure.


### 5.3.10 Geotechnical Investigations

- There will be no geotechnical investigation for the wood pole lines.


### 5.3.11 Electrical Effects / Considerations

Both electrode lines are considered as distribution lines, therefore, as per Newfoundiand Hydro standard D1-11-66-R1, the ROW will be 9 m , which is assumed to be within the acceptable limits for:

- Edge of right of way electric / magnetic field levels,
- Edge of right of way audible noise levels, and
- Edge of right of way radio and television interference.

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### 5.425 kV CONSTRUCTION POWER

### 5.4.1 Structure design

- All construction power structures will be Newfoundland Hydro standard 25 kV wood pole structures.
- Two custom structures will be designed to accommodate a long-span river crossing.
- Standard setting methods will be used for each structure.


### 5.4.2 Hardware Assemblies

- All construction power hardware assemblies will be Newfoundland Hydro standard 25 kV assemblies.
- Custom hardware will be designed to accommodate the river crossing.


### 5.4.3 Centerline / Layout

- The construction power centerline has been established to follow the existing north road and the future south access road to the accommodation complex for the majority of the route.
- Part of the 25 kV center line will also follow the existing 315 kV HVac line to minimize the tree clearing required.
- It is assumed that there is flexibility to modify the centerline and PI location in an effort to optimize the line layout.
- The survey data used for preliminary layout was provided by Nalcor and based on 2010 LiDAR survey and orthophotography.


### 5.4.4 Quantities of Structures

- The quantities of wood pole structures are based on preliminary ( $40 \%$ complete engineering) spotting.

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- Material extras for spares, un-foreseen re-routes, structure additions, design changes, etc. are not included.
- The quantities of guy wire and anchors are estimated based on the preliminary design and layout. Guy wire length is assumed to be 20 m per guy, four guys per dead end structure.


### 5.4.5 Quantities for Conductor and ADSS Hardware Assemblies

- The quantities of conductor and ADSS hardware assemblies are based on the total structure quantities from the preliminary centerline/layout.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.4.6 Quantities of insulators

- Quantity of insulators is based on total structure quantities, from the preliminary centerline/layout.
- The quantity and strength of insulators per structure will be based on Newfoundland Hydro distribution standards.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.4.7 Quantities of Conductor and OPGW

- A single 477 Aluminum Stranded Conductor (ASC) "Cosmos" will be used as the phase and jumper conductor. The quantity is based on the linear line length, with an additional 4\% included for sag and wastage.
- 4/0 Aluminum Alloy Stranded Conductor (AASC) "Oxlip" will be used as the neutral wire. The quantity is based on the linear line length, with an additional $4 \%$ included for sag and wastage.

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- Two ADSS cables, 48 fibres each, shall be installed and used for telecommunication. The quantity is based on the linear line length, with an additional $5 \%$ extra included for sag, down leads, splices, and wastage.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.4.8 Quantities of Conductor Accessories

- $100 \%$ of the line has been considered for compression type splices, dead-ends and jumper connectors.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.
- Three aerial marker cones (1 white and 2 orange) will be included for the river crossing.


### 5.4.9 Quantities of ADSS Accessories

- ADSS splice boxes will be installed approximately every 2000 m and on the first structure outside of the substation, as well as at required tap points.
- ADSS down lead clamps have been assumed to be required every 3 m .
- Bird diverters are not required, and are not included in the estimate.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.4.10 Grounding

- Ground rods will be installed at each guyed structure and/or at an interval of 3 structures per kilometre.

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### 5.4.11 Quantities of Miscellaneous Hardware and Material

- One structure number tag will be installed on every structure.


### 5.4.12 Electrical Effects / Considerations

- The ROW for the 25 kV construction power line is 7.5 m wide, as per the Newfoundland Hydro Standard.


### 5.4.13 Distribution and Transmission Line Conflicts

- The proposed 25 kV construction power line will have to cross one existing distribution line.


### 5.5 MODIFICATIONS TO EXISTING LINES FOR HVdc CROSSINGS

The new $\pm 350 \mathrm{kV}$ HVdc transmission line will only cross one existing transmission line per span. Six existing transmission lines will need alignment modifications to accommodate the new $\pm 350 \mathrm{kV}$ HVdc transmission line structures. See Table 1 for the list of lines that will need to be modified:

Table 1: Existing Lines to be modified

| Modfflcation <br> Number | Line to be modlfled | kV level | Structure Type |
| :---: | :---: | :---: | :---: |
| 1 | TL251 | 69 kV | Wood Pole |
| 2 | TL232 | 230 kV | Wood Pole |
| 3 | TL204 | 230 kV | Single Circuit Tower |
| 4 | NFP | 138 kV | Wood Pole |
| 5 | NFP | 138 kV | Wood Pole |
| 6 | TL201 | 230 kV | Wood Pole |

- Any change to an existing transmission line will utilize like structures and assemblies to maintain consistency.

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### 5.5.1 Structure Design

- The tower weights are estimated based on weights provided in NALCOR Dwg. No. 220-T-222.
- The foundations are assumed to be grillage type foundations for each tower.
- All wood pole structures will be Class 1 poles ranging from $15.4 \mathrm{~m}(50 \mathrm{ft})$ to $24.6 \mathrm{~m}(80 \mathrm{ft})$ in length.
- Wood poles will be direct embedded with the addition of guying, if required.
- No long-span or special crossing structures are included.


### 5.5.2 Centerline / Layout

- The center line and layout proposed by SLI was selected to minimize the cost and impact to the existing lines.
- The survey data used for the preliminary layout was provided by Nalcor and based on 2010 LiDAR survey and orthophotography.


### 5.5.3 Quantities of Structures and Foundation Steel

- The quantity of towers/wood poles estimated includes all standard structures, body extensions, and leg/mast extensions, including nuts, bolts, plates, washers, and attachment vangs, as per the design drawings, specifications and other contract documents.
- The quantities of steel towers/wood poles are based on preliminary ( $40 \%$ complete) design.
- Material extras for spares, un-foreseen re-routes, structure additions, design changes, etc. are not included.
- The quantities for the steel grillage are estimated based on the preliminary design and layout.

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### 5.5.4 Quantities for Conductor Hardware Assemblies

- The quantities of hardware assemblies ate based on total structure quantities from the preliminary centerline/layout.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.5.5 Quantities of Insulators

- The quantities of insulators are based on total structure quantities from the preliminary centerline/layout.
- The strength and type of insulator selected for each line is listed in Table 2.
- Porcelain or toughened glass insulators are assumed to be acceptable in the estimate. The quantity and strength of the insulators will match that of the existing line.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.

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Table 2 : Quantity of Insulators for each line to be modified

| Modification No. | Line to be modified | kV level | Insulator Type | insulator Quantity |
| :---: | :---: | :---: | :---: | :---: |
| 1 | TL251 | 69 kV | Tangent (line Post) | 6 |
|  |  |  | DE ( 6 bells - 111 kN ) | 72 |
|  |  |  | Jumper (line Post) | 6 |
| 2 | TL232 | 230 kV | Tangent ( 14 bells - 111 kN ) | 84 |
|  |  |  | DE ( 16 bells -111 kN ) | 576 |
|  |  |  | Jumper ( 14 bells 111 kN ) | 126 |
| 3 | TL204 | 230 kV | DE (16 bells - 111 kN ) | 192 |
|  |  |  | Jumper ( 14 bells 111 kN ) | 42 |
| 4 | NFP | 138 kV | DE ( 9 bells - 111 kN ) | 324 |
|  |  |  | Jumper ( 8 bells - 111 kN ) | 72 |
| 5 | NFP | 138 kV | DE ( 9 bells - 111 kN ) | 324 |
|  |  |  | Jumper ( 8 beils - 111 kN ) | 72 |
| 6 | TL201 | 230 kV | Tangent ( 14 bells - 111 kN ) | 42 |
|  |  |  | DE (16 bells - 111 kN ) | 576 |
|  |  |  | Jumper ( 14 bells 111 kN ) | 126 |

### 5.5.6 Quantities of Conductor and OHSW

- The quantity of conductor and OHSW is based on the linear line length, with an additional $4 \%$ included for sag and wastage.
- Table 3 outlines the existing types of conductor and OHSW required for each line modification.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.

Table 3: Exlsting Conductor and OHSW Type

| Modification <br> No. | Line to be <br> modified | kV level | Conductor / OHSW Type |
| :---: | :---: | :---: | :---: |
| 1 | TL251 | 69 kV | Single 266 Partridge ACSR |
|  | No OHSW |  |  |
| 2 | TL232 | 230 kV | Single 1192.5 Grackle ACSR |
|  |  | No OHSW |  |


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| 3 | TL204 | 230 kV | Single 1192.5 Grackle ACSR |
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|  |  |  | $1 / z^{\prime \prime}$ Steel Grade 220 OHSW |
| 4 | NFP | 138 kV | Single 397 Ibis ACSR |
|  |  |  | No OHSW |
|  | 5 | NFP | Single 397 Ibis ACSR |
| 6 | TL201 | 230 kV | No OHSW |
|  |  |  | No OHSW |

### 5.5.7 Quantities of Conductor Accessories

- It is assumed that compression type splices, dead-ends and jumper connectors will be used for each line modification.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.5.8 Quantities of Miscellaneous Hardware and Material

- The hardware required for structure grounding is included.
- One structure number tag will be installed on every structure.
- Two danger signs will be installed on every structure.


### 5.5.9 Geotechnical Investigations

- The cost of soil compaction testing is included.


### 5.6230 kV RE-TERMINATIONS AT THE FUTURE SOLDIER'S POND SUBSTATION

There are four existing transmission lines that will need to be reconfigured at the future Soldier's Pond substation site to accommodate the new $\pm 350 \mathrm{kV}$ HVdc transmission line (See Drawing No. ILK-SW-CD-4500-CV-PL-0001-01). See Table 4 for the list of lines that will need to be reconfigured:

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Table 4: Lines to be reconfigured at Soldier's Pond

| Line No. | kV level | Structure Types |
| :---: | :---: | :---: |
| TL201 | 230 kV | Wood Poles |
| TL217 | 230 kV | Single Circuit Towers |
| TL218 | 230 kV | Single Circuit Towers |
| TL242 | 230 kV | Wood Poles |

- Any change to these existing transmission lines will utilize like structures and assemblies to maintain consistency.


### 5.6.1 Structure Design

- The estimated tower weights are estimated based on the weights provided in Nalcor Dwg. No. 220-T-222.
- The foundations are assumed to be grillage type foundations for each tower.
- All wood poles will be Class H 1 poles ranging from $18.5 \mathrm{~m}(60 \mathrm{ft})$ to $24.6 \mathrm{~m}(80 \mathrm{ft})$ in length.
- The wood poles will be direct embedded with the addition of guying, if required.
- No long-span or special crossing structures have been considered.


### 5.6.2 Hardware Assemblies

- The hardware assemblies will be designed to match those of the existing transmission line assemblies in strength and function.


### 5.6.3 Engineering Studies and Front End Engineering

- Geotechnical investigation is not included.

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### 5.6.4 Centerline / Layout

- The centerline and layout has been established to accommodate the new Soldier's Pond substation while minimizing the cost and impact to the existing transmission lines.
- It is assumed that there is flexibility to modify the centerline and PI location in an effort to optimize the line layout.
- The survey data used for preliminary layout was provided by Nalcor and based on 2010 LiDAR survey and orthophotography.


### 5.6.5 Quantities of Towers / Wood poles and Foundation Steel

- The quantity of structures estimated includes all standard structures, body extensions, and leg/mast extensions, including nuts, bolts, plates, washers, and attachment vangs, as per the design drawings, specifications and other contract documents.
- The quantities of steel towers are based on preliminary PLS-CADD spotting.
- Material extras for spares, un-foreseen re-routes, structure additions, design changes, etc. are not included.
- The quantities of steel grillage, guy wire and anchors are estimated based on the preliminary design and layout. The guy wire length is assumed to be 40 m per guy, four guys per steel tower.


### 5.6.6 Quantities for Conductor and OHSW Hardware Assemblies

- The quantity of hardware assemblies is based on total structure quantities from the preliminary centerline/layout.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.

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### 5.6.7 Quantities of insulators

- The quantity of insulators is based on total structure quantities from the preliminary centerline/layout.
- The tangent structure will use single "l" string insulators per phase, per tower.
- The dead-end structure will use double strain insulator sets per phase, per tower.
- Porcelain or toughened glass insulators are assumed to be acceptable. The quantity and strength of insulators will match those of the existing structures along the line to maintain consistency.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.6.8 Quantities of Conductor and OHSW

- A single 804 kcmil , Aluminum Alloy Conductor Steel Reinforced Trapezoidal Wire (AACSR / TW) will be used as the pole and jumper conductor for each circuit. The quantity is based on the linear line length, with an additional $4 \%$ included for sag and wastage.
- Two $1 / 2^{\prime \prime}$ Grade 220 OHSW, will be used on each circuit for lightning protection. The quantity is based on the linear line length, with an additional $4 \%$ included for sag and wastage.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.6.9 Quantities of Conductor Accessories

- $100 \%$ of the line has been considered for compression type splices, dead-ends and jumper connectors.
- Conductor splices will be installed approximately every 1800 m .
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.

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### 5.6.10 Quantities of OHSW Accessories

- Dampers are assumed to be Stockbridge type, two per structure.
- Bird diverters will not be required, and are not included in the estimate.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.6.11 Quantities of Miscellaneous Hardware and Material

- The hardware required for structure grounding is included.
- Aerial structure number boards will be installed on the first structure outside of the substation.
- One structure number tag will be installed on every structure.
- Two danger signs will be installed on every structure.
- Aerial line number boards will be included per line, and will be installed on the first structure outside of the substation.


### 5.6.12 Electrical Effects / Considerations

- The 230 kV re-terminations will maintain a ROW width that will match that of the existing 230 kV line.


## $5.7 \quad 735 \mathrm{kV}$ HVac INTERCONNECTION

Two new 0.6 km of 735 kV HVac transmission lines will be required between the existing 735 kV Churchill Falls switchyard and the future 735 kV switchyard extension (See drawing No. MFA-SW-CD-4100-CV-PL-0001-01).

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### 5.7.1 Structure Design

- For estimating purposes, SLI has used the tower types and weights provided in document created by HATCH, titled "AC1020 - Tower Type Selection, 735 kV ".
- Tangent towers shall be tower type "NFGA", a guyed $V$ lattice tower.
- Dead-end towers shall be tower type "NFBL", a rigid self supporting tower with four legs.


### 5.7.2 Hardware Assemblies

- The hardware assemblies will match those of the existing 735 kV transmission lines.
- The tangent towers shall have two double " l " string insulators and one " $V$ " string insulator per tower.
- Dead-end towers shall have four strain insulator strings, per phase, per tower.
- Jumpers shall be "V" string insulators.


### 5.7.3 Centerline / Layout

- This estimate is based on the most efficient center line connection between the future addition to the existing 735 kV Churchill Falls switchyard and the future $735 \mathrm{kV} / 315 \mathrm{kV}$ Churchill Falls Switchyard (SLI Doc. No. 505573-480B-41DD-0001).
- The survey data used for the preliminary layout was provided by Nalcor and based on 2010 LiDAR survey and orthophotography.


### 5.7.4 Quantities of Towers and Foundation Steel

- The quantity of towers estimated includes all basic/standard towers, body extensions, and leg/mast extensions, including nuts, bolts, plates, washers, and attachment vangs, as per the design drawings, specifications and other contract documents.
- The quantity of towers is based on preliminary PLS-CADD spotting.

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- Material extras for spares, un-foreseen re-routes, structure additions, design changes, etc. are not included.
- The quantities of steel grillage, guy wire, and anchors are estimated based on the preliminary design and layout. The guy wire length is assumed to be 60 m per guy, four guys per tangent tower.


### 5.7.5 Quantities for Conductor, OHSW and OPGW Hardware Assemblies

- The quantity of hardware assemblies is based on total tower quantities from the preliminary centerline/layout.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.7.6 Quantities of Insulators

- The quantities of insulators are based on total tower quantities from the preliminary centerline/layout.
- Porcelain or toughened glass insulators are assumed to be acceptable.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.7.7 Quantities of Conductor and OHSW / OPGW

- Four-bundle 54/19 ACSR, "Plover" will be used as the phase and jumper conductor. The quantity is based on the linear line length, with an additional $4 \%$ included for sag and wastage.
- One $9 / 16^{n}$ grade 220 steel OHSW will be installed on each of the 735 kV lines. The quantity is based on the linear line length, with an additional $2 \%$ included for sag and wastage.

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- One OPGW, 24 fibres cable, will be installed on each 735 kV line. The quantity is based on the linear line length with an additional $5 \%$ extra included for sag, down leads, splices, and wastage.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.7.8 Quantities of Conductor Accessories

- Spacer dampers for quad bundled conductor are assumed to be installed every 60 m per phase and are assumed to be adequate for the damping requirements of the line.
- $100 \%$ of the line has been considered for compression type splices, dead-ends and jumper connectors.
- Rigid spacers will be used on jumper conductors, assuming six spacers per phase, per jumper.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.7.9 Quantities of OPGW Accessories

- OPGW down lead clamps have been assumed to be required every 3 m .
- Two vibration dampers per structure will be used on the OPGW, per the tower quantity estimation.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.7.10 Quantities of OHSW Accessories

- Two vibration dampers per structure will be used on the OHSW, per the tower quantity estimation.
- $100 \%$ of the line has been considered for compression type splices.

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- Bird diverters are not required, and are not included in the estimate.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.7.11 Quantities of Miscellaneous Hardware and Material

- The hardware required for tower grounding is included.
- One structure number tag will be installed on every structure.
- Two danger signs will be installed on every structure.


### 5.8315 kV HVac INTERCONNECTION AT MUSKRAT FALLS SUBSTATION

Four $0.5 \mathrm{~km}, 315 \mathrm{kV}$ HVac single circuit transmission lines will be required for the interconnection between the powerhouse and the switchyard at the Muskrat Falls Substation (Drawing No.MFA-SN-CD-4300-CV-PL-0001-01).

### 5.8.1 Tower Design and Testing

- This interconnection will utilize the same 315 kV lattice steel tower family developed specifically for the LCP project. The tower design criteria is based on the document " 315 kV HVac Tower Design Criteria (SLI Doc.505573-361B-43EC-0001)".
- The four lines will use the $D$ and $E$ type towers to complete the interconnection for this 50 mm radial ice loading zone.
- All tower weights are estimated based on tower designs completed by SLI.


### 5.8.2 Hardware Assemblies and Testing

- The interconnection will use the same hardware assemblies designed for the $250 \mathrm{~km}, 315 \mathrm{kV}$ HVac line from MF to CF.

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- All 315 kV assemblies will use reduced-corona hardware.
- The hardware assembly prototype testing is included, along with witness testing by SLI.
- Third party inspection during manufacturing has been included.


### 5.8.3 Centerline/Layout

- This estimate is based on the center line and layout that was established to facilitate the spans required to connect the new powerhouse to the 315 kV switch yard at the Muskrat Falls Substation.
- It is assumed that there is flexibility to modify the centerline and PI location in an effort to optimize the line layout.
- The survey data used for preliminary layout was provided by Nalcor and based on 2010 LiDAR survey and orthophotography.


### 5.8.4 Quantities of Towers and Foundation Steel

- The quantity of towers estimated includes all basic/standard towers, body extensions, and leg/mast extensions, including nuts, bolts, plates, washers, and attachment vangs, as per the design drawings, specifications and other contract documents.
- The quantity of towers is based on preliminary PLS-CADD spotting.
- Material extras for spares, un-foreseen re-routes, structure additions, design changes, etc. are not included.
- Steel grillage foundations will be used for these towers.


### 5.8.5 Quantitles for Conductor, OHSW and OHSW Hardware Assemblies

- The quantities of hardware assemblies are based on total tower quantities, from the preliminary centerline/layout.

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- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.8.6 Quantities of Insulators

- The quantities of insulators are based on total tower quantities, from the preliminary centerline/layout.
- Porcelain or toughened glass insulators are assumed to be acceptable. The quantity and strength of insulators is based on the document titled: " 315 kV HVac Line Design Criteria (SLI Doc.505573-361C-4ZEC-0001)".
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.8.7 Quantities of Conductor and OHSW / OPGW

- Two-bundle $795 \mathrm{kcmil}, 26 / 7$ ACSR "Drake", will be used as the phase and jumper conductor. The quantity is based on the linear line length, with an additional 4\% included for sag and wastage.
- One OHSW will be installed on each line, using $1 / 2^{\prime \prime}$ grade 220 steel. The quantity is based on the linear line length, with an additional $2 \%$ included for sag and wastage.
- One OPGW, 24 fibre cable, will be installed on each line, the quantity is based on the linear line length with an additional $5 \%$ extra included for sag, down leads, splices, and wastage.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.8.8 Quantities of Conductor Accessories

- Spacer dampers are assumed to be installed every 60 m , per phase, and are assumed to be adequate for the damping requirements of the line.

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- $100 \%$ of the line has been considered for compression type splices, dead-ends and jumper connectors.
- Rigid spacers will be used on jumper conductors, assuming six spacers, per phase, per jumper.
- One jumper assembly, per phase, per tower type $D$ and $E$ is included.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.8.9 Quantities of OPGW Accessories

- Two spiral vibration dampers per structure, will be used on the OPGW as per the tower quantity estimation.
- OPGW down lead clamps have been assumed to be required every 3 m .
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.


### 5.8.10 Quantities of OHSW Accessorles

- Two spiral vibration dampers, per structure will be used on the OHSW as per the tower quantity estimation.
- The bonding conductor is assumed to be \#2 ACSR "Sparrow" and the length is estimated to be 1.5 m for suspension towers and 2.0 m for the dead-end structures.
- $100 \%$ of the line has been considered for compression type splices.
- Bird diverters are not required and are not included in the estimate.
- Material extras for un-foreseen re-routes, structure additions, design changes, etc. are not included.

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### 5.8.11 Quantities of Miscellaneous Hardware and Material

- The hardware required for tower grounding is included.
- One structure number tag will be installed on every structure.
- Two danger signs will be installed on every structure.
- Aerial line number boards will be included per line, and will be installed on the first structure outside of the Muskrat Falls Substation.


### 5.8.12 Geotechnical Investigations

- Geotechnical investigation is not included.


### 5.8.13 Electrical Effects / Considerations

- Transmission line ROW is 50 m , which is assumed to be within the acceptable limits for:
- Edge of right of way electric / magnetic field levels,
- Edge of right of way audible noise levels, and
- Edge of right of way radio and television interference.


### 5.8.14 Distribution and Transmission Line Conflicts

- It is assumed that no line crossings will be required for this 315 kV interconnection.


## 6 PROCUREMENT ASSUMPTIONS

- The prices for lattice steel towers, foundation steel grillages, rock anchor and anchor bolts, conductor, insulators, grounding material, OHSW, OPGW and accessories, guy wires, hardware fittings for conductor, insulator, OHSW, and guy wire and poles are based on budget prices received from potential suppliers.
- Allowances have been made for inspection visits

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- Allowances are included for type tests of insulator strings and OPGW. Eight full scale tower tests (two for HVac and six for HVdc ) are also included.


### 6.1 REFERENCES

- List of bulk material - 315kV HVac Engineering Quantity tracking ( SLI Doc. No. 500573-4600-33RA-I-0001)
- List of bulk material - 350kV HVdc Engineering Quantity tracking ( SLI Doc. No. 500573-4600-33RA-1-0002)


## 7 CONSTRUCTION ASSUMPTIONS

### 7.1 OVERVIEW

### 7.1.1 Component 4 Construction Estimates

The assumptions reviewed in this document refer to the following estimates that are contained in the appendix:

- One estimate for the HVac clearing and line construction,
- Four estimates for the HVdc clearing and line construction,
- Estimate for the two wood pole electrode lines,
- Estimate for required modifications to existing lines that will be crossed by the HVdc line in the Avalon Peninsula package,
- Estimate for re-terminating existing 230 kV lines at the proposed Soldiers Pond station,
- Estimate for a 735 kV connection at Churchill Falls, and
- Estimate for 315 kV interconnections at Muskrat Falls (powerhouse).


### 7.1.2 Included in the Estimates

- The quantities of construction work involved as provided in the engineering estimates.

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- The crew sizes required and the productivity rates associated with completing the construction work. The labour rates are based on information provided by the client with modifications for specialists, such as linemen.
- Material handling and transportation.
- Survey work.
- Geo-technical investigations.
- Management and administration costs including supervision; safety and environmental monitoring; and quality and cost control.
- Accommodation for on-site employees based on installation cost of $\$ 50,000$, per camp bed, and a daily cost of $\$ 150$, per person.
- Travel for employees while on site and at the end of the rotation based on a $21 / 7$ schedule.
- Contractor target of $15 \%$ profit.
- Contractor Insurance of $1 \%$.
- Contractor bonding of $1 \%$.


### 7.1.3 Not Included in the Estimates

- Switching and outage costs related to Nalcor and other utility companies.
- Line inspections conducted by Nalcor and other utility companies.
- Salvage costs for TL240 between Happy Valley and Churchill Falls.
- Environmental field visits for obtaining site information, etc. for regulatory compliances including stream crossings, etc.
- SLI EPCM costs including civil material testing lab and services.
- Insurance for Nalcor supplied materials.

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### 7.1.4 Special Items

### 7.1.4.1 Helicopter Costs

Helicopters will be used extensively on Component 4 of the LCP. SLI and Nalcor will use small helicopters (three to five passengers) for supervision and to assist with medical evacuations and fire suppression. Geo-technical consultants will use small and medium helicopters to transport personnel and equipment for soil investigation. Construction contractors will use all sizes of these machines including heavy lift helicopters for setting towers, transporting men and equipment, and for stringing operations.

The cost for the helicopter usage is included in the construction assumptions that follow, or in the separate EPCM estimates. The rates used in the estimates for helicopters are in the following table:

## Table 5: Rates used in the EstImates for Helicopters

| Small Machines <br> AStar, 206LR (4 or 5 passengers; light loads of <br> material and tools) | $\$ 2,000 / \mathrm{hr}$ |
| :--- | :--- |
| Medium Machines | $\$ 3,500 / \mathrm{hr}$ |
| to |  |
| Various helicopters with capacity for 5 to 15 | to <br> passengers or a lift capacity of 3300 to 9000 lb |
| Heavy Lift Machines | $7,000 / \mathrm{hr}$ |
| Erickson Air-Crane S64E (20,000 lb lift) | $\$ 14,500 / \mathrm{hr}$ |
| Erickson Air-Crane S64F (25,000 lb lift) | $\$ 17,000 / \mathrm{hr}$ |

### 7.1.4.2 Material Marshalling

A logistics study is underway that will help to plan the management of the transmission line materials. The construction estimates are currently based on the assumption that there will be main marshalling yards established west of Happy Valley, near Corner Brook, and on the Avalon Peninsula. Based on this model, the line contractors will be responsible for transporting the material from these main yards to the transmission line, using temporary lay-down locations, as necessary.

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### 7.1.4.3 Site Offices and Accommodations

The contractors will be responsible for establishing their own accommodation and office facilities. Exceptions include:

- Using the Accommodation Complex planned for the Muskrat Falls site during the construction of the first few kilometres of the HVdc line.
- Using space at a proposed marshalling yard/office/accommodation complex that would be built west of Happy Valley.
- Using a free-issued camp that could be provided to a contractor for the HVac line.

For all camps established by the contractors, they will be obligated to provide accommodations and office space to SLI and the client. These spaces would be used by managers, engineers, inspectors/lab techs and HS \& E staff.

### 7.1.5 References

- Refer to Part 4 of the Construction Management Plan (SLI Doc. No. 505573-0000-30PL-1-0003) for detailed descriptions of the construction packages, line route conditions and schedule.
- Clearing Estimation Costs - HVac Lines (SLI Doc. No. 500573-4600-40RA-I-0001).
- Clearing Estimation Costs - HVdc Lines (SLI Doc. No. 500573-4600-40RA-I-0002).


### 7.2 315 KV HVac LINE CONSTRUCTION

### 7.2.1 Construction Quantities

As identified in section $4.1-315 \mathrm{kV}$ HVac Transmission Line, LIDAR survey information and aerial photography has been used to define the corridor for the two 315 kV circuits and to spot the tower types and heights that meet the design criteria. The dimensions of the corridor have been used to estimate the labour costs of clearing the right-of-way. The quantities of the various towers and foundations have been used to estimate the labour costs of constructing the line.

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### 7.2.2 Access

Accessibility to the two HVac lines is fairly well understood.

- The line route crosses the Trans Labrador Highway (TLH) twenty times, providing access to all of the work areas.
- Field investigation has taken place to review points of inflection and other areas of concern.
- A desk-top review of aerial mapping has been used to complete the tower spotting. It is assumed that no significant changes will be required.
- Based on the current assessment of access requirements, all structures can be accessed by a combination of:
- Existing roads and trails,
- Minor grading work, removal of small amounts of deadfall, stumps, rocks and other debris,
- Installation of culverts and temporary bridges, and
- If required, winter roads or frozen conditions for a small number of locations.

It is assumed that the TLH, including all bridges, etc. will provide unobstructed access for the project.

### 7.2.3 Survey

- The completed LIDAR survey-was not part of the SLI scope of work.
- The costs associated with marking the boundaries of the right-of-way prior to clearing and the staking of the structure centres will be completed by SLI as part of the EPCM agreement.
- The staking of the structure foundations and survey of the as-built locations of the completed foundations will be the responsibility of the line contractor and is included in the estimate.
- A post-construction legal survey of the right-of-way is not included in the estimate.

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### 7.2.4 Clearing and Access Construction

- A clearing and access study has identified tree densities and the locations where culverts and temporary crossings need to be installed. (A copy of the study is attached.) The study also identifies where off-right-of-way access is required.
- Environmental constraints have been identified and accounted for in the execution of clearing and access construction work. Approximately $1 \%$ of the clearing and access estimate is earmarked for environmental mitigation.
- Estimated costs of clearing are based on experience from previous projects and are proportional to vegetation density. It is assumed that $89 \%$ of the clearing will be completed mechanically (feller-bunchers, mulchers), $7 \%$ will be cleared by hand (chain saws) and the remaining $4 \%$ will not require tree removal.
- The cost of removing access to the right-of-way following completion of construction has been included in the estimate.


### 7.2.5 Foundation Construction

- The location and types of foundations have been based on a preliminary study and a report by AMEC engineers. In addition, a desk-top study using a bare earth model was used to determine the likely type of foundation at each tower site.
- Site-specific foundation types will be reviewed and adjusted through a geo-tech survey to be undertaken as tree clearing work in being completed. It is assumed that this survey will not significantly change the quantities of the foundation types that are used for the construction estimate. The cost of the geotechnical survey is included in the estimate.
- It is assumed that the majority of anchors for guyed towers will be drilled to a depth of 10 metres.
- During construction, inspection and testing of the soil conditions encountered during excavations will confirm the foundation type that is being used for each tower. This may result foundation type changes that requires transport of different foundation steel on and off site. A

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unit price for these possible changes will be included in the tender packages. For the construction estimate, it is assumed that this will be a rare occurrence.

- It is assumed that all tower sites will be accessible by ground transportation. A small number of locations may require the contractor to take advantage of frozen conditions in the winter.
- Estimated costs associated with the installation of each of the foundation types are determined by previous experience with similar foundation that includes labour, equipment and material such as concrete and backfill.


### 7.2.6 Tower Assembly and Erection

- It is anticipated that all tower sites will be accessible by ground transportation. This includes hauling tower steel and the movement of cranes that are large enough to set the towers.
- Estimated costs associated with the assembly and erection of each of the tower types are determined by previous experience with similar projects. Tower weights are a determining factor.


### 7.2.7 Stringing - Conductor, OPGW and OHSW

- It is assumed that all tower sites will be accessible by cranes with man-baskets.
- It is expected that the contractor will use a small helicopter for stringing lead-lines. They will employ tension stringing techniques.
- The cost of installing rider poles at twenty highway crossings and four line crossings is included in the estimate. As well, the planning and precautions associated with safely completing the stringing across these crossings is included.
- It is assumed that no modifications or line outages will be required on TL240. Recloser blocking will be required.
- Reel lengths of about 3000 m will be used for conductor and OHSW. Two-bundle, Drake conductor will be used and spacer dampers will be installed.

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- Reel lengths of about 6000 m will be used for the OPGW. Approximately 45 splices will be installed in each line.
- Estimated costs associated with stringing are determined by previous experience on similar projects.


### 7.2.8 Counterpoise

- It is assumed that the line route will be accessible for the installation of the counterpoise and related grounds and connections.


### 7.2.9 Continuity of Construction

It is unlikely that the HVac lines can be built consecutively from one end to the other. However, it is assumed that there will not be significant costs due to demobilizations or frequent transfers of men and equipment from one section of line to another.

## 7.3 $\mathbf{~} 350$ KV HVdc LINE CONSTRUCTION

### 7.3.1 Construction Quantities

As identified in section 4.2 - $\pm 350 \mathrm{kV}$ HVdc Transmission Line, ten families of towers are being designed to accommodate the conditions that will be met on the proposed transmission line between Muskrat Falls and Soldiers Pond. LIDAR survey information and aerial photography have been used to define the route and to make an initial pass at spotting towers. The initial estimate of quantities of foundations that are required is based on the proportion of foundation types proposed for the HVac lines.

### 7.3.2 Contract Packages

For contract bidding purposes, the HVdc line route has been divided into four packages. An independent estimate for clearing and line construction has been created for each package. The

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productivity rates for each estimate are based on the travel distances, weather conditions and access requirements within each package.

For each estimate, the dimensions of the corridor and approximate tree densities have been used to estimate the labour costs of clearing the right-of-way. The tower quantities within each package have been used to estimate the labour costs of foundation installation, tower assembly, setting and stringing.

### 7.3.3 Access

A high-level desk-top study and helicopter surveys of portions of the line route have been used to provide a good estimation of the accessibility to all portion of the HVdc line route. The estimates for access requirements are based on the following observations:

- Most of the line route on the island of Newfoundland is accessible from existing roads that cross the line, dividing it into manageable segments.
- The portion of line through the Long Range Mountains has been estimated for helicopter access for all phases of work.
- The portion of line going north from the south coast of Labrador has been estimated for helicopter access for all phases of work.
- The line route across the interior of Labrador from Muskrat Falls to the Bujeault River is remote but there should be access to the majority of structures. However, there are few access points to this portion of line and it is proposed that approximately 45 km of class 1 road be built to the south-east end of this section. As well, the access road along the right-of-way will have to be built and maintained to accommodate the traffic that will need to travel. One central portion of the line will likely be accessible only with ice bridges during the winter.

The estimates account for all of these identified conditions.

### 7.3.4 Survey

- The completed LIDAR survey was not part of the SLI scope of work.

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- The costs associated with marking the boundaries of the right-of-way prior to clearing and the staking of the structure centres will be completed by SLI as part of the EPCM agreement.
- Staking of the structure foundations and survey of the as-built locations of the completed foundations will be the responsibility of the ine contractor and is included in the estimate.
- A post-construction legal survey of the right-of-way is not included in the estimate.


### 7.3.5 Clearing and Access Construction

- A high level clearing and access study for the proposed HVdc line route has been used to approximate tree densities and to estimate the work required to establish access along the right-of-way. The study also identifies the existing access available and the amount of off-right-ofway access that is required for clearing and line construction.
- It is assumed that the majority of environmental constraints have been identified and accounted for in the estimate of clearing and access construction work. Approximately $1 \%$ of the clearing and access estimate is earmarked for environmental mitigation.
- Estimated costs of clearing are based on experience from previous projects and are proportional to vegetation density. It is assumed that $79 \%$ of the clearing will be completed mechanically (feller-bunchers, mulchers), $19 \%$ will be cleared by hand (chain saws) and the remaining $2 \%$ will not require tree removal.
- The cost of removing access to the right-of-way following completion of construction has been included in the estimate.


### 7.3.6 Foundation Construction

- As indicated, the initial quantities and sizes of HVdc tower foundations have been estimated by using amounts that are proportional to the HVac design. It is assumed that as engineering work progresses, the final foundation designs will not cause a significant change in the construction estimate.

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- It is assumed that the majority of anchors for guyed towers will be drilled to a depth of 10 metres.
- During construction, inspection and testing of the soil conditions encountered during excavations will confirm the foundation type that is being used for each tower. This may result foundation type changes that requires transport of different foundation steel on and off site. A unit price for these possible changes will be included in the tender packages. For the construction estimate, it is assumed that this will be a rare occurrence.
- Access to tower sites for foundation installation will vary considerably throughout the HVdc line. The variability is accounted for within each estimate. This includes some areas where men and equipment will have to be transported by helicopter.
- Estimated costs associated with the installation of each of the foundation types are determined by previous experience with similar foundation. The estimates include labour, equipment and material such as concrete and backfill.


### 7.3.7 Tower Assembly and Erection

- Access to tower sites for tower assembly and erection will vary considerably throughout the HVdc line. The majority of towers will be assembled at the tower sites and set by crane. Some of these locations will require winter access. Two large areas (southern Labrador and the Long Range Mountains in the Northern Peninsula) will require the use of helicopters for setting towers. One or two shorter sections may require helicopter setting as well. The cost of setting towers under these conditions is included in the estimates.
- Estimated costs associated with the assembly and erection of each of the tower types are determined by previous experience with similar projects.


### 7.3.8 Stringing - Conductor and OPGW

- It is assumed that the majority of tower sites will be accessible by cranes with man-baskets. It is also assumed that the areas where towers are set by helicopter will require crews to work off the towers without man-lifts and be transported by helicopter.

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- It is expected that the contractor will use a small helicopter for stringing lead-lines. He will employ tension stringing techniques.
- The cost of installing rider poles at highway crossings and line crossings is included in the estimate. As well, the planning and precautions associated with safely completing the stringing across these crossings is included.
- Modifications to existing circuits will be required is some cases and referenced below.
- Reel lengths of about 1200 m will be used for conductors.
- Reel lengths of about 6000 m will be used for the OPGW.
- Estimated costs associated with stringing are determined by previous experience on similar projects.


### 7.3.9 Counterpoise

- The installation of counterpoise will require a variety of forms of transportation. This is included in the estimate.


### 7.3.10 Continuity of Construction

Within each package of the HVdc line, contractors will be challenged to maintain a high level of productivity from their work-forces. It is unlikely that any package can be built consecutively from one end to the other. However, it is assumed that there will not be significant costs due to demobilizations or frequent transfers of men and equipment from one section of line to another.

### 7.4 MISCELLANEOUS PACKAGES

### 7.4.1 Additional Work - LCP Transmission System

The following sub-projects are required to complete the proposed transmission system:

- Two electrode lines

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- Modifications to existing lines for crossings in the fourth section of the HVdc line
- 230 kV line re-terminations at Soldiers Pond
- 735 kV interconnection at Churchill Falls
- 315 kV interconnection at Muskrat Falls (Powerhouse)

These sub-projects are being developed as separate engineering packages but will be included with the larger bid packages when they are tendered. Not included is the 25 kV Construction Power subproject.

The cost estimates to construct these packages were developed as follows:

- Based on experience, the crew size and equipment requirements were identified. Labour rates, equipment costs, indirect costs and overhead costs used for the major construction components were applied.
- The estimated number of crew days required to complete each sub-project is based on previous projects of similar scope.
- Access and clearing costs, if any, are based on a review of aerial mapping
- Outages and the extra time required to cross other circuits or roads is included in the estimate of crew days required. It is assumed that no significant delays will be encountered

It is assumed that there will be no major changes to the scope or location of these projects.

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Appendix 1

| Level 1 | Level 2 | Level 3 | Level 4 | Level 5 | Level 6 | Level7 | Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6000000 |  |  |  |  |  |  | No Physical Component |
|  | 5100100 |  |  |  |  |  | Indrect C-1 |
|  |  | 5100101 |  |  |  |  | Overall Project Management |
|  |  | 5100102 |  |  |  |  | Construction Management |
|  |  | 5100103 |  |  |  |  | Engineering Power Piant |
|  |  | 5100104 |  |  |  |  | Engineering Const Support PPlant |
|  |  | 5100105 |  |  |  |  | Engineering Management T.L. |
|  |  | 5100106 |  |  |  |  | Engineering Support T. L. |
|  |  | 5100107 |  |  |  |  | Engineering DC Speciaities |
|  |  | 5100108 |  |  |  |  | Procurement |
|  |  | 5100109 |  |  |  |  | Contract Management |
|  |  | 5100199 |  |  |  |  | Other Allowances / Indlrects |
|  | 5100300 |  |  |  |  |  | Indirect C-3 |
|  |  | 5100301 |  |  |  |  | Churclli Fails - Site management |
|  |  | 5100302 |  |  |  |  | Substation Muskart AC and DC - Site management |
|  |  | 5100303 |  |  |  |  | Muskrat Falls - Substation Tap 3t5/1/38/25kv - Site |
|  |  | 5100304 |  |  |  |  | Forteau Point - Transilton compounds - Slie manage |
|  |  | 5100305 |  |  |  |  | L'Anse-au-Dlable - Electrode - Slie management |
|  |  | 5100306 |  |  |  |  | Shoal Cove - Transition compounds - Site mgmt |
|  |  | 5100307 |  |  |  |  | Soldiers Pond DC Converter Station - Slie Mgmt |
|  |  | 5100308 |  |  |  |  | Solders Pond AC Substation - Stie Mgmt |
|  |  | 5100309 |  |  |  |  | Solders Pond - Symihronous condensers -Site Mgmt |
|  |  | 5100310 |  |  |  |  | Dowden's Point - Electrode - Site management |
|  |  | 5100311 |  |  |  |  | Traininig Personnal (Based al Si-Johns) |
|  |  | 5100312 |  |  |  |  | Construction Substation-Management - Slite St-John |
|  |  | 5100313 |  |  |  |  | ENGINEERING SUPPORT FOR DC SPECIALTIES |
|  |  | 5100399 |  |  |  |  | Other Allowances//indirects |
|  | 5100400 |  |  |  |  |  | Indirect C-4 |
|  |  | 5100401 |  |  |  |  | Engineering Mgmt T. L. |
|  |  | 5100402 |  |  |  |  | Project Management - St-Johns Stie |
|  |  | 5100499 |  |  |  |  | Indirect/Others |
| 10000000 |  |  |  |  |  |  | Support Faclilites - General |
|  | 11000000 |  |  |  |  |  | Access - General |
|  |  | 11100000 |  |  |  |  | Access Roads |
|  |  |  | 11100100 |  |  |  | Access Roads - Construction/Temporary |
|  |  |  | 11100200 |  |  |  | Access Roads - Permanent |
|  |  |  | 11100300 |  |  |  | Access Roads - North Spur |
|  |  | 11500000 |  |  |  |  | Construction Bridge over splliway approach channel |
|  |  | 11600000 |  |  |  |  | Barge / Ferry Access |
|  | 13000000 |  |  |  |  |  | Construction Power General |
|  |  | 13200000 |  |  |  |  | Constructlon Power - Muskrat Falis |
|  |  | 13300000 |  |  |  |  | Construction Power - Island Link |
|  | 14000000 |  |  |  |  |  | Construction Telecommunications - General |
|  |  | 14200000 |  |  |  |  | Construction Telecommünications - Muskrat Fails |
|  |  | 14300000 |  |  |  |  | Construction Telecommunications - Island LInk |
|  | 15000000 |  |  |  |  |  | Accommodation Complex / Temporary Builidings |
|  |  | 15100000 |  |  |  |  | General Site |
|  |  |  | 15110000 |  |  |  | Recreational Areas |
|  |  |  | 15120000 |  |  |  | Other Specialties |
|  |  | 15200000 |  |  |  |  | Buildings - Central Core |
|  |  | 15300000 |  |  |  |  | Buildings - Dormitories |
|  |  | 15400000 |  |  |  |  | Buildings - Administration Bulldings and Workshops |
|  |  | 15500000 |  |  |  |  | Buildings - Warehousing |
|  |  | 15600000 |  |  |  |  | Buildings - Other |
|  |  | 15700000 |  |  |  |  | Site Services (infrastructure) |
|  | 16000000 |  |  |  |  |  | Temporary Staging Areas |
|  |  | 16100000 |  |  |  |  | Overburden Stockpiling area |
|  |  | 16200000 |  |  |  |  | Rock Stockpliling Area |
|  |  | 16300000 |  |  |  |  | Rock Quarry |
|  | 17000000 |  |  |  |  |  | Housing Facilities (HF) |
|  |  | 17100000 |  |  |  |  | Happy Valley-Goose Bay HF (Option) |
|  | 18000000 |  |  |  |  |  | Offite Logistics infrastructure \& Support - Gener |
|  |  | 18100000 |  |  |  |  | Offsite Marshalling Areas and Warehousing |
|  |  | 18200000 |  |  |  |  | Offislte Port Facilities |
|  |  | 18300000 |  |  |  |  | Ofisilie Roads and Bridges |
|  | 19000000 |  |  |  |  |  | Other Offices - General |
|  |  | 19100000 |  |  |  |  | Happy Valley-Goose Bay Office (Option) |
|  |  | 19200000 |  |  |  |  | Other Offices |
| 20000000 |  |  |  |  |  |  | Reservoir, Diversion, Dam and Spillway - General |
|  | 21000000 |  |  |  |  |  | Reservoir - General |
|  |  | 21100000 |  |  |  |  | Reservoir |
|  |  |  | 21100100 |  |  |  | Access Roads |
|  |  |  | 21100200 |  |  |  | Clearing |
|  |  |  | 21100300 |  |  |  | Fish HADD |
|  |  | 21200000 |  |  |  |  | Water Sampling Stations |
|  |  | 21300000 |  |  |  |  | Trash Management Sysiem |
|  |  | 21400000 |  |  |  |  | Reservoir Stabilization |
|  |  | 21500000 |  |  |  |  | Water Management System |
|  | 23000000 |  |  |  |  |  | Dams and Cofferdams - General |
|  |  |  | 23000010 |  |  |  | Riverside RCC Cofferdam |
|  |  |  |  | 23000019 |  |  | Rock Excavation - Dry Conditions |
|  |  |  |  | 23000012 |  |  | Foundation Preparation, Inclusive of Cleaning - Ro |
|  |  |  |  | 23000013 |  |  | Dental Concrete |
|  |  |  |  | 23000014 |  |  | Sluch Grout on Fondation |
|  |  |  |  | 23000015 |  |  | Slush Grout Along Joints Every $900 \mathrm{~mm}, 2 / 3$ of area |
|  |  |  |  | 23000016 |  |  | Roiler Compacted Concrete |


| Level 1 | Level 2 | Level 3 | Level 4 | Level 5 | Level 6 | Level 7 | Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 23000020 |  |  |  | Riverside Cofierdam Rockill Section |
|  |  | 23000:00 |  |  |  |  | Phase 1 Riverside Cofferdam |
|  |  | 23008990 |  |  |  |  | Indirect |
|  |  |  | 23009991 |  |  |  | Indirect 1 |
|  |  |  | 23009992 |  |  |  | Indirect 2 |
|  |  | 23200000 |  |  |  |  | North RCC Dam |
|  |  |  | 23210100 |  |  |  | Common Excavation |
|  |  |  | 23210110 |  |  |  | Rock Excavation |
|  |  |  | 23210120 |  |  |  | Driil and Pressure Grout |
|  |  |  | 23210130 |  |  |  | Foundation Preparation |
|  |  |  | 23210140 |  |  |  | Drain Holes |
|  |  |  | 23210150 |  |  |  | Dental Concrete |
|  |  |  | 23210160 |  |  |  | Slush Grout Foundation |
|  |  |  | 23210170 |  |  |  | Roller Compacted Concrate |
|  |  |  | 23210180 |  |  |  | Slush Grout Interlayer |
|  |  |  | 23210190 |  |  |  | Concrete - Upatream Face |
|  |  |  | 23210200 |  |  |  | Concrete - Downstream Face |
|  |  |  | 23210210 |  |  |  | Concrete - Cap |
|  |  |  | 23210220 |  |  |  | Formwork - Drainage Gailery |
|  |  |  | 23210230 |  |  |  | Concrete North Abument |
|  |  |  | 23210240 |  |  |  | Instrumentation |
|  |  |  | 23220200 |  |  |  | Concrete \& RCC Operations |
|  |  |  |  | 23220270 |  |  | Concrete North Abutment |
|  |  |  |  |  | 23220280 |  | Concrete North Abutment |
|  |  |  |  |  | 23220285 |  | North Abutment Formwork |
|  |  |  |  |  | 23220290 |  | Steel Relnforcement |
|  |  |  |  |  | 23220295 |  | Overbreak Concrete \& Misc. |
|  |  |  |  |  |  | 23220296 | Overbreak Concrete |
|  |  |  |  |  |  | 23220297 | Waterstop |
|  |  | 23300000 |  |  |  |  | South Rockfill Dam |
|  |  |  | 23300100 |  |  |  | Common Excavation |
|  |  |  | 23300110 |  |  |  | Drill and Pressure Grout |
|  |  |  | 233000120 |  |  |  | Foundation Preparation |
|  |  |  | 23300130 |  |  |  | Drain Holes |
|  |  |  | 23300140 |  |  |  | Dental Concrete |
|  |  |  | 23300150 |  |  |  | Siush Grout |
|  |  |  | 23300160 |  |  |  | Compacted TIII Z1 |
|  |  |  | 23300170 |  |  |  | Compacted Filter Z2 |
|  |  |  | 23300180 |  |  |  | Comp Rkill $\mathrm{z3}$, 3 L 84 |
|  |  |  | 23300190 |  |  |  | Concrete - Crest - south dam (road bed only) |
|  |  |  | 23300200 |  |  |  | Concrate - Drainage gallery |
|  |  |  | 23300210 |  |  |  | Concrale- (CVC) |
|  |  |  | 23300220 |  |  |  | Instrumentation |
|  |  | 23400000 |  |  |  |  | Cofferdams |
|  |  |  | 23410000 |  |  |  | Cofferdam- Upstream |
|  |  |  |  | 23411000 |  |  | Sollway U/S Cofferdam |
|  |  |  |  |  | 23411110 |  | Common Excavation |
|  |  |  |  |  | 23411120 |  | Dumped Rockill $0-900 \mathrm{~mm}$ |
|  |  |  |  |  | 23411130 |  | Boulders (produced by others) $1000-1200 \mathrm{~mm}$ |
|  |  |  |  |  | 23411140 |  | Boulders (produced by others) $1200-1500 \mathrm{~mm}$ |
|  |  |  |  |  | 23411150 |  | Percussions Boreholes |
|  |  |  |  |  | 23411160 |  | Cement Bentonite Wail |
|  |  |  |  |  | 23411170 |  | Jet Grout Column |
|  |  |  |  |  | 23411180 |  | Dumped Granular or Crushed Rock Max 150 mm |
|  |  |  |  |  | 23411190 |  | Fine Rockfill Transition Max 300 mm |
|  |  |  |  |  | 23411200 |  | Compacled Till - Zone 1 |
|  |  |  |  |  | 23411210 |  | Compacted Granular - Zone 2C |
|  |  |  |  |  | 23411220 |  | Compacted Rockfill - Zone 3C |
|  |  |  |  |  | 23411230 |  | Riprap (produced by others) 4 Class 1 |
|  |  |  |  |  | 23411240 |  | Dumped Rockrill (access road) 0-900mm |
|  |  |  |  |  | 23411250 |  | Dumped Till |
|  |  |  |  |  | 23411280 |  | Removal Cofferdam |
|  |  |  |  |  | 23411270 |  | Access Road Intake Channel |
|  |  |  |  | 23412000 |  |  | ND U/S Rockill Cofterdam |
|  |  |  |  |  | 23412110 |  | Common Excavation |
|  |  |  |  |  | 23412120 |  | Dumped Rock fill $0-900 \mathrm{~mm}$ |
|  |  |  |  |  | 23412130 |  | Boulders (produced by others) $1000-1200 \mathrm{~mm}$ |
|  |  |  |  |  | 23412140 |  | Boulders (produced by others) $1200-1500 \mathrm{~mm}$ |
|  |  |  |  |  | 23412150 |  | Percussions Boreholes |
|  |  |  |  |  | 23412160 |  | Cement Bentontie Wail |
|  |  |  |  |  | 23412170 |  | Jet Grout Column |
|  |  |  |  |  | 23412180 |  | Dumped Granular or Crushed Rock Max 150 mm |
|  |  |  |  |  | 23412190 |  | Fine Rockfill Transition Max 300 mm |
|  |  |  |  |  | 23412200 |  | Compacled Till - Zone 1 |
|  |  |  |  |  | 23412210 |  | Compacled Granular - Zone 2C |
|  |  |  |  |  | 23412220 |  | Compacled Rockill - Zone 3C |
|  |  |  |  |  | 23412230 |  | Riprap (produced by others) 4 Class 1 |
|  |  |  |  |  | 23412240 |  | Dumped Rockfill (access road) $0-900 \mathrm{~mm}$ |
|  |  |  |  |  | 23412250 |  | Dumped Till |
|  |  |  |  |  | 23412260 |  | Removal Cofferdam |
|  |  |  |  |  | 23412270 |  | Access Road intake Channel |
|  |  |  |  |  | 23412280 |  | Compacted rockfill Zone 3D (0-800 mm) |
|  |  |  | 23420000 |  |  |  | Cofierdam -Downstream |
|  |  |  |  | 23421000 |  |  | North D/S Cofferdam |
|  |  |  |  |  | 23421100 |  | Excavation CGC |
|  |  |  |  |  | 23421110 |  | Compacled TIII |
|  |  |  |  |  | 23421120 |  | Compacted Granular |
|  |  |  |  |  | 23421130 |  | Compacled Rockill |


| Level 1 | Level 2 | Level 3 | Level 4 | Level 5 | Leval 6 | Level 7 | Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 23421140 |  | Temp Bridge Across Diversion Discharge Channel |
|  |  |  |  |  | 23421150 |  | Cofferdam Removal |
|  |  |  |  | 23422000 |  |  | Powerhouse D/S Cofferdam |
|  |  |  |  |  | 23422100 |  | Excavation CGC |
|  |  |  |  |  | 23422110 |  | Compacted Till |
|  |  |  |  |  | 23422120 |  | Compacted Granular |
|  |  |  |  |  | 23422130 |  | Compacted Rockilil |
|  |  |  |  |  | 23422140 |  | Temp Bridge Across Diversion Discharge Channel |
|  |  |  |  |  | 23422150 |  | Cofferdam Removal |
|  |  |  |  |  | 23422160 |  | Rip Rap PBO |
|  |  |  |  |  | 23422170 |  | Foundation Prep |
|  |  |  |  |  | 23422180 |  | Concrele |
|  |  |  |  |  | 23422190 |  | Access Road to in Channel |
|  |  |  |  | 23423000 |  |  | Spliway D/S Cofferdam |
|  |  |  |  |  | 23423100 |  | Excavation CGC |
|  |  |  |  |  | 23423110 |  | Compacted Till |
|  |  |  |  |  | 23423120 |  | Compacted Granular |
|  |  |  |  |  | 23423130 |  | Compacted Rockfili |
|  |  |  |  |  | 23423140 |  | Temp Bridge Across Diversion Discharge Channel |
|  |  |  |  |  | 23423150 |  | Cofferdam Removal |
|  |  |  |  |  | 23423180 |  | Rip Rap PBO |
|  |  |  | 23430000 |  |  |  | Coffierdam - intake Channel |
|  |  |  |  | 23431000 |  |  | Powerhouse U/S Cofferdam |
|  |  |  |  |  | 23430100 |  | Overburden Excavation |
|  |  |  |  |  | 23430110 |  | Compacted Till - Zone 1 |
|  |  |  |  |  | 23430120 |  | Compacted Granular - Zone 2C |
|  |  |  |  |  | 23430130 |  | Compacted Rockfill - Zone 3C |
|  |  |  |  |  | 23430140 |  | Riprap (produced by others) 4 Class 1 |
|  |  |  |  |  | 23430150 |  | Foundation Preparation |
|  |  |  |  |  | 23430180 |  | Concrete |
|  |  |  |  |  | 23430170 |  | Access Road To and Across Intake Channel Cofferdam |
|  |  |  |  |  | 23430180 |  | Temporay Bridge Across Diverslon Channel Baliey 8 |
|  |  |  |  |  | 23430190 |  | Remove Rockfill Cofferdam |
|  |  |  |  |  | 23430200 |  | Copacted Rockill - Zone 30 (0.900mm) |
|  |  |  |  |  | 23430900 |  | Powerhouse Concrele Coffierdam |
|  |  |  |  |  |  | 23430910 | Cofferdam Concrete |
|  |  |  |  |  |  | 23430920 | Overbreak Concrete |
|  |  | 23600000 |  |  |  |  | Transition Structures |
|  |  |  | 23810000 |  |  |  | North Transition Structure |
|  |  |  |  | 23810100 |  |  | Excavation |
|  |  |  |  | 23810200 |  |  | Concrete Operation |
|  |  |  |  |  | 23810210 |  | Concrate CVC |
|  |  |  |  |  | 23610280 |  | Dralnage Gailery Formwork |
|  |  |  |  |  | 23810290 |  | Reinforcing Sleel |
|  |  |  |  |  | 23810295 |  | Overbreak Concrete \& Misc. |
|  |  |  |  |  |  | 23610296 | Overbreak Concrete |
|  |  |  |  |  |  | 23610297 | Waterstop |
|  |  |  |  | 23610300 |  |  | Pressure Relief Holes |
|  |  |  | 23820000 |  |  |  | Center Transition Structure |
|  |  |  |  | 23620300 |  |  | Concrete Operations |
|  |  |  |  |  | 23620310 |  | Concrete CVC |
|  |  |  |  |  |  | 23620320 | Mass Concrete Dam Section |
|  |  |  |  |  |  | 23620330 | Butress Wall |
|  |  |  |  |  |  | 23620340 | Stoplogs Storage Deck |
|  |  |  |  |  |  | 23620350 | Gate Storage Pad |
|  |  |  |  |  | 23620380 |  | Drainage Gallery Formwork |
|  |  |  |  |  | 23820390 |  | Reinforcing Steel |
|  |  |  |  |  | 23820395 |  | Overbreak Concrete \& Mlsc. |
|  |  |  |  |  |  | 23620396 | Overbreak Concrete |
|  |  |  |  |  |  | 23620397 | Waterstop |
|  |  |  | 23630000 |  |  |  | South Transition Structure |
|  |  | 23700000 |  |  |  |  | Dams / Cofierdams Aüxillary Services |
|  |  | 23700050 |  |  |  |  | CGC Cofferdam Excavation |
|  |  |  | 23700098 |  |  |  | CGC North D/S Cofferdam |
|  |  |  | 23800000 |  |  |  | CGC Powerhouse U/S Cofferdam |
|  |  |  | 23800001 |  |  |  | CGC Powerhouse D/S Cofferdam |
|  |  |  | 23800002 |  |  |  | CGC Spillway D/S Cofferdam |
|  |  |  | 23800003 |  |  |  | CGC Spiliway U/S Cofferdam |
|  |  |  | 23800005 |  |  |  | CGC Spillway U/S Cofferdam R1 |
|  |  |  | 23800008 |  |  |  | CGC North Dam U/S Rockfill Cofferdam |
|  |  |  | 23800007 |  |  |  | CGC Concrete Aggregates Production |
|  |  |  | 23800008 |  |  |  | CGC South Rockilil Dam |
|  |  |  | 23800009 |  |  |  | CGC North RCC Dam |
|  |  |  | 23800010 |  |  |  | CGC Riverside RCC Cofferdam |
|  |  |  | 23800011 |  |  |  | CGC North Spur |
|  | 24000000 |  |  |  |  |  | Splliway - General |
|  |  | 24000100 |  |  |  |  | Phase 1, Spillway Excavation |
|  |  | 24100000 |  |  |  |  | Spllway Conorete Structure |
|  |  |  | 24100100 |  |  |  | Plers and End Walls |
|  |  |  |  | 24100110 |  |  | Concrete - Plers and End Walls |
|  |  |  |  |  | 24100111 |  | Plers \& End Walls - Curved Noses U/S to EL 45.5 |
|  |  |  |  |  | 24100112 |  | Plers \& End Walls - Straight Face D/S to EL37/19.3 |
|  |  |  |  | 24100120 |  |  | Concrete - LLO Headwails and Deck |
|  |  |  |  |  | 24100121 |  | LLO Lower Curved Structural Slabs a EL 15.5 |
|  |  |  |  |  | 24100122 |  | LLO Walis to EL 45.5 |
|  |  |  |  |  | 24100123 |  | LLO Upper Structural Siabs Q EL 42.7 |
|  |  |  | 24100200 |  |  |  | Slabs and Rollways |
|  |  |  |  | 24100210 |  |  | Concrete - Slabs |


| Level 1 | Level 2 | Level 3 | Level 4 | Level 5 | Level 6 | Level 7 | Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 24100211 |  | Base Slab @ EL 5.0 |
|  |  |  |  | 24100220 |  |  | Concrete-Rollways |
|  |  |  |  |  | 24100221 |  | Rollway Slabs to EL 15.7 |
|  |  |  | 24100300 |  |  |  | Bridge |
|  |  |  |  | 24100310 |  |  | Concrete - Bridge Decks |
|  |  |  |  |  | 24100311 |  | Bridge Decks - U/S \& D/S @ EL 45.5 \& 20.3 |
|  |  |  |  | 24100320 |  |  | Structural Steel - 8ridge |
|  |  |  |  | 24100330 |  |  | Miscelianeous Steel-Bridge |
|  |  |  |  | 24100340 |  |  | Steel Grating - Bridge Deck |
|  |  |  |  | 24100350 |  |  | Splliway D/S Bridge Ramp. |
|  |  |  | 24100400 |  |  |  | Secondary Concrete |
|  |  |  |  | 24100410 |  |  | Secondary Concrete - Guides, Silis and Lintels |
|  |  |  |  |  | 24100411 |  | Secondary Concrete - Gater \& Stoplogs |
|  |  |  | 24100500 |  |  |  | Reinforcing Steel |
|  |  |  |  | 24100510 |  |  | Reinforcing Stoel-Spillway, Incl Brdge |
|  |  |  | 24100600 |  |  |  | Overbreak Concrete and Misc. |
|  |  |  |  | 24100610 |  |  | Overbreak Concrete |
|  |  |  |  | 24100620 |  |  | Waterstops |
|  |  |  |  | 24100830 |  |  | Miscellaneous Steel - Spilway |
|  |  |  |  | 24100850 |  |  | Concrale Heating |
|  |  |  | 24100700 |  |  |  | Drilling and Grouting and Draln Holes |
|  |  |  |  | 24100705 |  |  | Drillthg Grout Holes |
|  |  |  |  | 24100710 |  |  | Connection for Grout Stage |
|  |  |  |  | 24100715 |  |  | Cement used for grouting |
|  |  |  |  | 24100720 |  |  | Drilling ChackiHoles (Cored NX) |
|  |  |  |  | 24100725 |  |  | Drilling Check Holes Non corred 45 deg inclination |
|  |  |  |  | 24100730 |  |  | Connection Water Pressura Testing |
|  |  |  |  | 24100735 |  |  | Water prassure test (lugeon - 5 stages) |
|  |  |  |  | 24100740 |  |  | Drain Holes |
|  |  | 24200000 |  |  |  |  | Gates, Stoplogs, Guides and Hoist |
|  |  |  | 24200100 |  |  |  | Splilway Gates Embedded Parts |
|  |  |  |  | 24200190 |  |  | Spllway Gates Primary Anchors (Instil) |
|  |  |  | 24200200 |  |  |  | Splilway Gates |
|  |  |  | 24200300 |  |  |  | Splliway Gates Holsting syatem |
|  |  |  | 24200400 |  |  |  | Splliway Stoplogs Embedded Parts |
|  |  |  |  | 24200480 |  |  | Spillway Stoplogs Primary Anchors (insti) |
|  |  |  | 24200500 |  |  |  | Splilway Stoploge |
|  |  |  | 24200800 |  |  |  | Splilway Stoplogs Hoisting system |
|  |  | 24300000 |  |  |  |  | Spillway Channels |
|  |  |  | 24301000 |  |  |  | Splilway Downstream Channel |
|  |  |  | 24302000 |  |  |  | Splilway Approach Channei |
|  |  |  |  | 24302100 |  |  | Spillway Centre Pier |
|  |  |  |  |  | 24302110 |  | Pier Concrete |
|  |  |  |  |  | 24302120 |  | Reinforcing Steel |
|  |  | 24400000 |  |  |  |  | Splilway Auxillary Services |
|  |  | 24500000 |  |  |  |  | Splilway Electrical |
|  | 28000000 |  |  |  |  |  | North Spur - General |
|  |  | 28000140 |  |  |  |  | North Spur - Kettle Lake Slabilization |
|  |  | 28100000 |  |  |  |  | North Spur - Upstream Rock Berm |
|  |  |  | 28100110 |  |  |  | Excavation |
|  |  |  | 28100120 |  |  |  | Siurry Cut-Off Wall |
|  |  |  | 28100130 |  |  |  | NWISlurry Cut-Off Wall |
|  |  |  | 28100140 |  |  |  | Compacled Rockill - Zone 38-North Shore |
|  |  |  | 28100150 |  |  |  | Till Blanket - Zone 1- North Shore |
|  |  |  | 28100180 |  |  |  | Rip Rap Zone 48 North Shore |
|  |  |  | 28100170 |  |  |  | Rip Rap Zone 48 South Shore |
|  |  |  | 28400180 |  |  |  | Zone 5-Materiai Crushed Stone Max. 31.5 mm (perma |
|  |  |  | 28100190 |  |  |  | Compacted Rockfill - Zone 3B - South Shore Excavat |
|  |  | 28200000 |  |  |  |  | North Spur - Downstream Stabilization |
|  |  |  | 28200110 |  |  |  | Dumped Rockfill - Zone 3-North Shore |
|  |  |  | 28200120 |  |  |  | Dumped Rockfili - Zone 3-South Shore |
|  |  |  | 28200130 |  |  |  | Compacted Rockfill - Zone 3A - North Shore |
|  |  |  | 28200140 |  |  |  | Compacted Rockfill - Zone 3A - South Shore |
|  |  |  | 28200150 |  |  |  | Compacled Rockfill - Zone 38 - South Shore |
|  |  |  | 28200180 |  |  |  | Granular Material - Zone 2 - North Shore |
|  |  |  | 28200170 |  |  |  | Geomembrane |
|  |  |  | 28200180 |  |  |  | Geotextile |
|  |  | 28300000 |  |  |  |  | North Spur - Pump wells |
|  |  |  | 28300110 |  |  |  | Now Pumpwelis |
|  |  |  | 28300120 |  |  |  | Refurblsh Existing Pumpwelis |
|  |  |  | 28300130 |  |  |  | Header Plipe ( $\mathrm{d}=600 \mathrm{~mm}$ ) |
|  |  |  | 28300140 |  |  |  | Rellef Drain Weils |
|  |  |  | 28400000 |  |  |  | North Spur - Crest Unloading |
|  |  |  | 28400110 |  |  |  | Geomembrane |
|  |  | 28600000 |  |  |  |  | North Spur Electrical |
| 30000000 |  |  |  |  |  |  | Power Facilities |
|  | 30001000 |  |  |  |  |  | Site preparation |
|  |  | 30001100 |  |  |  |  | Clearing |
|  |  |  | 30001110 |  |  |  | Clearing of Temporary Works (borrow area, access r |
|  |  | 30001200 |  |  |  |  | Stripping |
|  |  | 30001300 |  |  |  |  | Top soil removal |
|  |  | 30001400 |  |  |  |  | Overburden |
|  |  | 30001500 |  |  |  |  | Temporary Roads |
|  |  | 30001600 |  |  |  |  | Construction of Settlement Ponds |
|  | 30002000 |  |  |  |  |  | Misclianeous Work |
|  |  | 30002100 |  |  |  |  | Steel Guardralls |
|  | 31000000 |  |  |  |  |  | [Powerhouse Channels (Inc.Plugs and/or Cofferdam) |


| Level 1 | Level 2 | Level 3 | Level 4 | Level 5 | Level 6 | Level 7 | Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 31001000 |  |  |  |  | Approach Channel Common excavalion |
|  |  | 31002000 |  |  |  |  | Approach Channel Rock Excavation |
|  |  | 31003000 |  |  |  |  | Approach Channei Rook Consolidation |
|  |  |  | 31003100 |  |  |  | Approach Channel injected Rock Bolls |
|  |  |  | 31003200 |  |  |  | Approach Channel Non-Injected Rock Boits |
|  |  |  | 31003300 |  |  |  | Approach Channel Wire mesh |
|  |  | 31004000 |  |  |  |  | Approach Channel Cofferdam |
|  |  | 31005000 |  |  |  |  | Approach Channel Rock Plug |
|  |  | 31008000 |  |  |  |  | Talirace Channel Common excavation |
|  |  | 31007000 |  |  |  |  | Tailrace Channel Rock excavation |
|  |  |  | 31007100 |  |  |  | Tailrace Channel injected Rock Bolts |
|  |  |  | 31007200 |  |  |  | Talirace Channel Non-Injected Rock Bolts |
|  |  |  | 31007300 |  |  |  | Talirace Channel Wire mesh |
|  |  | 31008000 |  |  |  |  | Talirace Cofferdam |
|  |  | 31009000 |  |  |  |  | Taliface Rock Plug |
|  | 32000000 |  |  |  |  |  | Intake - General |
|  |  | 32001000 |  |  |  |  | Intake and Powerhouse Common excavation |
|  |  | 32002000 |  |  |  |  | intake and Powerhouse Rock Excavalion |
|  |  |  | 32002100 |  |  |  | Intake Rock Exc |
|  |  |  | 32002200 |  |  |  | Structure Rock Exc |
|  |  |  | 32002300 |  |  |  | Tailirace Rock Exc |
|  |  | 32003000 |  |  |  |  | intake Concrele Structure |
|  |  |  | 32003100 |  |  |  | Intake Bottom |
|  |  |  | 32003200 |  |  |  | Intake Top |
|  |  | 32004000 |  |  |  |  | Intake and Powerhouse Rock Consolidation |
|  |  |  | 32004100 |  |  |  | Intake and Powerhouse injected Rock B8 |
|  |  |  | 32004200 |  |  |  | Intake and Powerhouse Non-Injected RB |
|  |  |  | 32004300 |  |  |  | Intake and Powerhouse Wire mesh |
|  |  | 32200000 |  |  |  |  | Intake Concrele Siructure |
|  |  |  | 32200100 |  |  |  | Concrete |
|  |  |  |  | 32200105 |  |  | Intake Base Slabs to EL-1.7 |
|  |  |  |  | 32200110 |  |  | Intake Piers \& End Wails - Main |
|  |  |  |  | 322001.15 |  |  | Intake Divider Walis |
|  |  |  |  | 32200120 |  |  | Intake Siopling Structural Block from E 7.75-28.3 |
|  |  |  |  | 32200125 |  |  | Intake Structural Block from E line 26.30 to 45.5 |
|  |  |  |  | 32200130 |  |  | Intake Deck © 45.5 (Gallery Roof © Gata Hoist Bidg |
|  |  |  |  | 32200135 |  |  | Intake Gate Holst Bullding Wails from 45.50 |
|  |  |  |  | 32200140 |  |  | Intake Gate Holst Bullding Roof (Bidg \& Air Plens) |
|  |  |  |  | 32200145 |  |  | Intake Gate Holst Büllding Cuibs \& 51.50 \& 45.50 |
|  |  |  |  | 32200150 |  |  | Intake Gailerles/Shafts/Pits EXter,- Slabs from E |
|  |  |  |  | 32200155 |  |  | Intake Galieries/Shafts/Pits Exter, - Walls frome |
|  |  |  |  | 32200180 |  |  | Intake Galleries/Shafts/Pits Exter. - Str Stabs |
|  |  |  | 32200300 |  |  |  | Formwork - flat |
|  |  |  | 32200400 |  |  |  | Formwork-curved |
|  |  |  | 32200500 |  |  |  | Secondary Concrele |
|  |  |  |  | 32200510 |  |  | 2nd Phase concrete for steel emb. Part |
|  |  |  | 32200600 |  |  |  | Reinforcing Sleel |
|  |  |  |  | 32200810 |  |  | Reinforcing Stoel |
|  |  |  | 32200700 |  |  |  | Overbreak Concrete \& Misc. |
|  |  |  |  | 32200710 |  |  | Overbreak Concrete |
|  |  |  |  | 32200720 |  |  | Waterstops |
|  |  |  |  | 32200750 |  |  | Concrete Heating |
|  |  |  |  | 32200760 |  |  | Tower Crane Setups |
|  |  |  |  | 32200770 |  |  | Temporary Bulididng for Winter Protection |
|  |  | 32400000 |  |  |  |  | Intake Gates, Trashracks, Stoplogs and Holsis |
|  |  |  | 32400100 |  |  |  | Intake Gates Embedded Parts |
|  |  |  |  | 32400190 |  |  | Intake GatesPrimary Anchors (Instil) |
|  |  |  | 32400200 |  |  |  | Intake Gates |
|  |  |  | 32400300 |  |  |  | Intake Gates Hoisting system |
|  |  |  | 32400400 |  |  |  | Intake Trashracks Embedded Parts |
|  |  |  |  | 32400490 |  |  | Intake Trashracks Primary Anchors (insti) |
|  |  |  | 32400500 |  |  |  | Intake Trashracks |
|  |  |  | 32400800 |  |  |  | Intake Trashracks Mechanical System |
|  |  |  | 32400700 |  |  |  | Intake Stoplogs Embedded Parts |
|  |  |  |  | 32400790 |  |  | Intake Stoplogs Primary Anchors (instil) |
|  |  |  | 32400800 |  |  |  | Intake Stoplogs |
|  |  |  | 32400900 |  |  |  | Intake Stoplogs Holsting system |
|  |  | 32500000 |  |  |  |  | Penstocks |
|  |  | 32800000 |  |  |  |  | Penstocks Construction Addit |
|  |  | 32900000 |  |  |  |  | Intake Auxillary Services |
|  | 33000000 |  |  |  |  |  | Power House |
|  |  | 33100000 |  |  |  |  | Substructure |
|  |  |  | 33100100 |  |  |  | Powerhouse/Intake |
|  |  |  | 33100200 |  |  |  | Intake |
|  |  |  | 33100300 |  |  |  | Powerhouse Area of Units |
|  |  |  | 33100400 |  |  |  | Powerhouse - Service Bay |
|  |  |  | 33100500 |  |  |  | Poweriosue - South Transition |
|  |  |  | 33100800 |  |  |  | Powerhouse - Concrele Deck |
|  |  |  | 33101000 |  |  |  | Substructure - Area of Units |
|  |  |  |  | 33101100 |  |  | Concrete-18t Stage |
|  |  |  |  |  | 33101105 |  | PH Draft Tube Base Slab-34.1 to -31.1/-26.68 |
|  |  |  |  |  | 33101110 |  | PH Intake Side Base Slab-from 17.02 sioping up |
|  |  |  |  |  | 33101115 |  | PH Draft Tube Transitions Encasement -31.1 to-12 |
|  |  |  |  |  | 33101120 |  | PH Block Above Dewatering Gallery, D/S -17.8--12 |
|  |  |  |  |  | 33101125 |  | Draft Walls to Crown: D/S of Trans -31.1-17.8 |
|  |  |  |  |  | 33101130 |  | PH Intake Side Walls to Crown |
|  |  |  |  |  | 33101135 |  | PH Piers \& A-Line Walls D/S - 17.8 to 6.5 |
|  |  |  |  |  | 33101140 |  | PH D/S Curtain Walls -0.60 to Turbine Floor 6.50 |


| Level 1 | Level 2 | Level 3 | Level 4 | Level 5 | Level 6 | Level 7 | Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 33101145 |  | PH Turbine Floor D/S Craneway Walis 6.5 to 14.15 |
|  |  |  |  |  | 33101150 |  | PH Turbine Walls \& Pads: Trans/Ballast Walls/Pads |
|  |  |  |  |  | 33101155 |  | PH Turbine Floor Columne 8.50 to Tallrace Deck |
|  |  |  |  |  | 33101180 |  | PH Draft Tube Crown-0/S of Transition |
|  |  |  |  |  | 33101165 |  | PH Intake Side Block to 15.5 |
|  |  |  |  |  | 33101170 |  | PH Turbine Floor Slab D/S of A @ 6.5; Craneway Wik |
|  |  |  |  |  | 33101175 |  | PH Talirace SlabsBeams: U/S Face LineA 8m D/S 15.5 |
|  |  |  |  |  | 33101180 |  | PH Extermal Slabs on Grade - Line A \& Line 24 |
|  |  |  |  |  | 33101185 |  | PH External Walls - Line A \& Line 24 |
|  |  |  |  |  | 33101190 |  | PH Extemal Structurai Siabs - Line A \& LIne 24 |
|  |  |  |  | 33101200 |  |  | Concrete - 2nd Stage |
|  |  |  |  |  | 33101210 |  | PH Stage 2 Seml-Spiral Cases -12 to 6.5 Turb Fir |
|  |  |  |  |  | 33101220 |  | PH Stage 2 Tumine Floor Walis 8.5 to Gen Fir |
|  |  |  |  |  | 33101230 |  | PH Stage 2 Turbine Fioor Columns 6.5 to Gen Fir |
|  |  |  |  |  | 33101240 |  | PH Stage 2 Generator Floor Slabs \& Beams © 15.5 |
|  |  |  |  | 133101300 |  |  | Formwork - flat |
|  |  |  |  | 33101400 |  |  | Formwork - curved |
|  |  |  |  | 33101500 |  |  | Secondary Concrete |
|  |  |  |  |  | 33101510 |  | 2nd phase concrete for embed. Part |
|  |  |  |  | 33101600 |  |  | Reinforcing Steel |
|  |  |  |  |  | 33101610 |  | Reinforcing Stoel |
|  |  |  |  | 33101700 |  |  | Overbreak Concrete \& Misc. |
|  |  |  |  |  | 33101710 |  | Overbreak Concrete |
|  |  |  |  |  | 33101720 |  | Waterstops |
|  |  |  |  |  | 33101750 |  | Concrete Healing |
|  |  |  |  |  | 33101760 |  | Temporary Building for 2nd Stage Work |
|  |  |  | 33102000 |  |  |  | Substructure - Service Bay |
|  |  |  |  | 33102100 |  |  | Concrete |
|  |  |  |  |  | 33102110 |  | Service Bay Slabs on Grade D/S of LIne E |
|  |  |  |  |  | 33102120 |  | Service Bay Walls D/S of Line E |
|  |  |  |  |  | 33102130 |  | Service Bay Columns D/S of Line E |
|  |  |  |  |  | 33102140 |  | Service Bay Structural Stabs D/S of Line E |
|  |  |  |  |  | 33102150 |  | Gails/Shatts/Pits (Ext): Slabs U/S of E (Int Side) |
|  |  |  |  |  | 33102160 |  | Galls/Shaft//Pits (Ext): Walls U/S of E (Int Side) |
|  |  |  |  | 33102300 |  |  | Formwork - flat |
|  |  |  |  | 133102600 |  |  | Reinforcing Steel |
|  |  |  |  |  | 33102610 |  | Reinforcing Steel |
|  |  |  |  | 33102700 |  |  | Overbreak Concrete \& Misc. |
|  |  |  |  |  | 33102710 |  | Overbreak Concrete |
|  |  |  |  |  | 33102720 |  | Waterstops |
|  |  |  |  |  | 33102750 |  | Concrate Heating |
|  |  |  | 33103000 |  |  |  | Merz \& Parking Area - Slabs on Steel Deck \& SOG |
|  |  |  |  | 33103100 |  |  | Concrete |
|  |  |  |  |  | 33103110 |  | PH inlake Slde Mezz Slabs (1) 25.5 \& 34.5 E to C |
|  |  |  |  |  | 33103120 |  | Parking Area Slabs on Grade (Balance) |
|  |  |  |  | 33103600 |  |  | Rainforcing Steel |
|  |  |  |  |  | 33103610 |  | Reinforcing Steel |
|  |  |  |  | 33103700 |  |  | Overbreak Concrete \& Misc. |
|  |  |  |  |  | 33103710 |  | Overbreak Concrate |
|  |  |  |  |  | 33103720 |  | Waterstops |
|  |  | 33200000 |  |  |  |  | Superstructure (structure and architecture) |
|  |  |  | 33200100 |  |  |  | Superstructure - Structural Steel |
|  |  |  | 33200200 |  |  |  | Supersitucture - Misc. steel (Embed \& Non-Embed) |
|  |  |  |  | 33200280 |  |  | Süperstucture Steel |
|  |  |  |  | 33200290 |  |  | PH Embedded Misc Parts |
|  |  |  | 33200300 |  |  |  | Superstructure - Archilecture |
|  |  |  | 33200400 |  |  |  | Superstructure - Special Doors |
|  |  | 33300000 |  |  |  |  | Draft Tubes Gates, Stoplogs and Hoists |
|  |  |  | 33300100 |  |  |  | Draft Tubes Gates Embedded Parts |
|  |  |  | 33300200 |  |  |  | Draft Tubes Gates |
|  |  |  | 33300300 |  |  |  | Draft Tubes Stoplogs Embedded Parts |
|  |  |  |  | 33300380 |  |  | Draft Tube Stop Logs |
|  |  |  | 33300400 |  |  |  | Draft Tubes Stoplogs |
|  |  |  | 33300500 |  |  |  | Draft Tubes Gates and Stoplogs Hoisting System |
|  |  | 33400000 |  |  |  |  | Bullding Electical Services |
|  |  |  | 33400100 |  |  |  | AC Bus Bars and Auxillary Transformers |
|  |  |  | 33400200 |  |  |  | AC Electrical Distibution 600V and Lower |
|  |  |  | 33400300 |  |  |  | AC Auxiliary Systems cw batteries and Chargers |
|  |  |  | 33400350 |  |  |  | Powerhouse Buliding Electrical Major Equipment |
|  |  |  | 33400400 |  |  |  | Emergency Diesel Generalor |
|  |  |  | 33400500 |  |  |  | Lighting and power Outtet System |
|  |  |  | 33400600 |  |  |  | Fire Detection and Alarm Syslem |
|  |  |  | 33400700 |  |  |  | Telephone, Communication and Computer Systems |
|  |  |  | 33400900 |  |  |  | Cable Trays and Condulis |
|  |  | 33500000 |  |  |  |  | Building Mechanical Services |
|  |  |  | 33500100 |  |  |  | Fire Prolection System |
|  |  |  | 33500200 |  |  |  | Potabio Waler System |
|  |  |  | 33500300 |  |  |  | Sanitary drainage System |
|  |  |  | 33500400 |  |  |  | Powerhouse HVAC |
|  |  | 33600000 |  |  |  |  | Powerhouse Crane |
|  |  |  | 33600100 |  |  |  | Overhead Crane |
|  |  |  | 33600200 |  |  |  | Powerhouse Eievators |
|  |  |  | 33600300 |  |  |  | Powerhouse Auxiliary Monorails and Hoists |
|  | 34000000 |  |  |  |  |  | Power Generation |
|  |  | 34009999 |  |  |  |  | Indirect |
|  |  | 34100000 |  |  |  |  | Turbine |
|  |  |  | 34100100 |  |  |  | Governor |
|  |  |  | 34100200 |  |  |  | Turbine Moblle Parts |


| Level 1 | Level 2 | Level 3 | Level 4 | Level 5 | Level 6 | Level 7 | Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 34100300 |  |  |  | Turbine Fixed Parts |
|  |  |  | 34100400 |  |  |  | Spiral Case |
|  |  |  | 34100500 |  |  |  | Embedded Parts |
|  |  |  | 34100800 |  |  |  | Drafl Tube Liner |
|  |  | 34200000 |  |  |  |  | Generator |
|  |  |  | 34200100 |  |  |  | Excitation System |
|  |  |  | 34200200 |  |  |  | Rotor, Stator \& Rotor Guide Bearings |
|  |  |  | 34200300 |  |  |  | Embodded Parts |
|  |  |  | 34200400 |  |  |  | Genarator Circult Breaker |
|  |  |  | 34200500 |  |  |  | isolated Phase Bus |
|  |  |  | 34200600 |  |  |  | High Voltage Equipment ( 345 kV XLPE Cabie, _ ) |
|  |  |  | 34200700 |  |  |  | Fire Protection System |
|  |  |  | 34200800 |  |  |  | Acoustic Insuiation |
|  |  |  | 34200900 |  |  |  | Brake Jack equipment |
|  |  | 34300000 |  |  |  |  | Electrical Anciliary / Auxiliary Systéms |
|  |  |  | 34300100 |  |  |  | DC Power/ UPS System |
|  |  |  | 34300200 |  |  |  | MV Systems (601V 10 15kV) |
|  |  |  | 34300300 |  |  |  | LV Systems (up to 600V) |
|  |  |  | 34300400 |  |  |  | Unit Service Transformer |
|  |  |  | 34300500 |  |  |  | Station Service Transformers |
|  |  |  | 34300600 |  |  |  | Bus Duct |
|  |  |  | 34300700 |  |  |  | Dlesei Generators |
|  |  |  | 34300800 |  |  |  | Fire Protection System |
|  |  |  | 34300900 |  |  |  | Vendor Rep Services |
|  |  | 34400000 |  |  |  |  | Mechanical Anciliary/Auxiliary Systems |
|  |  |  | 34400100 |  |  |  | Service Air System |
|  |  |  | 34400200 |  |  |  | Governor Air System |
|  |  |  | 34400300 |  |  |  | Fire Protaction System |
|  |  |  | 34400400 |  |  |  | Pump Drainage System |
|  |  |  | 34400500 |  |  |  | Pump Dewatering System |
|  |  |  | 34400600 |  |  |  | Hydraulic Oil Handiling and Filitration System |
|  |  |  | 34400700 |  |  |  | Oly Water Interception System |
|  |  |  | 34400800 |  |  |  | Cooling Waler System |
|  |  |  | 34400900 |  |  |  | Servico Water System |
|  |  |  | 34401000 |  |  |  | Shaft Seai Water System |
|  |  |  | 34401100 |  |  |  | Plezometer System |
|  |  |  | 34408989 |  |  |  | Indirect |
|  |  | 34500000 |  |  |  |  | Protection, Control and monitoring |
|  |  |  | 34510000 |  |  |  | Protection |
|  |  |  | 34520000 |  |  |  | Control and Monitoring |
|  |  | 34600000 |  |  |  |  | Generator Transformers |
|  |  |  | 34600100 |  |  |  | Suppi \& instail Generator Transformers |
|  |  |  | 34600200 |  |  |  | Suppl \& instali Spare Transformers |
|  |  | 34700000 |  |  |  |  | Spare Parts and Special Toois |
|  | 35000000 |  |  |  |  |  | Not Used |
| 40000000 |  |  |  |  |  |  | Switchyards - General |
|  | 40000999 |  |  |  |  |  | Vendor Representatives services |
|  | 41000000 |  |  |  |  |  | Churchill Falis Extension - General |
|  |  | 41000100 |  |  |  |  | Churchili Fails Switchyard Extension - Civil |
|  |  |  | 41000110 |  |  |  | Clil Works |
|  |  |  | 41000120 |  |  |  | Concrete Works |
|  |  |  | 41000130 |  |  |  | Structural Steel Works |
|  |  |  | 41000140 |  |  |  | Archiliectura/Builidings |
|  |  |  | 41000150 |  |  |  | Mechanical Services |
|  |  |  | 41000160 |  |  |  | Mechanical Equipment |
|  |  |  | 41000170 |  |  |  | Demolition |
|  |  | 41000200 |  |  |  |  | Churchill Faiis Switchyard Extension-Equip \& Elec |
|  |  |  | 41000210 |  |  |  | Direct |
|  |  |  | 41000220 |  |  |  | Indirect |
|  |  |  | 41000989 |  |  |  | indirect |
|  | 43000000 |  |  |  |  |  | Muskrat Falls Switchyard |
|  |  | 43000100 |  |  |  |  | Muskrat Falis $315 \mathrm{KV}, ~ A C$ |
|  |  |  | 43000110 |  |  |  | Muskrat Falis $315 \mathrm{KV}, \mathrm{AC}$ Clvil works-General |
|  |  |  |  | 43000111 |  |  | Civil Works |
|  |  |  |  | 43000112 |  |  | Concrete Works |
|  |  |  |  | 43000113 |  |  | Structural Steel Works |
|  |  |  |  | 43000114 |  |  | Architectura/Bulidinge |
|  |  |  |  | 43000115 |  |  | Mechanical Services |
|  |  |  |  | 43000116 |  |  | Mechanical Equipment |
|  |  |  |  | 43000117 |  |  | Demolition |
|  |  |  | 43000120 |  |  |  | Muskrat Fails $315 \mathrm{KV}, \mathrm{AC}$-Equip \& Elec |
|  |  |  |  | 43000121 |  |  | Direct ...t |
|  |  |  |  | 43000122 |  |  | Indirect |
|  |  | 43000200 |  |  |  |  | Muskral Falls Substation TAP, 315/168/25 KV, AC |
|  |  |  | 43000210 |  |  |  | Muskral Falis Substation TAP, 315/168/25 KV, AC-CI |
|  |  |  |  | 43000211 |  |  | Crwil Works |
|  |  |  |  | 43000212 |  |  | Concrete Works |
|  |  |  |  | 43000213 |  |  | Structural Stoei Works |
|  |  |  |  | 43000214 |  |  | Architectura/Bulidings |
|  |  |  |  | 43000215 |  |  | Mechanical Servicas |
|  |  |  |  | 43000218 |  |  | Mechanical Equipment |
|  |  |  | 43000220 |  |  |  | Muskrat Falls Substation TAP, 316/168/25 KV, AC-Eq |
|  |  |  |  | 43000221 |  |  | Direct |
|  |  |  |  | 43000222 |  |  | indirect |
|  |  |  |  | 43000298 |  |  | indireet |
|  |  |  |  | 43000999 |  |  | indirect |
|  | 45000000 |  |  |  |  |  | Soldiers Pond Switchyard |


| Level 1 | Level 2 | Level 3 | Level 4 | Level 5 | Level 6 | Level 7 | Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 45000100 |  |  |  |  | Soidlers Pond Switchyard - Civil |
|  |  |  | 45000110 |  |  |  | Clvil Works |
|  |  |  | 45000120 |  |  |  | Concrete Works |
|  |  |  | 45000130 |  |  |  | Structural Steei Works |
|  |  |  | 45000140 |  |  |  | Architectural/Buildings |
|  |  |  | 45000150 |  |  |  | Mechanical Services |
|  |  |  | 45000180 |  |  |  | Mechanicai Equipment |
|  |  | 45000200 |  |  |  |  | Soldiers Pond Switchyard-Equipment and Electrica |
|  |  |  | 45000210 |  |  |  | Direct |
|  |  |  | 45000220 |  |  |  | indirect |
|  |  | 45000300 |  |  |  |  | Protection Panels for 230 KV Line |
|  |  |  | 45000998 |  |  |  | indirect |
| 60000000 |  |  |  |  |  |  | Overland Transmission - General |
|  | 61000000 |  |  |  |  |  | AC Overland Transmission (Towers and foundations) |
|  |  | 61300000 |  |  |  |  | Swithyard to Converter Station |
|  |  | 81400000 |  |  |  |  | Churchill Falis to Muskrat Falis (Gull is not phys |
|  |  |  | 61401000 |  |  |  | Contract 1 |
|  |  |  |  | 61400010 |  |  | Survey |
|  |  |  |  | 61400020 |  |  | Geotechnical |
|  |  |  |  | 61400030 |  |  | Access roads and Crossings |
|  |  |  |  | 61400040 |  |  | Clearing and Logging |
|  |  |  |  | 61400100 |  |  | Foundation Works |
|  |  |  |  |  | 61400110 |  | Supply and Install Anchors |
|  |  |  |  |  | 61400120 |  | Supply and instail Griliage |
|  |  |  |  |  | 61400130 |  | Supply and instail Concrete \& Rebar |
|  |  |  |  | 81400200 |  |  | Towers |
|  |  |  |  |  | 61400210 |  | Procurement of tower steei (Tower packaged) |
|  |  |  |  |  | 61400220 |  | Procurement of guy wires |
|  |  |  |  |  | 61400230 |  | Transport for construction (handiling at yard andt |
|  |  |  |  |  | 61400240 |  | Assembly |
|  |  |  |  |  | 61400250 |  | Eraction |
|  |  |  |  | 61400300 |  |  | Insulators and hardware |
|  |  |  |  |  | 61400310 |  | Supply and Install |
|  |  |  |  |  | 61400320 |  | Transport for construction (handling at yard and t |
|  |  |  |  | 61400400 |  |  | Conductors, Reels and Accossories |
|  |  |  |  |  | 61400410 |  | Supply and Instali |
|  |  |  |  |  |  | 61400411 | Insulators install |
|  |  |  |  |  |  | 61400412 | Cabla puller |
|  |  |  |  |  |  | 61400413 | Cable tensioneur |
|  |  |  |  |  |  | 61400414 | Sag. $\&$ clamp |
|  |  |  |  |  |  | 61400415 | Anchor Dead End |
|  |  |  |  |  |  | 61400416 | Jumper |
|  |  |  |  |  |  | 61400417 | Brace conductor |
|  |  |  |  |  |  | 61400418 | Move Team Puller-Tensioner |
|  |  |  |  |  |  | 61400419 | Temporary Protection |
|  |  |  |  |  | 61400420 |  | Transport for construction (handing at yard and t |
|  |  |  |  | 61400500 |  |  | Optical Power Ground Wire (OPGW) \& Accessories |
|  |  |  |  | 61400600 |  |  | Overhead Shiald Wire (OHSW) \& Accessories |
|  |  |  |  | 61400700 |  |  | Grounding |
|  |  |  |  | 61400800 |  |  | Remediai Work |
|  |  |  |  | 61400900 |  |  | Auxiliary work (generai to one or more sections) |
|  |  |  |  | 61400901 |  |  | Countermeight |
|  |  |  |  |  | 61400905 |  | Material Procurement Logistics |
|  |  |  |  |  | 61400910 |  | Marshalling Yards (Setup and Operation) |
|  |  |  |  |  | 81400915 |  | Construction and EPCM personnel Accommodations |
|  |  |  |  |  | 61400920 |  | Communication |
|  |  |  |  |  | 81400925 |  | Sites Offices and Supervision |
|  |  |  |  |  | 61400930 |  | Laboratory Costs |
|  |  |  |  |  | 61400935 |  | Materials and supply transport |
|  |  |  |  |  | 81400940 |  | EPCM Costs (Site \& St-John's) |
|  |  |  |  |  | 61400945 |  | Construction Permitting Costs |
|  |  |  |  |  | 81400950 |  | Other Permiltting Costs |
|  |  |  |  |  | 81400955 |  | Construction QAVC |
|  |  |  |  |  | 61400960 |  | Commissioning and turnover |
|  |  |  |  |  | 61400965 |  | Environmentai Monitoring |
|  |  |  |  |  | 61400970 |  | Helicopter costs |
|  |  |  |  |  | 61400975 |  | QA \& QC Costa (Nalcor, EPCM \& Contractor) |
|  |  |  |  | 61401999 |  |  | Indirects |
|  |  |  | 61402000 |  |  |  | Contract 2 |
|  |  |  |  | 61402010 |  |  | Survey |
|  |  |  |  | 61402020 |  |  | Geotechnical |
|  |  |  |  | 61402030 |  |  | Accesss roads and Crosings |
|  |  |  |  | 61402040 |  |  | Cloaring and Logging |
|  |  |  |  | 61402100 |  |  | Foundation Works |
|  |  |  |  |  | 61402110 |  | Supply and instali Anchors |
|  |  |  |  |  | 61402120 |  | Supply and instali Griilage |
|  |  |  |  |  | 61402130 |  | Supply and instali Concrete \& Rebar |
|  |  |  |  | 61402200 |  |  | Towers |
|  |  |  |  |  | 61402210 |  | Procurement of tower steel (Tower packaged) |
|  |  |  |  |  | 61402220 |  | Procurement of guy wires |
|  |  |  |  |  | 61402230 |  | Transport for construction (handiling at yard and t |
|  |  |  |  |  | 61402240 |  | Assembly |
|  |  |  |  |  | 61402250 |  | Eraction |
|  |  |  |  | 61402300 |  |  | insulators and hardware |
|  |  |  |  |  | 61402310 |  | Suppiy and Install |
|  |  |  |  |  | 61402320 |  | Transport for construction (handling at yard and t |
|  |  |  |  | 61402400 |  |  | Conductors, Reels and Accessories |
|  |  |  |  |  | 61402410 |  | Supply and instail |


| Leval 1 | Level 2 | Lovel 3 | Level 4 | Level 5 | Level 6 | Level 7 | Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | 61402411 | Insulators install |
|  |  |  |  |  |  | 61402412 | Cable puller |
|  |  |  |  |  |  | 61402413 | Cable tensioneur |
|  |  |  |  |  |  | 61402414 | Sag.\& clamp |
|  |  |  |  |  |  | 61402415 | Anchor Dead End |
|  |  |  |  |  |  | 61402416 | Jumper |
|  |  |  |  |  |  | 61402417 | Brace conductor |
|  |  |  |  |  |  | 61402418 | Move Team Puller-Tensioner |
|  |  |  |  |  |  | 61402419 | Temporary Protection |
|  |  |  |  |  | 61402420 |  | Transport for construction (handiling at yard and t |
|  |  |  |  | 61402500 |  |  | Optical Power Ground Wire (OPGW) \& Accessories |
|  |  |  |  | 61402600 |  |  | Overhead Shield Wire (OHSW) \& Accessories |
|  |  |  |  | 61402700 |  |  | Grounding |
|  |  |  |  | 61402800 |  |  | Remedial Work |
|  |  |  |  | 61402900 |  |  | Auxiliary work (generai to one or more sections) |
|  |  |  |  | 61402901 |  |  | Counterweight |
|  |  |  |  |  | 61402905 |  | Material Procurement Logistics |
|  |  |  |  |  | 61402910 |  | Marshaliing Yards (Setup and Operation) |
|  |  |  |  |  | 81402915 |  | Construction and EPCM personnel Accommodations |
|  |  |  |  |  | 61402920 |  | Communication |
|  |  |  |  |  | 61402925 |  | Siles Offices and Supervision |
|  |  |  |  |  | 61402930 |  | Laboratory Cosis |
|  |  |  |  |  | 61402935 |  | Materials and supply transport |
|  |  |  |  |  | 61402940 |  | EPCM Costs (Site \& St-John's) |
|  |  |  |  |  | 61402945 |  | Construction Permitting Costs |
|  |  |  |  |  | 81402950 |  | Other Permitting Costs |
|  |  |  |  |  | 61402955 |  | Construction QAMC |
|  |  |  |  |  | 61402980 |  | Commisstoning and tumover |
|  |  |  |  |  | 81402985 |  | Environmental Monitoring |
|  |  |  |  |  | 61402970 |  | Helicopler costs |
|  |  |  |  |  | 61402975 |  | QA \& QC Costa (Naicor, EPCM \& Contractor) |
|  |  |  |  | 61402998 |  |  | Indirects |
|  |  | 61800000 |  |  |  |  | Coilector Lines Powerhouse to Swilchyand |
|  | 62000000 |  |  |  |  |  | HVDC Overland Transmission |
|  |  | 62200000 |  |  |  |  | Island Overland DC Transmission (IODCT) |
|  |  |  | 62201000 |  |  |  | IODCT Section 1 - 250 km from SOBI to PK250 |
|  |  |  |  | 62201010 |  |  | Anchor drililing DC Segment. 2 WA |
|  |  |  |  |  | 62201020 |  | Supply Anchor bar |
|  |  |  |  |  | 62201030 |  | Helico-Anchor |
|  |  |  |  |  | 62201040 |  | Anchor drilling DC Segment. 2 WA |
|  |  |  |  |  | 62201050 |  | Anchor Drilling move st |
|  |  |  |  |  | 62201080 |  | Grout |
|  |  |  |  |  | 62201070 |  | Manufacturing guya |
|  |  |  |  |  | 62201080 |  | Anchor Test |
|  |  |  |  |  | 62201090 |  | INDIRECTS |
|  |  |  |  | 62201100 |  |  | Foundation DC Segment 2 WA |
|  |  |  |  |  | 62201110 |  | Supply Steel found. |
|  |  |  |  |  | 62201120 |  | Helico |
|  |  |  |  |  | 62201130 |  | Type A.1 250 kpa |
|  |  |  |  |  | 62201140 |  | Type A-2 100kpa |
|  |  |  |  |  | 62201150 |  | Type A Roc |
|  |  |  |  |  | 62201160 |  | Type B-1 250kpa |
|  |  |  |  |  | 62201170 |  | Type B-2 100kpa |
|  |  |  |  |  | 62201180 |  | Type B Roc |
|  |  |  |  |  | 62201190 |  | Type C-1 250kpa |
|  |  |  |  |  | 62201200 |  | Type C-2 100kpa |
|  |  |  |  |  | 62201210 |  | Type C Roc |
|  |  |  |  |  | 62201220 |  | Type D-1 250kpa |
|  |  |  |  |  | 62201230 |  | Type D-2 100kpa |
|  |  |  |  |  | 62201240 |  | Type D Roc |
|  |  |  |  |  | 62201250 |  | Type E-1 250 kpa |
|  |  |  |  |  | 62201280 |  | Type E-2 100kpa |
|  |  |  |  |  | 62201270 |  | Type E Roc |
|  |  |  |  |  | 82201280 |  | Pile driving |
|  |  |  |  |  | 62201290 |  | Deep found Head pile |
|  |  |  |  |  | 62201300 |  | Change 250kpa to Roc |
|  |  |  |  |  | 62201310 |  | Change 100kpa to Doep |
|  |  |  |  |  | 62201320 |  | Exc Mat Disposal |
|  |  |  |  |  | 62201330 |  | Backiiil \& Compact |
|  |  |  |  |  | 62201340 |  | INDIRECTS |
|  |  |  |  | 62201400 |  |  | Assembly tower DC Segment.2 WA |
|  |  |  |  |  | 62201410 |  | Supply Steei Tower |
|  |  |  |  |  | 62201420 |  | Hellicopter |
|  |  |  |  |  | 62201430 |  | Assembly Type A |
|  |  |  |  |  | 62201440 |  | Assembly Type B |
|  |  |  |  |  | 82201450 |  | Assembly Type C |
|  |  |  |  |  | 62201460 |  | Assembly Type D |
|  |  |  |  |  | 62201470 |  | Assembly Type E |
|  |  |  |  |  | 62201480 |  | INDIRECTS |
|  |  |  |  | 62201500 |  |  | Erection towar DC Segment. 2 - WA |
|  |  |  |  |  | 62201510 |  | Hellicopter |
|  |  |  |  |  | 62201520 |  | Assembly Type A |
|  |  |  |  |  | 62201530 |  | Assembly Type B |
|  |  |  |  |  | 62201540 |  | Assembly Type C |
|  |  |  |  |  | 62201550 |  | Assembly Type D |
|  |  |  |  |  | 62201560 |  | Assembly Type E |
|  |  |  |  |  | 62201570 |  | Inspection Final |
|  |  |  |  |  | 62201580 |  | INDIRECTS |


| Level 1 | Level 2 | Leval 3 | Level 4 | Level 5 | Level 6 | Level 7 | Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | 82201600 |  |  | Counterpolse DC Segment.2-WA |
|  |  |  |  |  | 62201610 |  | Supply Counterpoise |
|  |  |  |  |  | 62201620 |  | Helico |
|  |  |  |  |  | 62201630 |  | Counterpoise |
|  |  |  |  |  | 62201640 |  | INDIRECTS |
|  |  |  |  | 62201700 |  |  | Conductors(4) DC Segment. 2-WA |
|  |  |  |  |  | 62201710 |  | Supply Insulator |
|  |  |  |  |  | 62201720 |  | Suppy conductor |
|  |  |  |  |  | 82201730 |  | Helico-Cond |
|  |  |  |  |  | 62201740 |  | Insulators install |
|  |  |  |  |  | 62201750 |  | Cabie puiler |
|  |  |  |  |  | 62201780 |  | Cable tensioneur |
|  |  |  |  |  | 62201770 |  | Sag. 8 clamp |
|  |  |  |  |  | 62201780 |  | Anchor Dead End |
|  |  |  |  |  | 62201790 |  | Jumper |
|  |  |  |  |  | 62201800 |  | Brace conductor |
|  |  |  |  |  | 62201810 |  | Move Team Puller-Tensioner |
|  |  |  |  |  | 62201820 |  | Temporary Protection |
|  |  |  |  |  | 62201830 |  | INDIRECTS |
|  |  |  |  | 62201840 |  |  | OHSW\&OPGW (1)DC Segment 2 WA |
|  |  |  |  |  | 62201850 |  | Helico |
|  |  |  |  |  | 62201860 |  | Supply OH-OP |
|  |  |  |  |  | 62201670 |  | Cabla OHSW |
|  |  |  |  |  | 62201860 |  | Cable OPGW |
|  |  |  |  |  | 62201882 |  | Fusion OPGW |
|  |  |  |  |  | 62201884 |  | Indirects |
|  |  |  |  | 62201890 |  |  | Indirect DC Segment.2 WA |
|  |  |  |  |  | 62201895 |  | MOB \& DEMOB |
|  |  |  |  |  | 62201900 |  | SITE OFFICE |
|  |  |  |  |  | 62201805 |  | PERIODIQUE HOMELEAVE |
|  |  |  |  |  | 62201910 |  | MARSHALLING |
|  |  |  |  |  | 62201915 |  | TRANS. PIER TO MARSHALLING |
|  |  |  |  |  | 62201920 |  | Access Road Class 3 |
|  |  |  |  |  | 62201925 |  | Campement 182 |
|  |  |  |  |  | 62201930 |  | Campement 3 |
|  |  |  |  |  | 62201935 |  | TEAM SUPPORT GENERAL |
|  |  |  |  |  | 62201940 |  | DISTRIBUTION TO THE SITE |
|  |  |  |  |  | 62201945 |  | MAINTENANCE ROAD |
|  |  |  |  |  | 62201950 |  | ADMINISTRATION \& PROFIT |
|  |  |  | 62202000 |  |  |  | IODCT Section 2 - 280km from PK250 to PK510 |
|  |  |  |  | 62202010 |  |  | Anchor drililing DC Segment 3 WA |
|  |  |  |  |  | 62202020 |  | Supply Anchor bar |
|  |  |  |  |  | 62202030 |  | Helico-Anchor |
|  |  |  |  |  | 62202040 |  | Anchor drilling DC Segment. 3 WA |
|  |  |  |  |  | 62202050 |  | Anchor Driiling move st |
|  |  |  |  |  | 62202060 |  | Grout |
|  |  |  |  |  | 62202070 |  | Manuffacturing guy |
|  |  |  |  |  | 62202080 |  | Anchor Test |
|  |  |  |  |  | 62202090 |  | INDIRECTS |
|  |  |  |  | 62202100 |  |  | Foundation DC Segment. 3 WA |
|  |  |  |  |  | 62202110 |  | Supply Stael found. |
|  |  |  |  |  | 62202120 |  | Helico |
|  |  |  |  |  | 62202130 |  | Type A-1 250kpa |
|  |  |  |  |  | 62202140 |  | Type A-2 100kpa |
|  |  |  |  |  | 62202150 |  | Type A Roc |
|  |  |  |  |  | 62202160 |  | Type B-1 250 kpa |
|  |  |  |  |  | 62202170 |  | Type B-2 100kpa |
|  |  |  |  |  | 62202180 |  | Type B Roc |
|  |  |  |  |  | 62202190 |  | Type C-1 250 kpa |
|  |  |  |  |  | 62202200 |  | Type C-2 100kpa |
|  |  |  |  |  | 62202210 |  | Type C Roc |
|  |  |  |  |  | 62202220 |  | Type D-1 250 kpa |
|  |  |  |  |  | 62202230 |  | Type D-2 100kpa |
|  |  |  |  |  | 62202240 |  | Type D Roc |
|  |  |  |  |  | 62202250 |  | Type E-1 250 kpa |
|  |  |  |  |  | 62202280 |  | Type E-2 100kpa |
|  |  |  |  |  | 62202270 |  | Type E Roc |
|  |  |  |  |  | 62202260 |  | Pile driving |
|  |  |  |  |  | 62202290 |  | Deep found Head pile |
|  |  |  |  |  | 62202300 |  | Change 250kpa to Roc |
|  |  |  |  |  | 82202310 |  | Change 100kpa to Deep |
|  |  |  |  |  | 62202320 |  | Exc Mat Disposai |
|  |  |  |  |  | 62202330 |  | Backfiil \& Compact |
|  |  |  |  |  | 62202340 |  | INDIRECTS |
|  |  |  |  | 62202400 |  |  | Assembly tower DC Segment.3 WA |
|  |  |  |  |  | 62202410 |  | Supply Steel Tower |
|  |  |  |  |  | 82202420 |  | Helicopter |
|  |  |  |  |  | 62202430 |  | Assembly Type A |
|  |  |  |  |  | 62202440 |  | Assembly Type B |
|  |  |  |  |  | 62202450 |  | Assembly Type C |
|  |  |  |  |  | 62202460 |  | Assembly Type D |
|  |  |  |  |  | 62202470 |  | Assembly Type E |
|  |  |  |  |  | 62202480 |  | INDIRECTS |
|  |  |  |  | 62202500 |  |  | Erection tower DC Segment. 3-WA |
|  |  |  |  |  | 62202510 |  | Hellicopter |
|  |  |  |  |  | 62202520 |  | Assembly Type A |
|  |  |  |  |  | 62202530 |  | Assembly Type B |
|  |  |  |  |  | 82202540 |  | Assembly Type C |


| Level 1 | Level 2 | Level 3 | Level 4 | Level 5 | Level 6 | Level 7 | Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 62202550 |  | Assembly Type D |
|  |  |  |  |  | 62202560 |  | Assembly Type E |
|  |  |  |  |  | 62202570 |  | Inspection Final |
|  |  |  |  |  | 62202580 |  | INDIRECTS |
|  |  |  |  | 62202600 |  |  | Counterpolse DC Segment.3-WA |
|  |  |  |  |  | 62202610 |  | Supply Counterpolse |
|  |  |  |  |  | 62202820 |  | Helico |
|  |  |  |  |  | 62202830 |  | Countappoise |
|  |  |  |  |  | 82202640 |  | INDIRECTS |
|  |  |  |  | 62202700 |  |  | Conductore(4) DC Segment.3-WA |
|  |  |  |  |  | 62202710 |  | Supply Insulator |
|  |  |  |  |  | 62202720 |  | Suppy conductor |
|  |  |  |  |  | 62202730 |  | Helico-Cond |
|  |  |  |  |  | 62202740 |  | Insulators install |
|  |  |  |  |  | 62202750 |  | Cable puiler |
|  |  |  |  |  | 62202780 |  | Cable tensioneur |
|  |  |  |  |  | 82202770 |  | Sag. 8 clamp |
|  |  |  |  |  | 62202780 |  | Anchor Dead End |
|  |  |  |  |  | 62202790 |  | Jumper |
|  |  |  |  |  | 62202800 |  | Brace conductor |
|  |  |  |  |  | 62202810 |  | Move Team Puilier-Tensioner |
|  |  |  |  |  | 62202820 |  | Temporary Protection |
|  |  |  |  |  | 62202830 |  | INDIRECTS |
|  |  |  |  | 62202840 |  |  | OHSW\&OPGW (1) DC Segment 3 WA |
|  |  |  |  |  | 62202850 |  | Helico |
|  |  |  |  |  | 62202860 |  | Supply OH-OP |
|  |  |  |  |  | 62202670 |  | Cable OHSW |
|  |  |  |  |  | 62202880 |  | Cable OPGW |
|  |  |  |  |  | 62202882 |  | Fusion OPGW |
|  |  |  |  |  | 62202884 |  | Indirects |
|  |  |  |  | 62202880 |  |  | Indirect DC Segment 3 WA |
|  |  |  |  |  | 62202895 |  | MOB \& DEMOB |
|  |  |  |  |  | 62202900 |  | SITE OFFICE |
|  |  |  |  |  | 62202905 |  | PERIODIQUE HOMELEAVE |
|  |  |  |  |  | 62202910 |  | MARSHALLING |
|  |  |  |  |  | 62202915 |  | TRANS. PIER TO MARSHALLING |
|  |  |  |  |  | 62202920 |  | Access Road Class 2 |
|  |  |  |  |  | 62202925 |  | Campement 1 |
|  |  |  |  |  | 62202930 |  | Campement 2 |
|  |  |  |  |  | 62202935 |  | TEAM SUPPORT GENERAL |
|  |  |  |  |  | 62202940 |  | DISTRIBUTION TO THE SITE |
|  |  |  |  |  | 62202945 |  | MAINTENANCE ROAD |
|  |  |  |  |  | 62202947 |  | Miligation |
|  |  |  |  |  | 62202948 |  | Reamenagement Final |
|  |  |  |  |  | 62202950 |  | ADMINISTRATION \& PROFIT |
|  |  |  | 62203000 |  |  |  | IODCT Section 3-180km from PK510 to Soldiers Pon |
|  |  |  |  | 82203005 |  |  | Anchor Driling DC Segment.4 WA |
|  |  |  |  |  | 62203010 |  | Supply Anchor bar |
|  |  |  |  |  | 62203020 |  | Helico-Anchor |
|  |  |  |  |  | 62203030 |  | Anchor drililing DC Segment. 4 WA |
|  |  |  |  |  | 62203040 |  | Anchor Drilling move sit |
|  |  |  |  |  | 62203050 |  | Grout |
|  |  |  |  |  | 62203060 |  | Manufacturing guys |
|  |  |  |  |  | 62203070 |  | Anchor Test |
|  |  |  |  |  | 62203080 |  | INDIRECTS |
|  |  |  |  | 62203100 |  |  | Foundation DC Segment. 4 WA |
|  |  |  |  |  | 62203110 |  | Supply Steel found. |
|  |  |  |  |  | 82203120 |  | Helico |
|  |  |  |  |  | 62203130 |  | Type A-1 250 kpa |
|  |  |  |  |  | 62203140 |  | Type A-2 100kpa |
|  |  |  |  |  | 62203150 |  | Type A Roc |
|  |  |  |  |  | 62203160 |  | Type B-1 250 kpa |
|  |  |  |  |  | 62203170 |  | Type B-2 100kpa |
|  |  |  |  |  | 62203180 |  | Type B Roc |
|  |  |  |  |  | 62203190 |  | Type C-1 250kpa |
|  |  |  |  |  | 62203200 |  | Type C-2 100kpa |
|  |  |  |  |  | 62203210 |  | Type C Roc |
|  |  |  |  |  | 62203220 |  | Type D-1 250 kpa |
|  |  |  |  |  | 62203230 |  | Type D-2 100kpa |
|  |  |  |  |  | 82203240 |  | Type D Roc |
|  |  |  |  |  | 62203250 |  | Type E-1 250kpa |
|  |  |  |  |  | 62203280 |  | Type E.2 100kpa |
|  |  |  |  |  | 62203270 |  | Type E Roc |
|  |  |  |  |  | 62203280 |  | Pilie driving |
|  |  |  |  |  | 62203290 |  | Deep found Head pila |
|  |  |  |  |  | 62203300 |  | Change 250kpa to Roc |
|  |  |  |  |  | 62203310 |  | Change 100kpa to Doep |
|  |  |  |  |  | 62203320 |  | Exc Mat Disposal |
|  |  |  |  |  | 62203330 |  | Backilil \& Compact |
|  |  |  |  |  | 62203340 |  | INDIRECTS |
|  |  |  |  | 62203400. |  |  | Assembly tower DC Segment. 4 WA |
|  |  |  |  |  | 62203410 |  | Supply Steol Tower |
|  |  |  |  |  | 62203420 |  | Heilicopter |
|  |  |  |  |  | 62203430 |  | Assembly Type A |
|  |  |  |  |  | 62203440 |  | Assembly Type B |
|  |  |  |  |  | 62203450 |  | Assembly Type C |
|  |  |  |  |  | 62203460 |  | Assembly Type D |
|  |  |  |  |  | 62203470 |  | Assembly Type E |


| Leval 1 | Level 2 | Level 3 | Level 4 | Level 5 | Level 6 | Leovel 7 | Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 62203480 |  | INDIRECTS |
|  |  |  |  | 62203500 |  |  | Erection tower DC Segment.4-WA |
|  |  |  |  |  | 62203510 |  | Helicopter |
|  |  |  |  |  | 62203520 |  | Assembly Type A |
|  |  |  |  |  | 62203530 |  | Assembly Type B |
|  |  |  |  |  | 62203540 |  | Assembly Type C |
|  |  |  |  |  | 62203550 |  | Assembly Type D |
|  |  |  |  |  | 82203580 |  | Assembly Type E |
|  |  |  |  |  | 62203570 |  | inspection Finai |
|  |  |  |  |  | 62203580 |  | INDIRECTS |
|  |  |  |  | 62203600 |  |  | Counterpoise DC Segment. 4 - WA |
|  |  |  |  |  | 62203810 |  | Supply Counterpoise |
|  |  |  |  |  | 62203620 |  | Helico |
|  |  |  |  |  | 62203830 |  | Counterpoise |
|  |  |  |  |  | 62203840 |  | INDIRECTS |
|  |  |  |  | 62203700 |  |  | Conductors(4) DC Segment.4-WA |
|  |  |  |  |  | 62203710 |  | Supply Insulator |
|  |  |  |  |  | 62203720 |  | Suppy conductor |
|  |  |  |  |  | 62203730 |  | Helico-Cond |
|  |  |  |  |  | 62203740 |  | Insulators Instail |
|  |  |  |  |  | 62203750 |  | Cable pulier |
|  |  |  |  |  | 62203780 |  | Cabie tensioneur |
|  |  |  |  |  | 62203770 |  | Sag. 8 clamp |
|  |  |  |  |  | 62203780 |  | Anchor Dead End |
|  |  |  |  |  | 62203790 |  | Jumper |
|  |  |  |  |  | 62203800 |  | Brace conductor |
|  |  |  |  |  | 62203810 |  | Move Team Puiler-Tensioner |
|  |  |  |  |  | 62203820 |  | Temporary Prolection |
|  |  |  |  |  | 62203830 |  | INDIRECTS |
|  |  |  |  | 62203840 |  |  | OHSW8OPGW (1) DC Segment 4 WA |
|  |  |  |  |  | 62203850 |  | Heilico |
|  |  |  |  |  | 62203860 |  | Supply OH-OP |
|  |  |  |  |  | 62203870 |  | Cable OHSW |
|  |  |  |  |  | 62203880 |  | Cable OPGW |
|  |  |  |  |  | 62203882 |  | Fusion OPGW |
|  |  |  |  |  | 62203884 |  | Indirects |
|  |  |  |  | 62203890 |  |  | indirect DC Segment 4 WA |
|  |  |  |  |  | 62203695 |  | MOB \& DEMOB |
|  |  |  |  |  | 62203900 |  | SITE OFFICE |
|  |  |  |  |  | 62203905 |  | PERIODIQUE HOMELEAVE |
|  |  |  |  |  | 82203910 |  | MARSHALLING |
|  |  |  |  |  | 62203915 |  | TRANS. PIER TO MARSHALLING |
|  |  |  |  |  | 62203920 |  | Access Road Class 2 |
|  |  |  |  |  | 62203925 |  | Campement |
|  |  |  |  |  | 62203930 |  | Campement 1 |
|  |  |  |  |  | 62203935 |  | TEAM SUPPORT GENERAL |
|  |  |  |  |  | 62203940 |  | DISTRIBUTION TO THE SITE |
|  |  |  |  |  | 62203945 |  | MAINTENANCE ROAD |
|  |  |  |  |  | 62203947 |  | Mitigation |
|  |  |  |  |  | 62203948 |  | Reamenagement Final |
|  |  |  |  |  | 82203950 |  | ADMINISTRATION \& PROFIT |
|  |  |  | 62204000 |  |  |  | IODCT - Auxiliary work |
|  |  |  |  | 62204050 |  |  | Material Procurement Logistics |
|  |  |  |  | 62204100 |  |  | Marshalling Yards (Setup and Operation) |
|  |  |  |  | 82204150 |  |  | Construction and EPCM personnel Accommodations |
|  |  |  |  | 62204200 |  |  | Communication |
|  |  |  |  | 62204250 |  |  | Sites Offices and Supervision |
|  |  |  |  | 62204300 |  |  | Laboratory Costs |
|  |  |  |  | 62204350 |  |  | Materials and supply transport |
|  |  |  |  | 62204400 |  |  | EPCM Costs (Site \& StWohn's) |
|  |  |  |  | 62204450 |  |  | Constiruction Permilting Costs |
|  |  |  |  | 62204500 |  |  | Other Permititing Costs |
|  |  |  |  | 62204550 |  |  | Construction QAOC |
|  |  |  |  | 62204600 |  |  | Commissioning and turnover |
|  |  |  |  | 62204650 |  |  | Environmentai Monitoring |
|  |  |  |  | 62204700 |  |  | Helicopter costs |
|  |  |  |  | 62204750 |  |  | QA \& QC Costa (Nalcor, EPCM \& Contractor) |
|  |  |  | 82205000 |  |  |  | Clear DC line LRM \& Estin Segm 6 |
|  |  |  |  | 82205010 |  |  | Feller buncher |
|  |  |  |  | 62205020 |  |  | Manual |
|  |  |  |  | 62205030 |  |  | Stockppliing in Box |
|  |  |  |  | 82205040 |  |  | Accas |
|  |  |  |  | 62205050 |  |  | Fascine stacking |
|  |  |  |  | 62205060 |  |  | Fascine implement |
|  |  |  |  | 02205070 |  |  | Temporary bridge |
|  |  |  |  | 82205080 |  |  | Culverts |
|  |  |  |  | 62205090 |  |  | Maintenance access |
|  |  |  |  | 62205100 |  |  | Team Support |
|  |  |  |  | 82205110 |  |  | Supervision |
|  |  |  |  | 62205120 |  |  | Indirects |
|  |  |  | 62206000 |  |  |  | Clear DC line LRM Segm 5 |
|  |  |  |  | 82206010 |  |  | Feilar buncher |
|  |  |  |  | - 82208020 |  |  | Manual |
|  |  |  |  | 62206030 |  |  | Stockppliing in Box |
|  |  |  |  | 62206040 |  |  | Acces |
|  |  |  |  | 82206050 |  |  | Fascine stacking |
|  |  |  |  | 82208060 |  |  | Fascine impiement |
|  |  |  |  | 62206070 |  |  | Temporary bridge |


| Level 1 | Level 2 | Level 3 | Level 4 | Level 5 | Level 6 | Level 7 | Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | 62206080 |  |  | Culverts |
|  |  |  |  | 62206090 |  |  | Maintenance access |
|  |  |  |  | 82208100 |  |  | Team Support |
|  |  |  |  | 62206110 |  |  | Supervision |
|  |  |  |  | 62208120 |  |  | Indirects |
|  |  |  | 62207000 |  |  |  | Clear DC line NL Estn Segm 7 |
|  |  |  |  | 62207010 |  |  | Feller buncher |
|  |  |  |  | 62207020 |  |  | Manual |
|  |  |  |  | 62207030 |  |  | Stockpliling In Box |
|  |  |  |  | 62207040 |  |  | Acces |
|  |  |  |  | 62207050 |  |  | Fascine stacking |
|  |  |  |  | 62207060 |  |  | Fascine Implement |
|  |  |  |  | 62207070 |  |  | Temporary bridge |
|  |  |  |  | 62207080 |  |  | Culverts |
|  |  |  |  | 62207090 |  |  | Maintenance access |
|  |  |  |  | 62207100 |  |  | Team Support |
|  |  |  |  | 62207110 |  |  | Supervision |
|  |  |  |  | 62207.120 |  |  | Indirects |
|  |  |  | 62208000 |  |  |  | Ciear DC line NL Estn Segm 8 |
|  |  |  |  | 62208010 |  |  | Feiler buncher |
|  |  |  |  | 62208020 |  |  | Manial |
|  |  |  |  | 62208030 |  |  | Stockpliling in Box |
|  |  |  |  | 62208040 |  |  | Acces |
|  |  |  |  | 62208050 |  |  | Fascine stacking |
|  |  |  |  | 62208060 |  |  | Fascine impiement |
|  |  |  |  | 62208070 |  |  | Temporay bridge |
|  |  |  |  | 62208080 |  |  | Culverts |
|  |  |  |  | 62208090 |  |  | Maintenancea access |
|  |  |  |  | 62208100 |  |  | Team Support |
|  |  |  |  | 82208110 |  |  | Supervision |
|  |  |  |  | 62208120 |  |  | indirects |
|  |  |  | 82208000 |  |  |  | Clear DC IIne LRM Segm 4 |
|  |  |  |  | 62208010 |  |  | Failer buncher |
|  |  |  |  | 62209020 |  |  | Manual |
|  |  |  |  | 62209030 |  |  | Stackpling In Box |
|  |  |  |  | 62209040 |  |  | Acces |
|  |  |  |  | 62209050 |  |  | Fascine stacking |
|  |  |  |  | 62209060 |  |  | Fascine implement |
|  |  |  |  | 62209070 |  |  | Temporary bridge |
|  |  |  |  | 62209080 |  |  | Culverts |
|  |  |  |  | 62209090 |  |  | Maintenarice access |
|  |  |  |  | 82209100 |  |  | Team Support |
|  |  |  |  | 62209110 |  |  | Supervision |
|  |  |  |  | 62209120 |  |  | Indirects |
|  |  | 62700000 |  |  |  |  | Labrador Overiand DC Transmission (LODCT) |
|  |  |  | 62701000 |  |  |  | LODCT Section 1-180km from MF to PK160 |
|  |  |  |  | 62701110 |  |  | Survey |
|  |  |  |  | 62701120 |  |  | Geotechnical |
|  |  |  |  | 62701130 |  |  | Accoss roads and Crossings |
|  |  |  |  | 62701140 |  |  | Clearing and Logging |
|  |  |  |  | 62701150 |  |  | Foundation Works |
|  |  |  |  |  | 62701151 |  | Supply and instail Anchors |
|  |  |  |  |  |  | 62700150 | Supply Anchor Bar |
|  |  |  |  |  |  | 62700151 | Helicopter Anchor |
|  |  |  |  |  |  | 62700152 | Anchor Drilling |
|  |  |  |  |  |  | 62700153 | Anchor Drilling Move sit |
|  |  |  |  |  |  | 62700154 | Grout |
|  |  |  |  |  |  | 62700155 | Manufacturing guys. |
|  |  |  |  |  |  | 62700156 | Anchor Test |
|  |  |  |  |  |  | 62700157 | Indirects |
|  |  |  |  |  | 62701152 |  | Supply and Install Grillage |
|  |  |  |  |  | 62701153 |  | Supply and install Concrete \& Rebar |
|  |  |  |  | 62701210 |  |  | Towers |
|  |  |  |  |  | 62701211 |  | Procurement of tower steel (Tower packaged) |
|  |  |  |  |  | 62701212 |  | Procurement of guy wires |
|  |  |  |  |  | 62701213 |  | Transport for construction (handiling at yard and t |
|  |  |  |  |  | 62701214 |  | Assembly |
|  |  |  |  |  | 62701215 |  | Erection |
|  |  |  |  | 62701310 |  |  | insulators and hardware |
|  |  |  |  |  | 62701311 |  | Supply and instail |
|  |  |  |  |  | 62701312 |  | Transport for construction (handling at yard and t |
|  |  |  |  | 62701410 |  |  | Conductors, Reels and Accessories |
|  |  |  |  |  | 62701411 |  | Supply and Instail |
|  |  |  |  |  | 62701412 |  | Transport for construction (handling at yard and t |
|  |  |  |  | 62701510 |  |  | Opticai Power Ground Wire (OPGW \& Accessories |
|  |  |  |  | 82701610 |  |  | Overhead Shiodd Wire (OHSW \& Accessories |
|  |  |  |  | 627017.10 |  |  | Grounding |
|  |  |  |  | 62701810 |  |  | Remedlai Work |
|  |  |  |  | 82701910 |  |  | Counterpoise |
|  |  |  |  | 82701998 |  |  | Indirect |
|  |  |  | 62702000 |  |  |  | LODCT Section 2 - PK160 to SOBI |
|  |  |  |  | 627021.10 |  |  | Survey |
|  |  |  |  | 62702120 |  |  | Geotechnical |
|  |  |  |  | 62702130 |  |  | Access roads and Crossings |
|  |  |  |  | 62702140 |  |  | Clearing and Logging |
|  |  |  |  | 62702150 |  |  | Foundation Works |
|  |  |  |  |  | 62702151 |  | Supply and Instail Anchors |
|  |  |  |  |  |  | 62700250 | Supply Anchor Bar |


| Level 1 | Level 2 | Level 3 | Level 4 | Level 5 | Level 6 | Level 7 | Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | 62700251 | Helicopter Anchor |
|  |  |  |  |  |  | 62700252 | Anchor Drilling |
|  |  |  |  |  |  | 62700253 | Anchor Drilling Move stt |
|  |  |  |  |  |  | 62700254 | Grout |
|  |  |  |  |  |  | 62700255 | Manufacturing guys |
|  |  |  |  |  |  | 62700256 | Anchor Test |
|  |  |  |  |  |  | 62700257 | Indirects |
|  |  |  |  |  | 62702152 |  | Supply and Install Grillage |
|  |  |  |  |  | 62702153 |  | Supply and Instail Concrete \& Rebar |
|  |  |  |  | 62702210 |  |  | Towers |
|  |  |  |  |  | 62702211 |  | Procurement of tower steel (Tower packaged) |
|  |  |  |  |  | 62702212 |  | Procurement of guy wires |
|  |  |  |  |  | 62702213 |  | Transport for construction (handiling at yard and t |
|  |  |  |  |  | 62702214 |  | Assembly |
|  |  |  |  |  | 62702215 |  | Erection |
|  |  |  |  | 62702310 |  |  | Insulators and hardware |
|  |  |  |  |  | 62702311 |  | Supply and Install |
|  |  |  |  |  | 62702312 |  | Transport for construction (handiling at yard and I |
|  |  |  |  | 62702410 |  |  | Conductors, Reels and Accessories |
|  |  |  |  |  | 62702411 |  | Supply and Install |
|  |  |  |  |  | 62702412 |  | Transport for construction (handling at yard and i |
|  |  |  |  | 62702510 |  |  | Optical Power Ground Wire (OPGW $\&$ Accassories |
|  |  |  |  | 62702810 |  |  | Overhead Shield Wire (OHSW) \& Accessories |
|  |  |  |  | 62702710 |  |  | Grounding |
|  |  |  |  | 62702810 |  |  | Remedial Work |
|  |  |  |  | 62702910 |  |  | Counterpoise |
|  |  |  | 62703000 |  |  |  | LODCT - Auxillary work |
|  |  |  |  | 62703050 |  |  | Matertal Procurement Logistics |
|  |  |  |  | 62703100 |  |  | Marshalling Yards (Setup and Operation) |
|  |  |  |  | 62703150 |  |  | Construction and EPCM personnel Accommodations |
|  |  |  |  | 62703200 |  |  | Communication |
|  |  |  |  | 62703250 |  |  | Sties Offices and Supervislon |
|  |  |  |  | 62703300 |  |  | Laboratory Costs |
|  |  |  |  | 62703350 |  |  | Materials and supply transport |
|  |  |  |  | 62703400 |  |  | EPCM Costs (Site \& St-John's) |
|  |  |  |  | 62703450 |  |  | Construction Permitting Costs |
|  |  |  |  | 62703500 |  |  | Other Permilting Costs |
|  |  |  |  | 62703550 |  |  | Construction QAQC |
|  |  |  |  | 62703600 |  |  | Commissioning and turnover |
|  |  |  |  | 62703650 |  |  | Environmental Monitoring |
|  |  |  |  | 62703700 |  |  | Helicopter costs |
|  |  |  |  | 62703750 |  |  | OA \& OC Costa (Nalcor, EPCM \& Contractor) |
|  |  |  | 62704000 |  |  |  | Clear DC Lab Segm 1 \& 2 |
|  |  |  |  | 62704010 |  |  | Feiller buncher |
|  |  |  |  | 62704020 |  |  | Manual |
|  |  |  |  | 62704030 |  |  | Stockpplling In Box |
|  |  |  |  | 82704040 |  |  | Accas |
|  |  |  |  | 62704050 |  |  | Fascine stacking |
|  |  |  |  | 62704080 |  |  | Fascine implement |
|  |  |  |  | 62704070 |  |  | Temporary bridge |
|  |  |  |  | 62704080 |  |  | Cubverts |
|  |  |  |  | 62704090 |  |  | Maintenance access |
|  |  |  |  | 62704100 |  |  | Team Support |
|  |  |  |  | 62704110 |  |  | Supervision |
|  |  |  |  | 62704120 |  |  | Indirects |
|  |  |  | 62705000 |  |  |  | Clear DC Lab Sobl Segm 3 |
|  |  |  |  | 62705010 |  |  | Feller buncher |
|  |  |  |  | 62705020 |  |  | Manual |
|  |  |  |  | 62705030 |  |  | Stockplling In Box |
|  |  |  |  | 62705040 |  |  | Acces |
|  |  |  |  | 62705050 |  |  | Faschne stacking |
|  |  |  |  | 62705060 |  |  | Fasclne implament |
|  |  |  |  | 62705070 |  |  | Temporary bridge |
|  |  |  |  | 62705080 |  |  | Culverts |
|  |  |  |  | 62705090 |  |  | Maintenance access |
|  |  |  |  | 62705100 |  |  | Team Support |
|  |  |  |  | 62705110 |  |  | Supervision |
|  |  |  |  | 62705120 |  |  | Indirects |
|  | 63000000 |  |  |  |  |  | Electrode Lines |
|  |  | 63100000 |  |  |  |  | Electrode Line-Labrador |
|  |  |  | 63101000 |  |  |  | Framing Wood Pole LAB |
|  |  |  |  | 63101010 |  |  | Supply Wood Pole |
|  |  |  |  | 63101020 |  |  | Susp. 1 Post |
|  |  |  |  | 63101030 |  |  | Dead End, 1/Post |
|  |  |  |  | 63101040 |  |  | Dead End, 2 Post |
|  |  |  |  | 63101050 |  |  | Dead End, 3 Post |
|  |  |  |  | 63101080 |  |  | Indrects |
|  |  |  | 63102000 |  |  |  | Implement Wood Pota LAB |
|  |  |  |  | 63102010 |  |  | Supply Post |
|  |  |  |  | 63102020 |  |  | Str. Earth 1 Post |
|  |  |  |  | 63102030 |  |  | Str. Rock 1 Post |
|  |  |  |  | 63102040 |  |  | Str, Earth D-end 2 Post |
|  |  |  |  | 63102050 |  |  | Str. Rock 2 Post |
|  |  |  |  | 63102060 |  |  | Str. Earth D-end 3 Post |
|  |  |  |  | 63102070 |  |  | Str. Rock 3 Post |
|  |  |  |  | 63102080 |  |  | Backilil \& Compact |
|  |  |  |  | 63102080 |  |  | Indiracts |
|  |  |  | 63103600 |  |  |  | Counterpoise DC Elect LAB |


| Level 1 | Level 2 | \|Level 3 | Level 4 | Level 5 | Level 6 | Level 7 | Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | 63103610 |  |  | Supply Counterpoise |
|  |  |  |  | 63103820 |  |  | Helico |
|  |  |  |  | 63103630 |  |  | Counterpolse |
|  |  |  |  | 63103840 |  |  | INDIRECTS |
|  |  |  | 63103700 |  |  |  | Conductors Electrode Lline LAB |
|  |  |  |  | 83103710 |  |  | Supply Insulator |
|  |  |  |  | 63103720 |  |  | Suppy conductor |
|  |  |  |  | 63103740 |  |  | Insiulators Install |
|  |  |  |  | 63103750 |  |  | Cable puller |
|  |  |  |  | 63103760 |  |  | Cable tenslonour |
|  |  |  |  | 63103770 |  |  | Sag.\& clamp |
|  |  |  |  | 63103780 |  |  | Anchor Dead End |
|  |  |  |  | 63103790 |  |  | Jumper |
|  |  |  |  | 63103810 |  |  | Move Team Puller-Tensioner |
|  |  |  |  | 63103820 |  |  | Temporary Protection |
|  |  |  |  | 63103830 |  |  | INDIRECTS |
|  |  |  | 63103840 |  |  |  | OHSW:OPGW Electrode Line LAB |
|  |  |  |  | 63103850 |  |  | Hellico |
|  |  |  |  | 63103880 |  |  | Supply OH-OP |
|  |  |  |  | 63103870 |  |  | Cable OHSW |
|  |  |  |  | 63103880 |  |  | Cable OPGW |
|  |  |  |  | 63103882 |  |  | Fusion OPGW |
|  |  |  |  | 63103884 |  |  | Indirects |
|  |  |  | 63103880 |  |  |  | Indirect DC Electrode Line LAB |
|  |  |  |  | 63103895 |  |  | MOB \& DEMOB |
|  |  |  |  | 63103900 |  |  | SITE OFFICE |
|  |  |  |  | 63103905 |  |  | PERIODIQUE HOMELEAVE |
|  |  |  |  | 63103910 |  |  | MARSHALLING |
|  |  |  |  | 63103915 |  |  | TRANS, PIER TO MARSHALLING |
|  |  |  |  | 63103925 |  |  | Camperment |
|  |  |  |  | 83103935 |  |  | TEAM SUPPORT GENERAL |
|  |  |  |  | 63103940 |  |  | DISTRIBUTION TO THE SITE |
|  |  |  |  | 83103945 |  |  | MAINTENANCE ROAD |
|  |  |  |  | 83103950 |  |  | ADMINISTRATION \& PROFIT |
|  |  | 63200000 |  |  |  |  | Electrode Line - Newfoundland East |
|  |  |  | 63201000 |  |  |  | Framing Wood Pole NL |
|  |  |  |  | 63201010 |  |  | Supply Wood Pole |
|  |  |  |  | 63201020 |  |  | Susp. 1 Poost |
|  |  |  |  | 63201030 |  |  | Dead End. 1 Post |
|  |  |  |  | 63201040 |  |  | Doad End 2 Post |
|  |  |  |  | 63201050 |  |  | Dead End. 3 Post |
|  |  |  |  | 83201060 |  |  | Indrects |
|  |  |  | 63202000 |  |  |  | Implement Wood Pole NL |
|  |  |  |  | 63202010 |  |  | Supply Post |
|  |  |  |  | 63202020 |  |  | Str. Earth 1 Post |
|  |  |  |  | 83202030 |  |  | Str. Rock 1 Post |
|  |  |  |  | 63202040 |  |  | Str. Earth D-end 2 Post |
|  |  |  |  | 63202050 |  |  | Str. Rock 2 Post |
|  |  |  |  | 63202080 |  |  | Str. Earth D-ond 3 Post |
|  |  |  |  | 63202070 |  |  | Str: Rock 3 Post |
|  |  |  |  | 63202080 |  |  | Backilil \& Compact |
|  |  |  |  | 63202090 |  |  | Indrects |
|  |  |  | 63203700 |  |  |  | Conductors Electrode Line NL |
|  |  |  |  | 63203710 |  |  | Supply Insulator |
|  |  |  |  | 63203720 |  |  | Suppy conductor |
|  |  |  |  | 63203740 |  |  | Insulators install |
|  |  |  |  | 63203750 |  |  | Cable puller |
|  |  |  |  | 63203760 |  |  | Cable tensioneur |
|  |  |  |  | 63203770 |  |  | Seq.\& clamp |
|  |  |  |  | 63203780 |  |  | Anchor Dead End |
|  |  |  |  | 63203790 |  |  | Jumper |
|  |  |  |  | 63203810 |  |  | Move Team Pullar-Tensioner |
|  |  |  |  | 63203820 |  |  | Temporary Protection |
|  |  |  |  | 63203830 |  |  | INDIRECTS |
|  |  |  | 63203890 |  |  |  | Indirect DC Electrode Line NL |
|  |  |  |  | 83203895 |  |  | MOB\&DEMOB |
|  |  |  |  | 63203900 |  |  | SITE OFFICE |
|  |  |  |  | 63203805 |  |  | PERIODIQUE HOMELEAVE |
|  |  |  |  | 63203910 |  |  | MARSHALLING |
|  |  |  |  | 63203915 |  |  | TRANS, PIER TO MARSHALILING |
|  |  |  |  | 63203925 |  |  | Campement |
|  |  |  |  | 63203935 |  |  | TEAM SUPPORT GENERAL |
|  |  |  |  | 83203940 |  |  | DISTRIBUTION TO THE SITE |
|  |  |  |  | 63203945 |  |  | MAINTENANCE ROAD |
|  |  |  |  | 63203950 |  |  | ADMINISTRATION \& PROFIT |
| 71200000 |  |  |  |  |  |  | New Synchronous Condenser |
|  | 71200100 |  |  |  |  |  | Naw Synchronous Condenser-Civil |
|  |  | 71200110 |  |  |  |  | Clvil Works |
|  |  | 71200120 |  |  |  |  | Concrete Works |
|  |  | 71200130 |  |  |  |  | Structural Steel Works |
|  |  | 71200140 |  |  |  |  | Architectural/Buildings |
|  |  | 71200150 |  |  |  |  | Mechanical Services |
|  |  | 71200180 |  |  |  |  | Mechanlcal Equipment |
|  |  | 71200170 |  |  |  |  | Indrect |
|  | 71200200 |  |  |  |  |  | Now Synchronous Condenser-Equipment |
| 80000000 |  |  |  |  |  |  | DC Specialties |
|  | 80009000 |  |  |  |  |  | Testing for Major Electrical Equipment |


| Level 1 | Level 2 | Level 3 | Level 4 | Level 5 | Level 6 | Level 7 | Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 82000000 |  |  |  |  |  | DC Speclalties - Converter Stations |
|  |  | 82100000 |  |  |  |  | Labrador Converter Slation (near MF) |
|  |  |  | 82100100 |  |  |  | labrador Converter Station - Civil |
|  |  |  |  | 82100110 |  |  | Cwil Works |
|  |  |  |  | 82100120 |  |  | Concrele Works |
|  |  |  |  | 82100130 |  |  | Structural Steel Works |
|  |  |  |  | - 82100140 |  |  | Archiltectura/Bulldings |
|  |  |  |  | 82100150 |  |  | Mechanical Services |
|  |  |  |  | 62100160 |  |  | Mechanical Equlpment |
|  |  |  | 82100200 |  |  |  | labrador Converter Station - Equip\&Elac |
|  |  |  |  | 82100999 |  |  | Indirects |
|  |  | 82200000 |  |  |  |  | Soldiers Pond Converter Station |
|  |  |  | 82200100 |  |  |  | Soldiers Pond Converter Station - Civil |
|  |  |  |  | 82200110 |  |  | Cwil Works |
|  |  |  |  | 82200120 |  |  | Concrete Works |
|  |  |  |  | 82200130 |  |  | Structural Sleel Works |
|  |  |  |  | 82200140 |  |  | Archilectura/Building |
|  |  |  |  | 82200150 |  |  | Mechanlcal Services |
|  |  |  |  | 82200180 |  |  | Mechanical Equipment |
|  |  |  | 82200200 |  |  |  | Soldiers Pond Converter Station - Equip\&Elec |
|  |  |  |  | 82200999 |  |  | Indirects |
|  | 85000000 |  |  |  |  |  | DC Speclattes - Transition Compounds |
|  |  | 85100000 |  |  |  |  | Transililon Compound - Labrador |
|  |  |  | 85100100 |  |  |  | Transition Compound - Labrador - Civil |
|  |  |  |  | 85100110 |  |  | Civll Works |
|  |  |  |  | 85100120 |  |  | Concrete Works |
|  |  |  |  | 85100130 |  |  | Structural Steel Works |
|  |  |  |  | 65100140 |  |  | Archilectura/Builiding |
|  |  |  |  | 85100150 |  |  | Mechanlcal Services |
|  |  |  |  | 85100160 |  |  | Mechanical Equlpment |
|  |  |  | 85100200 |  |  |  | Transilion Compound -Labrador - Equip\&Elec |
|  |  |  |  | 85100999 |  |  | Indirect |
|  |  | 85200000 |  |  |  |  | Transilion Compound - Northem Peninsula (NP) |
|  |  |  | 85200100 |  |  |  | Transilion Compound - NP - Civil |
|  |  |  |  | 852001.10 |  |  | CivilWorks |
|  |  |  |  | 85200120 |  |  | Concrete Works |
|  |  |  |  | 85200130 |  |  | Strüctural Steel Works |
|  |  |  |  | 85200140 |  |  | Archliectura/Bülding |
|  |  |  |  | 85200150 |  |  | Mechanlcal Services |
|  |  |  |  | 85200160 |  |  | Mechanlcal Equipment |
|  |  |  | 85200200 |  |  |  | Transiltion Compound - NP - Equlp\&Elec |
|  |  |  |  | 85200999 |  |  | Indirect |
|  | 86000000 |  |  |  |  |  | DC Specialtes - Electrodes |
|  |  | 86100000 |  |  |  |  | Electrode Labrador |
|  |  |  | 88101000 |  |  |  | Civil Works |
|  |  |  |  | 86101100 |  |  | Direct |
|  |  |  |  | 88101200 |  |  | Indirect |
|  |  |  | 86102000 |  |  |  | Electrical Works |
|  |  |  |  | 86102100 |  |  | Direct |
|  |  |  |  | 88102200 |  |  | Indreat |
|  |  | 86200000 |  |  |  |  | Electrode Newfoundland East |
| 90000000 |  |  |  |  |  |  | Other Speciafties - General |
|  | 92000006 |  |  |  |  |  | Operations Telecommunications Systems |
|  |  | 92200000 |  |  |  |  | Operatons Telecommunication System - Muskrat Fall |
|  |  |  | 92200100 |  |  |  | Muskrat Falls Microwave System |
|  |  |  | 82200200 |  |  |  | Muskrat Falls Fiber Optic Terminal Equlpment |
|  |  |  | 82200300 |  |  |  | Operations Telecommunications Systems |
|  |  | 92300000 |  |  |  |  | Operations Telecommunication System - Island Link |
|  |  |  | 92300100 |  |  |  | Island Link Microwave System |
|  |  |  | 92300200 |  |  |  | Island LInk Fiber Optic Teminal Equipment |
| 99000000 |  |  |  |  |  |  | ESTIMATORINDIRECTS |
|  | 99100000 |  |  |  |  |  | DAUBERSMITH - Reinforced Concrate Structures |
|  |  | 99123600 |  |  |  |  | Transilion Structures Concrete Indirects |
|  |  |  | 99123610 |  |  |  | Mab \& Demob |
|  |  |  | 99123620 |  |  |  | Supervision |
|  |  |  | 99123630 |  |  |  | Temporary Buldilings |
|  |  |  | 99123640 |  |  |  | Utillities (Alr, Water, Power) |
|  |  |  | 99123650 |  |  |  | Support Equlpment |
|  |  |  | 89123680 |  |  |  | Administration \& Profit |
|  |  | 99124100 |  |  |  |  | Spillway Concrete Structure Indirects |
|  |  |  | 99124110 |  |  |  | Mob \& Demob |
|  |  |  | 99124120 |  |  |  | Supervision |
|  |  |  | 99124130 |  |  |  | Temporary Bulldings |
|  |  |  | 99124140 |  |  |  | Utillties (Alr, Water, Power) |
|  |  |  | 99124150 |  |  |  | Support Equlpment |
|  |  |  | 99124160 |  |  |  | Adminlistration \& Profit |
|  |  | 99132200 |  |  |  |  | Intake Concrete Structure Indirects |
|  |  |  | 99132210 |  |  |  | Mob \& Demob |
|  |  |  | 99132220 |  |  |  | Supervision |
|  |  |  | 99132230 |  |  |  | Temporary Bulldings |
|  |  |  | 99132240 |  |  |  | Utillites (Alr, Water, Power) |
|  |  |  | 89132250 |  |  |  | Support Equipment |
|  |  |  | 99132260 |  |  |  | Administration \& Profit |
|  |  | 89133100 |  |  |  |  | Powerhouse Substructure Concrete Indirecis |
|  |  |  | 99133110 |  |  |  | Mob \& Demob |
|  |  |  | 99133120 |  |  |  | Supervision |
|  |  |  | 99133130 |  |  |  | Temporary Bulldings |


| Level 1 | Level 2 | Level 3 | Level 4 | Level 5 | Level 6 | Level 7 | Description |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  |  | 99133140 |  |  |  | Utilities (Air, Water, Power) |
|  |  |  | 99133150 |  |  |  | Support Equipment |
|  |  |  | 99133180 |  |  |  | Administration \& Profil |


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Appendix 2

## Nalcor Physical Component coding structure

Lower Churchill Project
Physical Components by Project
For Use in Coding
(Dec14 Edit)




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## Appendix 3

CCE Labour Rates

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> * The total per hour is the base rate + taxes + fringes. It DOES NOT include worker's comp computation, that component will be added to burden only when the labor cost resource is entered into the estimate.

> Labor with a unit other than ' $M H$ ' is in italics.

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## Appendix 4

## CCE Equipment Rates



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| 8AIRCRANE | Helicopter-Air Crane |
| :--- | :--- |
| 8ATJH60 | Jackhammer 60\# |
| 8ATRB30 | Rivet Buster 30\# |
| 8BC | Bomag Compactor |
| 8BCT1 | Cable Breaker Timberland |
| 8BH225B | Backhoe CMW cat 225B |
| 8BH315 | Backhoe 315 |
| 8BH320 | Backhoe 320 |
| 8BH325B | BACKHOE C/W CAT 325B |
| 8BH345B | BACKHOE CNW CAT 345B |
| 8BH365B | BACKHOE CAT 365B |
| 8CABPL45B | CabletteTimberland PI45b |
| 8CCCCP | CGC Conc Pump |
| 8CCCONCT10 | TRUCK CONCRETE 8M3 |
| 8CCONCCT36 | Concrete Trowel 36" |
| 8CCONCGM16 | Grout Mixer 16cf |
| 8CCONCHCGEN | Concrete Hi-Cycle Generator |
| 8CCONCHCVIB | Concrete Hi-Cycle Vibrator |
| 8CCONCP2 | TRUCK CONCRETE PUMP R |
| 8CCONCP52 | Concrete Pump Boom 52m |
| 8CCONCPTC | Concrete Pump Truck Chassi |
| 8CCONCRS | Concrete Roller Screed |
| 8CCONCVIB | Concrete Vibrator |
| 8CCV | Concrete Vibrator SE |
| 8CH22 | Chipper 22 inch |
| 8CMPD0150 | Compressor NM 150 |
| 8CMPD0185 | Compressor Diesel 185 C.F.M |
| 8CMPD0650 | Compressor NM 650 |
| 8CMPD075 | COMPRESSOR DIESEL 750 |
| 8CMPD150 | Compressor 150 pCm |
| 8CMPD650 | Compressor 650 C.F.M |
| 8COB | Compactor Cat 563 |
| 8COB850T | VIBRATOR SINGLE DRUM B |
| 8CPT1.8 | Cable Puller Timberland P20 |
| 8CRANE20 | Crane 20 ton RT-58D |
| 8CRHYDC50 | CRANE HYDRAULIC 50 TON |
| 8CRMOB100 | CRANE MOBILE 100 TON |


| HR | 1 | 124.380 | 0.003 | 124.383 | 2011-09-29 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| HR | 1 | 200.000 | 0.003 | 200.003 | 2011-11-11 |
| HR | 1 | 0.000 | 0.002 | 0.002 |  |
| HR | 1 | 233.800 | 0.003 | 233.803 | 2011-09-29 |
| HR | 1 | 300.000 | 0.003 | 300.003 | 2011-11-11 |
| HR | 1 | 331.640 | 0.004 | 331.644 | 2011-09-29 |
| HR | I | 430.000 | 0.003 | 430.003 | 2011-11-11 |
| HR | I | 67.010 | 0.003 | 67.013 | 2011-11-11 |
| HR | 1 | 250.000 | 0.003 | 250.003 | 2011-11-11 |
| HR | 1 | 2.800 | 0.003 | 2.803 | 2011-11-11 |
| HR | 1 | 90.800 | 0.001 | 90.801 | 2011-09-29 |
| HR | I | 2.000 | 0.003 | 2.003 | 2011-11-11 |
| HR | 1 | 290.000 | 0.003 | 290.003 | 2011-11-11 |
| HR | 1 | 270.000 | 0.003 | 270.003 | 2011-11-11 |
| HR | I | 304.000 | 0.003 | 304.003 | 2011-11-11 |
| HR | 1 | 170.000 | 0.003 | 170.003 | 2011-11-11 |
| HR | I | 52.100 | 0.003 | 52.103 | 2011-11-11 |
| HR | I | 58.910 | 0.003 | 58.913 | 2011-11-11 |
| HR | 1 | 77.000 | 0.003 | 77.003 | 2011-11-11 |
| HR | 1 | 150.220 | 0.004 | 150.224 | 2011-09-29 |
| HR | I | 199.190 | 0.005 | 199.195 | 2011-09-29 |
| HR | 1 | 5.000 | 0.000 | 5.000 | 2011-12-05 |
| HR | I | 45.000 | 0.000 | 45.000 | 2011-12-03 |
| HR | I | 146.280 | 0.003 | 146.283 | 2011-11-11 |
| HR | I | 266.000 | 0.003 | 266.003 | 2011-11-11 |
| HR | I | 5.000 | 0.003 | 5.003 | 2011-11-11 |
| HR | 1 | 45.000 | 0.003 | 45.003 | 2011-11-11 |
| HR | 1 | 50.000 | 0.003 | 50.003 | 2011-11-11 |
| HR | 1 | 13.870 | 0.001 | 13.871 | 2011-09-29 |
| HR | 1 | 5.000 | 0.003 | 5.003 | 2011-11-11 |
| HR | 1 | 30.000 | 0.003 | 30.003 | 2011-11-11 |
| HR | I | 62.840 | 0.004 | 62.844 | 2011-09-29 |
| HR | 1 | 115.800 | 0.003 | 115.803 | 2011-09-29 |
| HR | 1 | 144.000 | 0.003 | 144.003 | 2011-11-11 |
| HR | I | 154.430 | 0.003 | 154.433 | 2011-09-29 |
| HR | I | 20.000 | 0.003 | 20.003 | 2011-11-11 |
| HR | I | 2,000.000 | 0.000 | 2,000.000 | 2011-11-30 |


| 8CRTC050 | CRANE ROUGH TERRAIN 5 |
| :--- | :--- |
| 8CRTC100 | Crane Rough Terrain 100 Ton |
| 8CRTOW20 |  |
| 8CRW150 | CRANE CRAWLER 150 TON |
| 8CRW200 | Crane Crawler 200 Ton |
| 8CRW250 | CRANE CRAWLER 250 TON |
| 8CRW300 | Crane Crawler 300 Ton |
| 8CRWN17 | Nodwell 17 ton Crane |
| 8CRWTC | Tower Crane |
| 8CSB16 | Chainsaw 16" blade |
| 8CT18T BOOM | BOOM TRUCK 18 TON |
| 8CUTTO | Cutting Torch |
| 8CXLT0106 | Lokotrack LT 106 Primary |
| 8CXLT0200 | Lokotrack LT 200 Tertiary |
| 8CXLT1100 | Lokotrack LT 1100 Secondary |
| 8CXLTSP | Lokotrack Screening Plant |
| 8DD03 | Dozer D-3 |
| 8DD05 | Dozer D-5 |
| 8DD05W | Dozer D-5 With Winch |
| 8DD08N | DOZER C/W U-BLADE CAT |
| 8DD09R | DOZER C/W U-BLADE CAT |
| 8DNDM | Drill Manual |
| 8DNM601 | Drill NM 601 |
| 8DRCHYD7 | HYDRAULIC DRILL ROC D7 |
| 8DRCHYDR47 | HYDRAULIC CRAWLER DRI |
| 8DRM | Drill Manuel |
| 8DRRO601 | Drill Rock 601 |
| 8EQPFS | Equipment for fuison |
| 8GEN020 | GENERATOR DIESEL 20 KW |
| 8GEN05 | Generator 5 kw |
| 8GEN060 | Generator Diesel 60 KW |
| 8GEN150 | GENERATOR DIESEL 150 K |
| 8GR14H | GRADER 14H CAT |
| 8GR14M | Grader 14M |
| 8GR16H | GRADER 16H CAT |
| 8GROUT | Grout Plant |
| 8HELI | Helicopter |
|  |  |


| Unit | Type | Rent Rate | EOE | Total | Updated |
| :---: | :---: | :---: | :---: | :---: | :---: |
| HR | I | 44.130 | 0.001 | 44.131 | 2011-09-29 |
| HR | I | 90.000 | 0.003 | 90.003 | 2011-11-11 |
| HR | 1 | 4.390 | 0.003 | 4.393 | 2011-11-11 |
| HR | I | 31.110 | 0.003 | 31.113 | 2011-11-11 |
| HR | I | 5.000 | 0.003 | 5.003 | 2011-11-11 |
| HR | I | 15.000 | 0.003 | 15.003 | 2011-11-11 |
| HR | I | 10.200 | 0.003 | 10.203 | 2011-11-11 |
| HR | 1 | 15.690 | 0.003 | 15.693 | 2011-11-11 |
| HR | , | 76.440 | 0.003 | 76.443 | 2011-09-29 |
| HR | I | 150.770 | 0.005 | 150.775 | 2011-09-29 |
| HR | I | 434.900 | 0.003 | 434.903 | 2011-11-11 |
| HR | I | 27.660 | 0.001 | 27.661 | 2011-09-29 |
| HR | I | 80.000 | 0.003 | 80.003 | 2011-11-11 |
| HR | , | 10.000 | 0.003 | 10.003 | 2011-11-11 |
| HR | , | 15.000 | 0.003 | 15.003 | 2011-11-11 |
| HR | I | 70.440 | 0.001 | 70.441 | 2011-09-29 |
| HR | I | 2.000 | 0.003 | 2.003 | 2011-11-11 |
| HR | 1 | 3.500 | 0.003 | 3.503 | 2011-11-11 |
| HR | 1 | 6.910 | 0.003 | 6.913 | 2011-11-11 |
| HR | I | 8.720 | 0.003 | 8.723 | 2011-11-11 |
| HR | , | 10.000 | 0.003 | 10.003 | 2011-11-11 |
| HR | 1 | 15.000 | 0.003 | 15.003 | 2011-11-11 |
| HR | I | 30.280 | 0.003 | 30.283 | 2011-11-11 |
| HR | 1 | 136.000 | 0.003 | 136.003 | 2011-11-11 |
| HR | 1 | 13.000 | 0.003 | 13.003 | 2011-11-11 |
| HR | I | 40.000 | 0.003 | 40.003 | 2011-11-11 |
| HR | I | 25.000 | 0.003 | 25.003 | 2011-11-11 |
| HR | I | 102.290 | 0.003 | 102.293 | 2011-11-11 |
| HR | I | 118.250 | 0.003 | 118.253 | 2011-11-11 |
| HR | I | 153.390 | 0.004 | 153.394 | 2011-09-29 |
| HR | 1 | 177.430 | 0.005 | 177.435 | 2011-09-29 |
| HR | I | 63.290 | 0.003 | 63.293 | 2011-11-11 |
| HR | 1 | 50.000 | 0.003 | 50.003 | 2011-11-11 |
| HR | I | 8.000 | 0.003 | 8.003 | 2011-11-11 |
| HR | I | 80.000 | 0.003 | 80.003 | 2011-11-11 |
| HR | 1 | 28.440 | 0.002 | 28.442 | 2011-09-29 |
| HR | 1 | 19.820 | 0.001 | 19.821 | 2011-09-29 |




$\qquad$


## STANDARD EQUIPMENT LIST



| Equip Code | Description | Unit | Type | Rent Rate | EOE | Total | Updated |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 8WT1 | Wild T-1 \& Tripod | HR | 1 | 3.000 | 0.003 | 3.003 | 2011-11-11 |
| 8ZBT100 | Boom Trk 100' boom | HR | I | 200.000 | 0.003 | 200.003 | 2011-11-11 |
| 8ZCABL | Cablette de Tirage Timber | HR | 1 | 33.000 | 0.003 | 33.003 | 2011-11-11 |
| 8ZCC | Cableway carriage | HR | 1 | 11.000 | 0.003 | 11.003 | 2011-11-11 |
| 8ZCHEV | Chevalet Deroulage Timberla | HR | I | 3.000 | 0.003 | 3.003 | 2011-11-11 |
| 8ZCPBC | Break Cable T25-15 | HR | I | 35.000 | 0.000 | 35.000 | 2011-12-04 |
| 8ZCPTP20 | Cable Puller Timb P20 | HR | I | 24.000 | 0.000 | 24.000 | 2011-12-04 |
| 8ZNLT | Norm Lost Time Eq Cost | HR | 1 | 0.000 | 0.003 | 0.003 | 2011-11-11 |
| 8ZNTR | Norm Travel Eq Cost | HR | I | 0.000 | 0.003 | 0.003 | 2011-11-11 |
| 8ZP100 | Press 100T | HR | I | 10.000 | 0.003 | 10.003 | 2011-11-11 |
| 8ZPD | Poulie Deroulage 1 Cable | HR | 1 | 0.850 | 0.003 | 0.853 | 2011-11-11 |
| 8ZPTL300 | Puller Timberland P-300 | HR | 1 | 35.000 | 0.003 | 35.003 | 2011-11-11 |
| 8ZRC580 | Retro Chrgr 580 Case | HR | 1 | 33.000 | 0.003 | 33.003 | 2011-11-11 |
| 8ZRPR | Remorque pour rebobineuse | HR | I | 4.570 | 0.003 | 4.573 | 2011-11-11 |
| 8ZRT6811 | Reenrouleur TL 6811 | HR | I | 5.360 | 0.003 | 5.363 | 2011-11-11 |
| 8ZT1 | T1 Wild \& Tripod | HR | 1 | 3.000 | 0.003 | 3.003 | 2011-11-11 |
| 8ZTENS | Tensioneur Timberland | HR | I | 47.500 | 0.003 | 47.503 | 2011-11-11 |
| 8ZZFUEL | Fuel | LTR | 1 | 1.090 | 0.003 | 1.093 | 2011-11-11 |
| 8ZZMISCT | Misc Tools | HR | 1 | 10.000 | 0.003 | 10.003 | 2011-11-11 |
| 8ZZOPC | Operating Cost | HR | 1 | 1.000 | 0.003 | 1.003 | 2011-11-11 |

[^1]| SNC+ LAVALIN | DG3 Capital Cost Estimate - Basis of Estimate Nalcor Doc. No. LCP-SN-CD-0000-EP-ES-0002-01 | Revision |  | Page |
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## Appendix 5

## Estimate Ground Rules

## Lemay, Paul

To:
Subject:
Lemay, Paul
Estimate ground rules

Gentlemen,
In order to have a reliable estimate as much as possible and avoid inaccurate pricing, here are the setting rules for all of us:

Most of you will prepare your estimate on an EXCEL format, with the exception of Jim Daubersmith who has the HCSS license, and it is important we follow the same pattern, so it will be easy to transfer the data into HCSS, after.

Each package has a sequence number that relate to a proper physical element and must be carried out for each activity of your estimate items. I am including the general list with an example to follow.

## ESTIMATE DETAILS INSTRUCTIONS:

## DIRECTS COSTS:

## - CONSTRUCTION EQUIPMENT, HOURLY RATE:

We will use the 2011, first half of the year, of the Equipment Watch, BLUE BOOK edition, and more specifically, their FHWA, rates. I will email you the starter list I have prepared, and you can add other pieces of equipment as required, but always from the BLUE BOOK edition. If you do not have this edition, please send me your list of equipment and I will forward you the rates.

Note for Jim Daubersmith: I put an hourly plug price to start with, for the "Concrete Batch Plant" and the "Crusher", but it must be re-adjust depending of the size we will be using and the production we will need to face. (See details at, OTHERS).

- LABOR RATES:

We will use the NALCOR Trade Labor Rates that was provided to us and I am forwarding it to all of you. In general we will use a sole rate, including all the fringes and benefit normally carried out here in NL. The workings hours will be $10 \mathrm{hrs} /$ day, two shifts and 7 days per week long, on a 21-7 rotation cycle.

- PERMANENT MATERIALS \& STS:

I have prepared a general list of plugs for permanents materials, STS and Subs, you can add some more if you need to.
The concrete plug price indicated in the PM's list, will be use in the estimate for the small quantities that some of you may have, I am talking less than 200 m 3 . Same thing for the crushed stone of small diameter for various purpose and again, less than 500 TM ( or $300 \mathrm{m3}$ )

- OTHERS:

A separate price prepared by Jim Daubersmith must be developed and re-imported into the proper item of the estimate under a \# item like (\#CONCR for the concrete ).

For the filtered zone material of the cofferdams and the RCC materials, CGC will prepare a price for the crusher ( \# CRUSH ) and the stockpile zone, and Daubersmith will take is aggregates from these stockpile, since the Concrete Batch plant and the Crusher will be in the same laydown area.

For over break concrete, consider 500 mm horizontal and 300 mm vertically.

## INDIRECTS COSTS:

For the indirect costs, I suggest that after you have done it, you enter the total indirect cost on one a line entry on your Direct cost "EXCEL" Summary Sheet, or HCSS entry:
I have include an example ( see Appendix I)

- Instructions to follow while making your price:

Mobilization \& Demobilization: Assume that "THE CONTRACTOR" will come from a maximum of 2000 km " radius" for travelling purpose of the staff and crew, and for the fleet equipment mobilization, a flat rate of $\$$ 7,500 / trip ( ground travel, low boy or highboy )
For air travel, use a \$ 700 / trip / person on a 21-7 rotation cycle.
Note: A 1,500 man-camp facilities, will be located at approximately 10 km from the site. Arrange Shuttle bus, for transportation of all craft personal.
Also, an area will be assigned at the camp site for his offices if he desire it, but all the warehouses, mechanical shop, garage will be at the lay down area approximately 2 km from the construction site.

Supervision: We will use a unique all inclusive rate per week / per person ( covering fringes, overtime ( 70 -hrs ), remoteness premium, bonus, etc ). I have included a list of the main position and the all inclusive rate to use as follow:

Project Manager: \$6,000
General superintendant: \$5,500
Field engineer: \$ 4,000
Intermediate engineer: \$4,000
Secretary: \$ 2,000
Administrator/ accountant: \$3,500
Inspector: \$ 3,500
Quality engineer: \$ 3,000
Planner: \$ 3,000
Draftsman: \$ 2,800
Cost engineer: \$ 3,000
Surveyors: \$3,500
Temporary buildings set-up \& dismantle: No particular comment, but don't forget to include provision for winter protection if applicable!

## Utility supply ( air, water and power ):

Air: Use diesel or electric compressor at 0.08 / kw -hr and $\$ 1,50$ / liter for the piece of equipment not mention in the main Equipment list.
Water: Industrial water can be obtained direct from the river for the construction needs and potable water will be available at the camp site.
Electricity: A supply of $2,0 \mathrm{MVA}$ will be available at the lay down area located at approximately 2 km from the site, mainly for the concrete batch plant and the crusher equipments. However, at the site itself, the power available should be around 0,5 MVA.

For the peak needs, use propane gas (ex: winter shelter heating )
Job cars \& pick-up and support equipment:

Use shuttle to transport workers at site. Pick-up for superintendant, quality control \& survey are recommended, but not all staff of the contractor.

Job office expenses: I suggest you use a dollar figur, for each craft hour of the job.
Administration fees: ( head office expense, overhead \& profit )

Contingency: Do not include anything at this item.

## Paul Lemay, p.eng

 Lead Estimator.Lower Churchill Project
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## SNC•LAVALIN


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[^1]:    All costs are per hour.
    I/O indicates whether the rent is inside (company) or outside.

